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AN ADDITIONAL STUDY AND IMPLEMENTATION OF
TONE CALIBRATED TECHNIQUE OF MODULATION

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Final Report

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1. INTRODUCTION

The material presented in this Final report is concerned with the work performed on An Additional Study and Implementation of Tone Calibrated Technique of Modulation for the Jet Propulsion Laboratory, contract number 957190.

Earlier studies [1,2,3] have shown that pilot-aided coherent modulation techniques, of which the Tone Calibrated Technique (TCT) is an example, can be used to alleviate the effects of multipath fading in Land Mobile Radio (LMR) communication links. It appears, at the moment, that there are no commercial pilot-aided LMR links in operation. Conventional LMR links predominantly use non-coherent detection methods at the receiver to allow rapid burst signal acquisition. This also has the advantage of fast re-acquisition of the transmit signal when multipath fading is encountered. However, non-coherent detection generally has a poorer bit error rate (BER) performance than coherent and differentially coherent detection schemes.

Coherent detection schemes which regenerate a phase reference directly from the received signal, are typically not used on LMR links due to the complexity involved in configuring them to track fading signals. As an alternative, pilot-aided techniques have much to offer due to the presence of a transmitted reference. They are the subject of this report. The differentially coherent receiver enjoys a BER performance which, for additive white gaussian channels, lies somewhere between that of the coherent and non-coherent detection schemes. In the presence of multipath fading, this receiver displays an irreducible error detection floor, just as the in the case of the non-coherent detector.

The TCT communication method has been shown [4] to be theoretically free from an error floor, and is only limited, in practice, by implementation constraints. Section 2 of this report introduces the concept of the TCT transmission scheme along with a baseband implementation of a suitable demodulator. Two techniques for the generation of the TCT signal are considered: a Manchester source encoding scheme (MTCT) and a subcarrier based technique (STCT).

Section 3 summarizes the results of the TCT link computer simulation which was previously described in detail in the First Interim Report[5]. Section 4 addresses the hardware implementation of the MTCT system and outlines the digital signal processing design considerations involved in satisfying the modulator/demodulator requirements.

Section 5 presents a discussion on the program findings and suggests future directions based on conclusions made regarding the suitability of the TCT system for the transmission channel presently under consideration.

2. TCT DATA TRANSMISSION SYSTEM

The Tone Calibrated Technique has been explored in a related program [1], sponsored by JPL, and discussed in the open literature [2]. The underlying concept is the use of a pilot, or tone, to synchronously remove channel perturbations from the data bearing sidebands and, simultaneously, perform coherent data detection. This requires that the pilot be situated at a suitable location in the transmit frequency band; the channel distortions should be distributed symmetrically around this location and there should be no data sideband energy present. It also assumes that the transmit link is linear to avoid capture of the pilot due to hardlimiting effects.

The TCT system positions the pilot at the midpoint of the transmit band. Prior to carrier modulation, the data modulated signal has been removed from this location by the creation of a spectral null at zero frequency. The data modulation scheme employed is M-ary Phase Shift Keying (PSK); this requirement is imposed by channel bandwidth constraints and is not a limitation of the TCT method, which is compatible with many other types of modulation schemes. For the given signalling requirements, the transmission of data at a rate of 2.4 kbps in a 3.6 kHz RF bandwidth, using quadriphase PSK (QPSK) modulation offers the minimum possible PSK signalling set.

The previous TCT program [1] was concerned with the proof-of-concept phase and was principally a hardware implementation study. Of major interest was the realization of the TCT demodulator and its performance in the presence

of additive white gaussian noise (AWGN) and hardware simulated multipath fading. An IF TCT demodulator was designed and studied. Results derived from the experimental set-up indicated that the pilot-aided demodulation could remove the error floor normally associated with non-coherent and strictly coherent receivers, the latter case holding true when conditioned on the fact that no attempt has been made to compensate for fading effects. This result was subsequently supported by theoretical analyses [4]. The TCT system bit error rate performance appears to be acceptable given the power penalty of including the pilot. This encouraging result was somewhat overshadowed by the doubling of the transmit bandwidth over that actually required by other modulation schemes. This is due to the Manchester source encoding which was employed to generate the spectral null around zero frequency.

Although the bandwidth constraints can be mitigated by using higher order PSK signalling sets, it is reasonable to assume that their use would cause the link bit error rate performance to degrade significantly due to the reduced decision space and sensitivity to the recovered pilot.

This report is concerned with two major areas of the TCT system, (a) the generation of the pre-modulation spectral null in the transmitter and (b) the use of baseband processing techniques to implement the demodulator. The use of digital signal processing elements to implement both the modulator and demodulator was considered to be a key element and, consequently, is a topic of detailed discussion in the report.

Two schemes were initially investigated for the generation of the TCT signalling format and are described in the remainder of this section. The first to be considered is based on a Manchester encoding scheme to generate the spectral null at the transmitter; this was the method investigated in the previous study. The other method considered centers on the use of subcarrier modulation techniques for spectral null generation. It was decided during the course of the program, primarily due to time constraints, to pursue only the Manchester TCT system to full hardware implementation.

2.1 Manchester Encoded TCT

2.1.1 Modulator

Manchester source encoding acts upon the input digital data in such a way as to redistribute the data energy away from zero frequency. The resulting power spectrum is given by:

$$M(f) = \sin^2(x) \operatorname{sinc}^2(x) \quad (2.1)$$

where

$$x = \pi f T_s / 2$$

$$\operatorname{sinc}(x) = \sin(x)/x$$

Eqn. (2.1) clearly shows that a null is created at zero frequency and that the main spectral lobe has almost doubled in width. To meet the single-sided RF occupancy requirements, which call for the transmit signal to be attenuated by 40dBC at 1.8 kHz removed from the center of the band, some form of spectral shaping must be used. The shaping employed is the raised-cosine pulse in the frequency domain with a maximum excess bandwidth fraction, β , of 0.5. The shaping is implemented as a time domain function and can be expressed as follows:

$$p(t) = \frac{\sin(\pi t/T_b)}{\pi t/T_b} \frac{\cos(\pi \beta t/T_b)}{(1-(2\beta t/T_b)^2)} \quad -\infty < t < \infty \quad (2.2)$$

where T_b is the bit rate, 2.4 kbps. The corresponding frequency spectrum is given by eqn.(2.3).

$$p(f) = \begin{cases} 1; & 0 \leq f \leq (1-\beta)/2T_b \\ \frac{1}{2} [1 - \sin(\pi T_b (f - 1/2T_b)/\beta)]; & \frac{(1-\beta)}{2T_b} \leq f \leq \frac{(1+\beta)}{2T_b} \end{cases} \quad (2.3)$$

As previously mentioned, the modulation scheme employed is QPSK, so the input data is split into even and odd streams, where the Manchester encoding and pulse-shaping will be performed independently of each other. Figure 2.1 illustrates the complete Manchester system pre-modulation data processing.

Included in both processing paths of Figure 2.1 are highpass filters to enlarge the necessary spectral null. It has been determined [1] that Manchester encoding by itself does not create a sufficiently wide spectral null. There is simply too much residual data energy which will overlap the pilot recovery passband at the receiver and result in the degradation of the TCT calibration process in the demodulator. Moreover, the pulse-shaping employed has a constant amplitude frequency response in the vicinity of d.c. (see 2.3), hence the need for additional spectral shaping through the use of the highpass filters.

The pre-modulation processing is implemented digitally, this allows for the use of linear phase, finite impulse response highpass filters. In this way, an attempt is made to minimize the effects of intersymbol interference (ISI) arising from the removal of the low frequency data energy.

The output of the highpass filters constitute the inphase (I) and quadrature (Q) components of the QPSK modulation. It is desired to use I and Q path staggering to generate offset QPSK (OQPSK) as this reduces transmit envelope amplitude variations. The Q path, $S_q(t)$, is therefore delayed $T_b/2$ seconds relative to the I path, $S_i(t)$. The exact description of $S_i(t)$ and $S_q(t)$ is delayed until section 4.2 where they are described in relation to the hardware implementation. Signals $S_i(t)$ and $S_q(t)$ are converted to analog waveforms, then passed through lowpass reconstruction filters to generate signals $S'_i(t)$ and $S'_q(t)$. These are then used to modulate a quadrature carrier pair as follows,

$$OQPSK(t) = S'_i(t)\cos(w_0 t) + S'_q(t)\sin(w_0 t) \quad (2.4)$$

where w_0 is the radian carrier frequency.

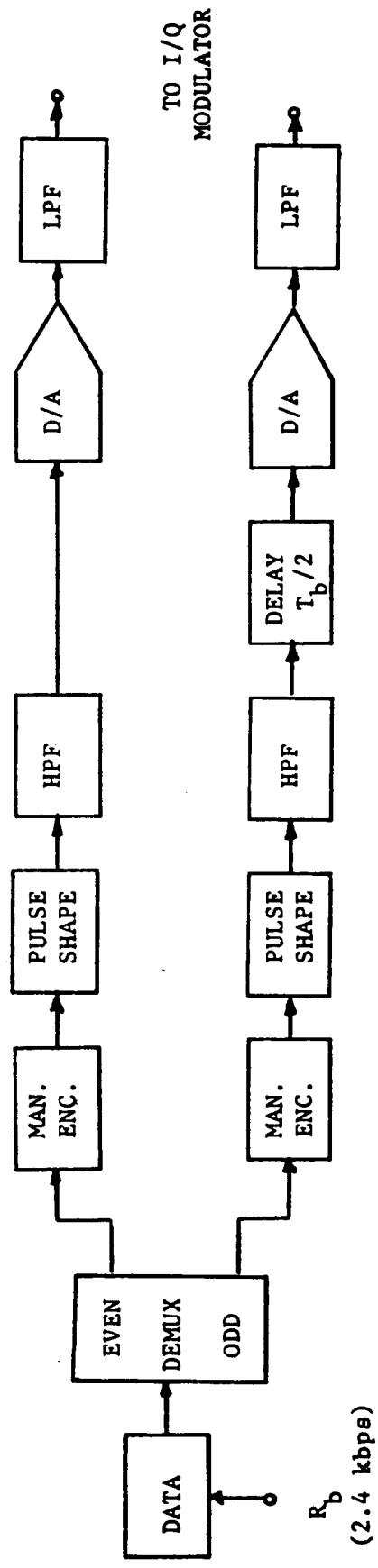


FIGURE 2.1 TCT MANCHESTER BASEBAND PROCESSING

2.1.2 Demodulator

The demodulator configuration of the previous TCT study was an IF arrangement which employed analog techniques. This study is considered to be the next stage in the TCT demodulator development since it employs digital baseband I/Q signal processing. The baseband approach is particularly attractive because its low data rate makes possible the extensive use of various DSP techniques. Many signal processing chips are commercially available, and could be utilized in this low data rate environment. This should reduce the complexity of TCT transceiver hardware as well as result in an implementation that is well suited to custom IC fabrication.

The demodulator configuration investigated was derived from that suggested by Davarian [2]. Figure 2.2 illustrates the digital Manchester based TCT demodulator.

The received signal at the demodulator consists of the pilot tone and OQPSK data signal, corrupted by multipath fading, along with a thermal noise component. This signal can be expressed as follows,

$$r(t) = aX_t \cos(w_0 t + Y_t) \quad (2.5)$$

$$+ A/\sqrt{2} S_i(t) W_t \cos(w_0 t + Y_t)$$

$$+ A/\sqrt{2} S_q(t) X_t \sin(w_0 t + Y_t)$$

$$+ N_i(t) \cos(w_0 t) + N_q(t) \sin(w_0 t)$$

The first term of eqn.(2.5) represents the the pilot term, the second and third terms correspond to the OQPSK signal, while the remaining terms are attributed to the thermal noise. X_t and Y_t are random variables which describe the amplitude and phase variations used to model the multipath fading effects [2].

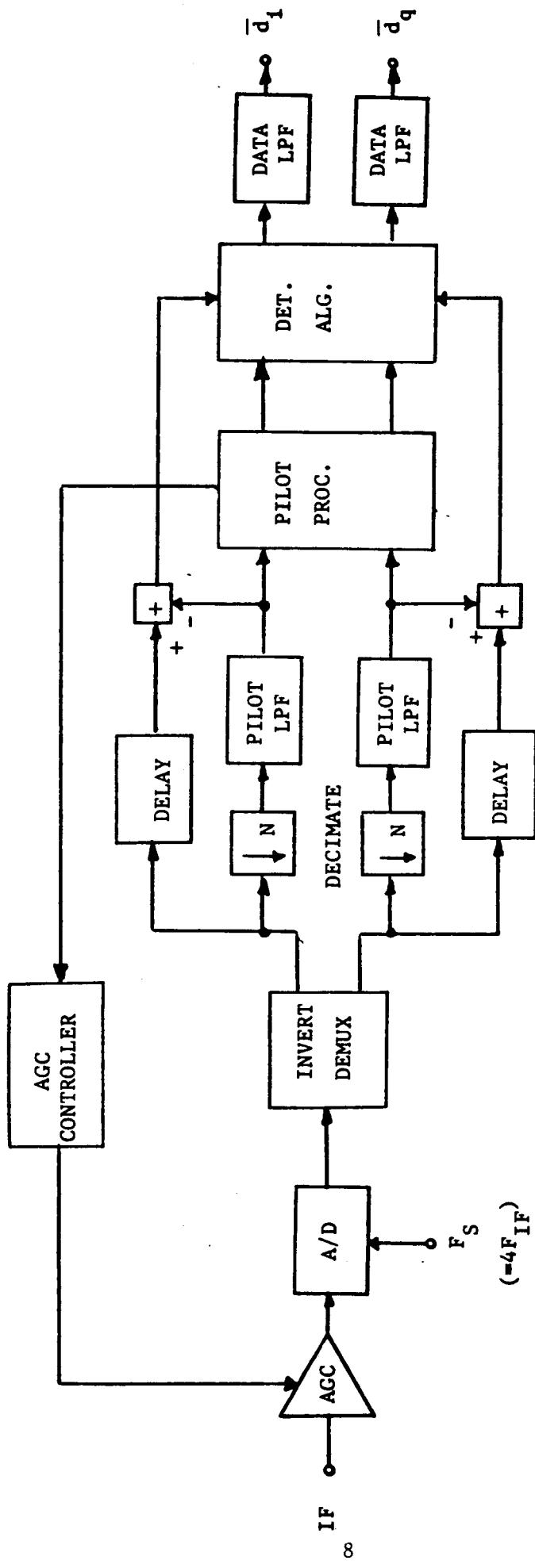


FIGURE 2.2 DIGITAL MTCT DEMODULATOR

The received signal is first passed through a bandpass filter and the AGC amplifier before it is translated to baseband, where the majority of the processing will take place. The bandpass filter is used to reduce the composite input signal strength and excess noise bandwidth. The translation to baseband is performed by mixing the received signal with quadrature sinusoids operating at the IF frequency. In this way the inphase (I) and quadrature (Q) signals necessary for baseband processing are generated.

The I and Q components of the received pilot are recovered by passing the two streams through a filter which has a passband equivalent to the fading bandwidth [1]. In parallel with this operation, the I and Q signals are also fed to a delay buffer which compensates for the overall pilot processing time. The delayed signals will eventually be utilized in conjunction with the appropriately processed pilot I and Q signals, to obtain an estimate of the transmitted data.

The received signal is corrupted by channel perturbations and for the link considered, these perturbations are induced by additive white gaussian noise and multipath fading. Hence, the recovered pilot signal will have impressed upon it amplitude and phase related information about the fading. The task of the pilot processing section is to extract this information from the recovered pilot prior to data detection. A linear TCT pilot processor that was considered previously produces an output with an amplitude component which is the reciprocal of the input pilot amplitude. This method necessitates a squaring and division operation. The processing scheme employed here uses I/Q hardlimiting in a similar fashion to that proposed earlier by Davarian[6]. This has two advantages: it removes the fading amplitude component from the recovered pilot and it simplifies the arithmetic processing requirements. The I/Q hardlimiting is performed by taking the arctangent of Q_p/I_p , recall (2.5),

$$\Psi = \tan^{-1} \left[\frac{aX_t \cos(\Omega t + \theta_0 - Y_t)}{aX_t \sin(\Omega t + \theta_0 - Y_t)} \right] = (\Omega t + \theta_0 - Y_t) \quad (2.6)$$

where θ_0 and Ωt are residual system phase and frequency offsets. It can be

seen that the amplitude fading has been removed and that the output of the arctangent function is an estimate of the phase perturbation process. This output is then passed on to the detection algorithm. Since data detection is a phase comparison process the pilot amplitude is not strictly required. The long term data sideband amplitude variations can be handled using an AGC loop with a control signal as given below. Faster variations can be addressed by maintaining a sufficient processing signal-to-noise ratio to meet the system performance requirements at low absolute input levels, however, this is probably only realistic for Rician fading channels.

The detection section of the demodulator performs the simultaneous operations of data recovery and the removal of channel phase perturbations. The output of the arctangent function is converted to sine and cosine terms which act as coherent phase references. The detection algorithm can be expressed as follows,

$$Z_I = I_D C + Q_D S \quad (2.7a)$$

$$Z_Q = Q_D C - I_D S \quad (2.7b)$$

where

$$C = 2\cos(\Psi), \quad S = 2\sin(\Psi)$$

and Ψ is as given in 2.6. I_D and Q_D are the outputs of the delay buffers from which the inphase and quadrature components of the recovered pilot, I_p and Q_p , have been removed, see Figure 2.2. This is accomplished by the action of the adders immediately following the delay buffers. Signals Z_I and Z_Q are then passed on to integrate-and-dump filters to produce estimates of the transmitted data.

An AGC control signal can be derived by taking advantage of the pilot and data detection processors. For example, the amplitude variations on the inphase pilot component can be obtained as follows.

$$E = I_p / \cos(\Psi) \quad (2.8)$$

E can then be compared to a nominal value and suitably lowpass filtered to generate a control signal which will be used to set the gain of the IF AGC amplifier.

2.2 Subcarrier TCT

The subcarrier version of the TCT (STCT) modem is, in fact, very similar to the previously described Manchester modem. The main difference between the two is the manner in which the spectral null at d.c., which is necessary for the proper transmission of the pilot tone, is created. The MTCT version relies upon Manchester coding followed by highpass filtering of the shaped data to remove unwanted sideband energy around zero frequency. The STCT method, on the other hand, modulates the shaped data onto a very low frequency subcarrier to redistribute its data sideband energy away from d.c. The resulting frequency spectra of the two methods are similar, as would be expected, however, software simulations indicate that the subcarrier method does provide some advantages, and, hence, warrants attention.

2.2.1 Modulator

Two advantages of the subcarrier method are immediately obvious. For one, the modulation allows the arbitrary location of the data sidebands in a symmetric position around d.c. Also, the pulse shaping can then be used to control the low and high-side roll-off of these sidebands, which cannot be done in the case of the Manchester encoded data.

The implementation of this STCT modulator is quite simple, see Figure 2.3. The data bits are split into even and odd streams, bipolar encoded, then pulse-shaped using the same raised-cosine filtering employed in the MTCT modulator. In this case, however, the excess bandwidth fraction must be reduced to 0.4. The shaped data streams then modulate a quadrature subcarrier signal pair operating at a frequency of 960 Hz. This frequency is a submultiple of the data clock, which is very useful from an implementation standpoint since

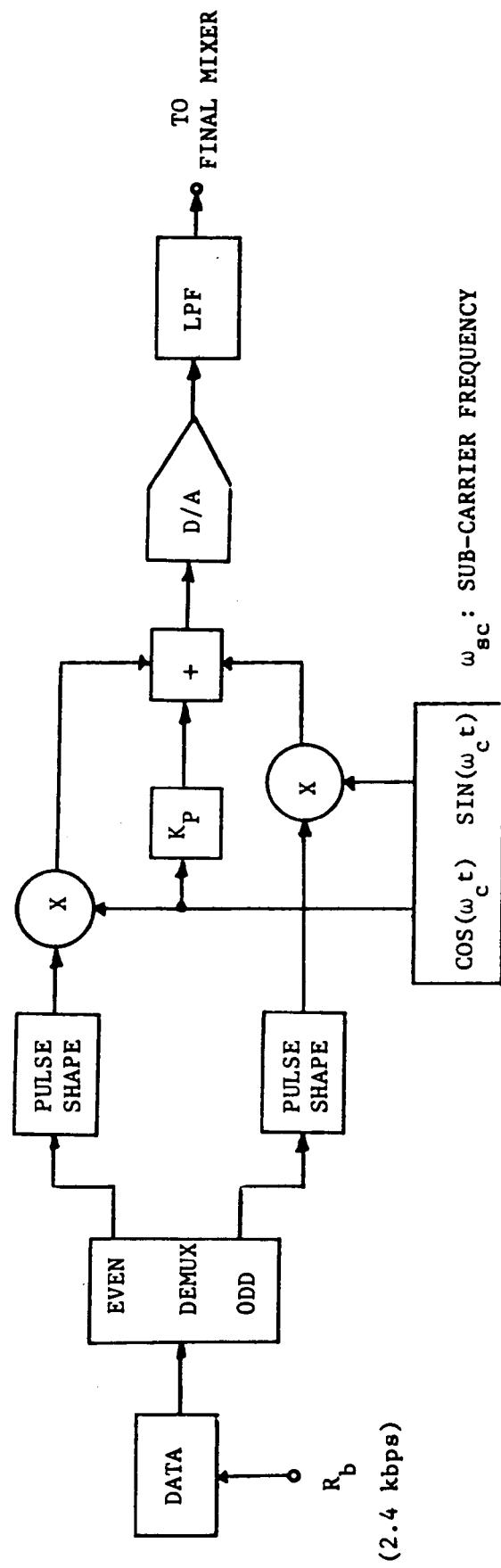


FIGURE 2.3 SUB-CARRIER TCT MODULATOR

the sine and cosine generators are effectively synchronized to this data clock.

It will be shown in section 3.2.1 that this method of frequency redistribution does in fact produce the desired null at d.c. without the need for dual highpass filters and the attendant penalty of added data ISI.

2.2.2 Demodulator

The demodulator for the subcarrier version of TCT, illustrated in Figure 2.4, resembles its MTCT counterpart. The difference here is the added remodulation and subcarrier phase estimation functions. Fading compensation and synchronous detection are performed at the subcarrier frequency; hence the need for the remodulation function which modulates the recovered pilot phase onto locally generated sine and cosine subcarrier phase references. These local references are produced by phase-locking a local source to the incoming suppressed subcarrier. It should be noted that the action of the pilot in the synchronous detector is to remove any residual frequency and phase offsets, thus the subcarrier recovery circuits, in theory, only have to align the phase of the local reference to the transmitted one.

This synchronization is performed by a first order phase-locked loop. The outputs of the final data filters serve as a source of the receive phase states. The receive phase states are compared to the known nominal receive data phase states. The angular difference between these two quantities becomes the error signal. The phase-locked loop output is an estimate of the phase difference between the local and the received subcarrier, this is added to the recovered pilot phase angle prior to the remodulation process.

3. TCT SYSTEM COMPUTER SIMULATION

The initial investigation of the baseband Tone Calibrated Technique required the development of a software simulation. A simulation was generated which omitted the modelling of any channel perturbations so that the modem performance could be evaluated solely in terms of system parameters.

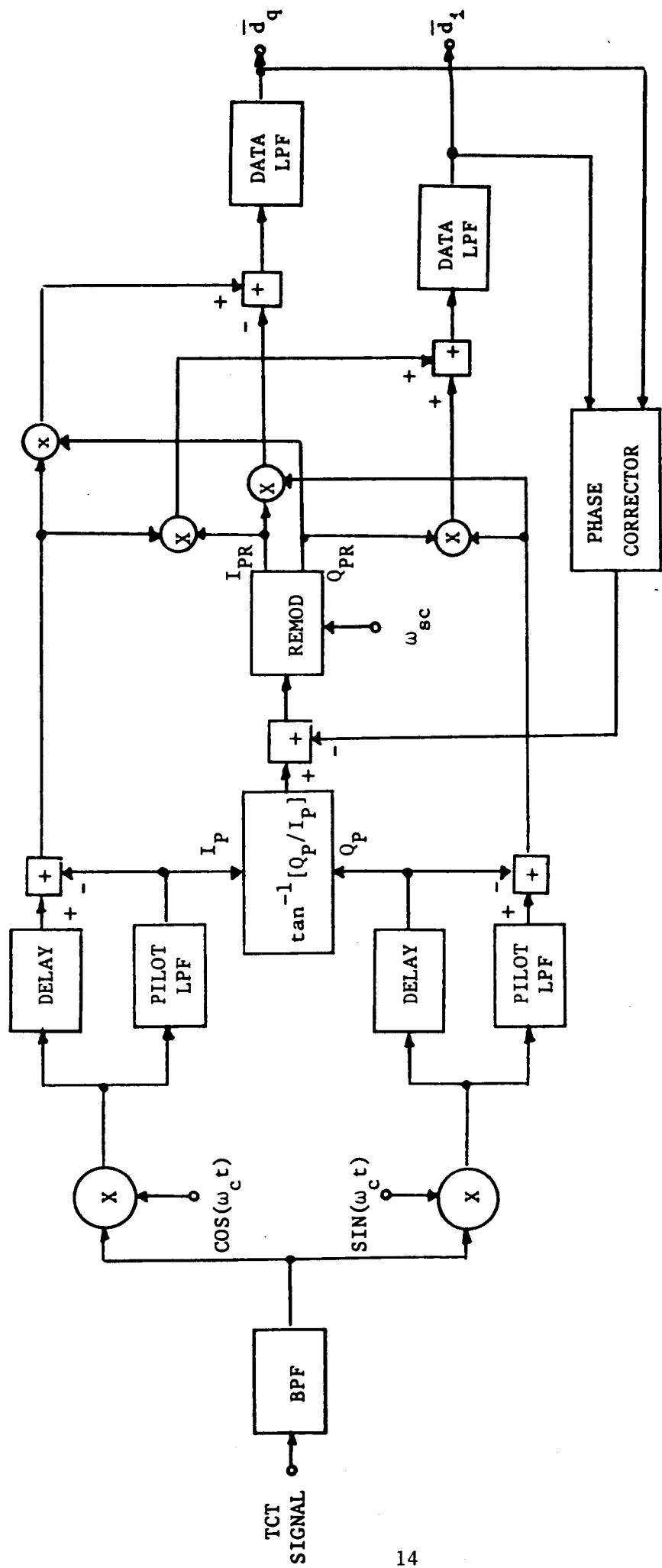


FIGURE 2.4 STCT DEMODULATOR

Subsequent development continued to focus on the signal processing structures of the modem. By concentrating on emulating the elements of the real-time implementation, the simulation effectively became a valuable design tool. The structure of the final design could be fully developed before committing it to hardware, allowing for a relatively smooth implementation. The inclusion of multipath fading and thermal noise to the simulation was not viewed as critical, since the impact of these effects would be examined in the real-time system.

The simulations were written in FORTRAN and interfaced to the Interactive Laboratory System (ILS) digital signal processing software package for purposes of graphical presentation and analysis. In addition, ILS was employed in designing all the required digital filters. Linear phase filters were used throughout to minimize phase distortion and the design algorithm employed was the Remez Exchange Algorithm which produces equiripple in both the passband and stopband. A data eye pattern was generated from a $2^{10} - 1$ pseudo-random bit sequence and the recovered eye quality was used as an indication of system performance. ILS is commercially available through Signal Technology, Inc.

Appendix I contains a program listing of the MTCT modem simulation described in the next section.

3.1 Manchester Encoded TCT

3.1.1 Modulator

The Manchester encoded TCT modulator was first simulated as shown in Figure 2.1, except without the highpass filters. Since no channel modelling was performed, the data was QPSK modulated to 12 kHz, the receiver final IF frequency. The data at IF was represented as a 48 kHz sampled signal, consistent with the demodulator IF sampling frequency.

In order to meet the specified bandwidth requirements, frequency domain raised-cosine pulse-shaping was employed with a Nyquist excess fraction, β , of 0.5 at a data rate of 2.4 kbps. Figures 3.1(a) and 3.1(b) show respectively the baseband data eye and the data eye spectrum. The pulse shape extends over

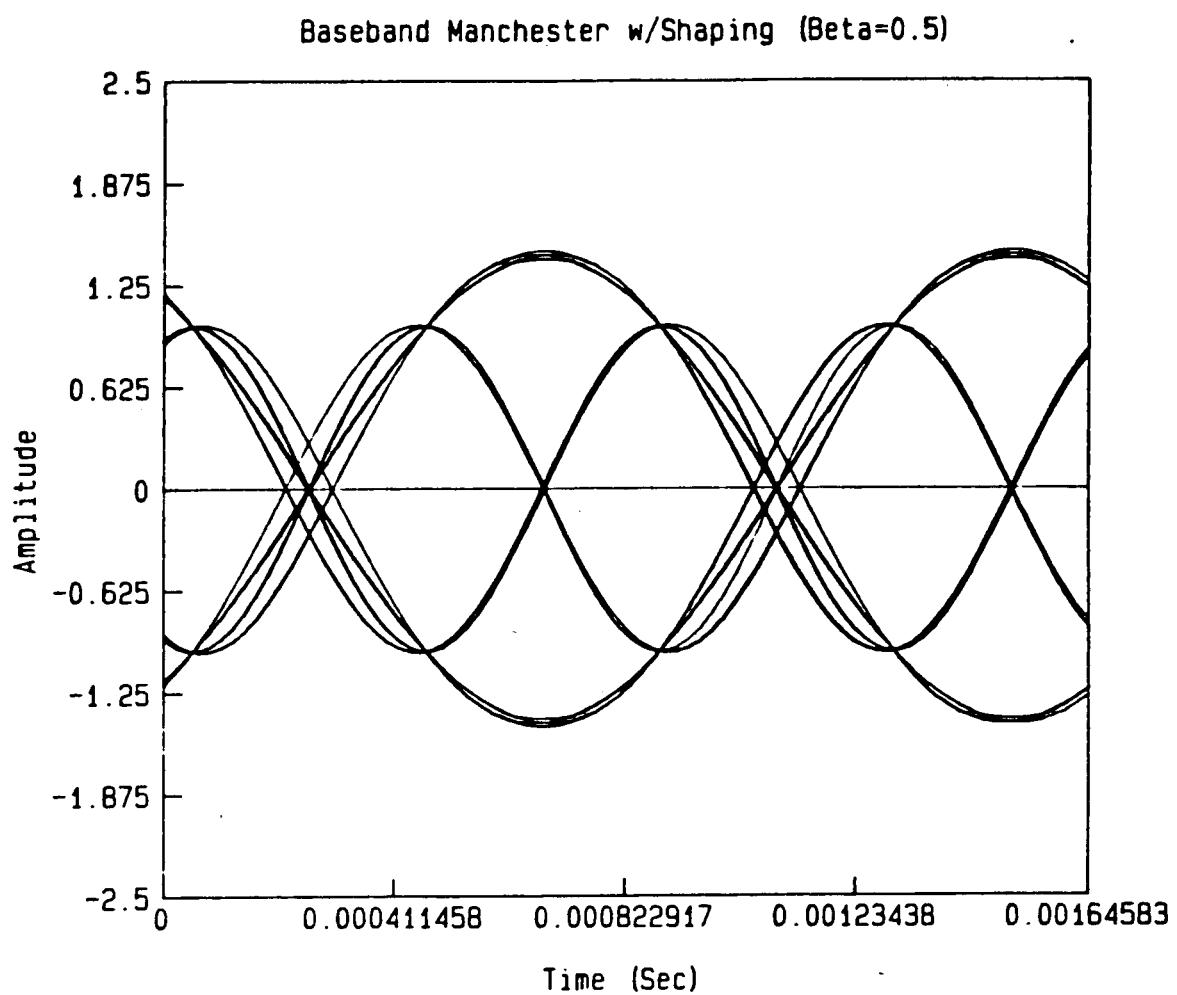


FIGURE 3.1(a) SHAPED MANCHESTER ENCODED DATA, NO HIGHPASS FILTER

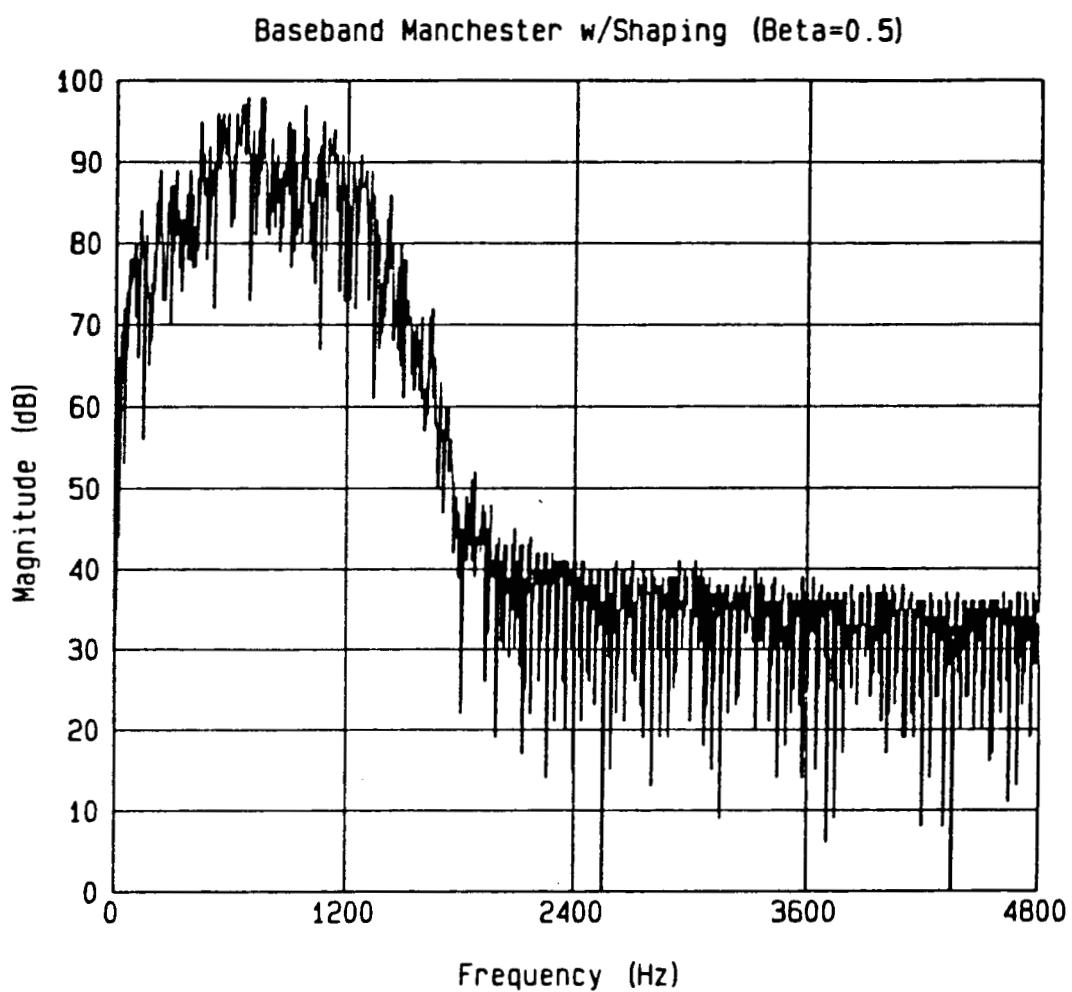


FIGURE 3.1(b) FREQUENCY SPECTRUM OF FIGURE 3.1(a)

eight Manchester bit time periods and provides sufficient spectral occupancy characteristics, i.e. over 40 dB of attenuation at 1.8 kHz from the center frequency, while generating an eye pattern with points of no ISI.

Although the pulse shaping is more than adequate in fulfilling bandwidth constraints, the generation of a zero frequency null is poorly implemented with Manchester encoding alone. A null width of 100 Hz is desired for the insertion of a carrier to track multipath fading characteristics. If a highpass filter is employed, a significant null can be created, see Figure 3.2(b); however, Figure 3.2(a) shows the distortion introduced by filtering out low frequency components from the data.

A 91 tap highpass filter is used initially as a control to establish a frequency response with a very sharp cut-off and no passband ripple. The 91 tap filter has a 3 dB point at 150 Hz and functions at the baseband processing rate of 9.6 kHz. The degradation due to this filter is approximately 16% as measured by comparing the size of the eye closure to the nominal opening. A 45 tap highpass filter design is also examined, since the longer length filter cannot be implemented in the proposed processor for the real-time system. The frequency response of this filter has a half dB ripple in the passband, a 3 dB point at 150 Hz and less attenuation in the stopband. Figures 3.3(a) and 3.3(b) show the data eye pattern and the data frequency spectrum. Both diagrams appear quite close to the 91 tap control filter simulation results, with the 45 tap filter eye pattern showing slightly more ISI.

The final step in the modulator simulation involved generating a 48 kHz sampled signal from the 9.6 kHz baseband process for the demodulator IF input requirements. This was done in two steps. First, the 9.6 kHz signal was zero insertion upsampled by a factor of 1:5 to a sampling frequency of 48 kHz. The spectrum of this signal is shown in Figure 3.4(a). The baseband spectrum is centered at multiples of 9.6 kHz. The high frequency images are then removed by lowpass filtering, yielding the spectrum of Figure 3.4(b). Although the baseband images are still recognizable, they represent negligible energy compared to the data spectrum. The 48 kHz sampled baseband data is then QPSK modulated to the 12 kHz demodulator IF frequency.

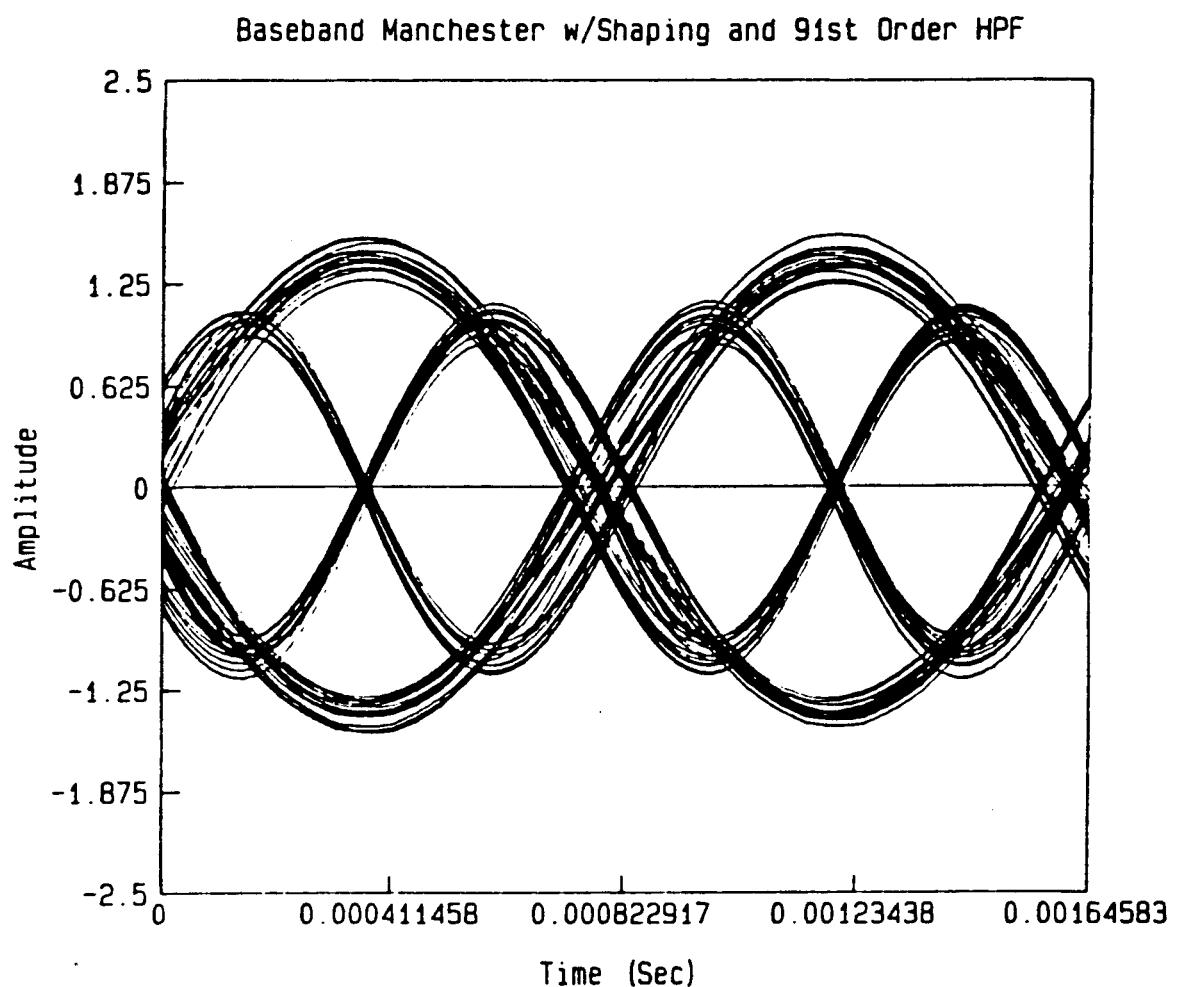


FIGURE 3.2(a) SHAPED MANCHESTER ENCODED DATA WITH HIGHPASS FILTERING
(91st ORDER)

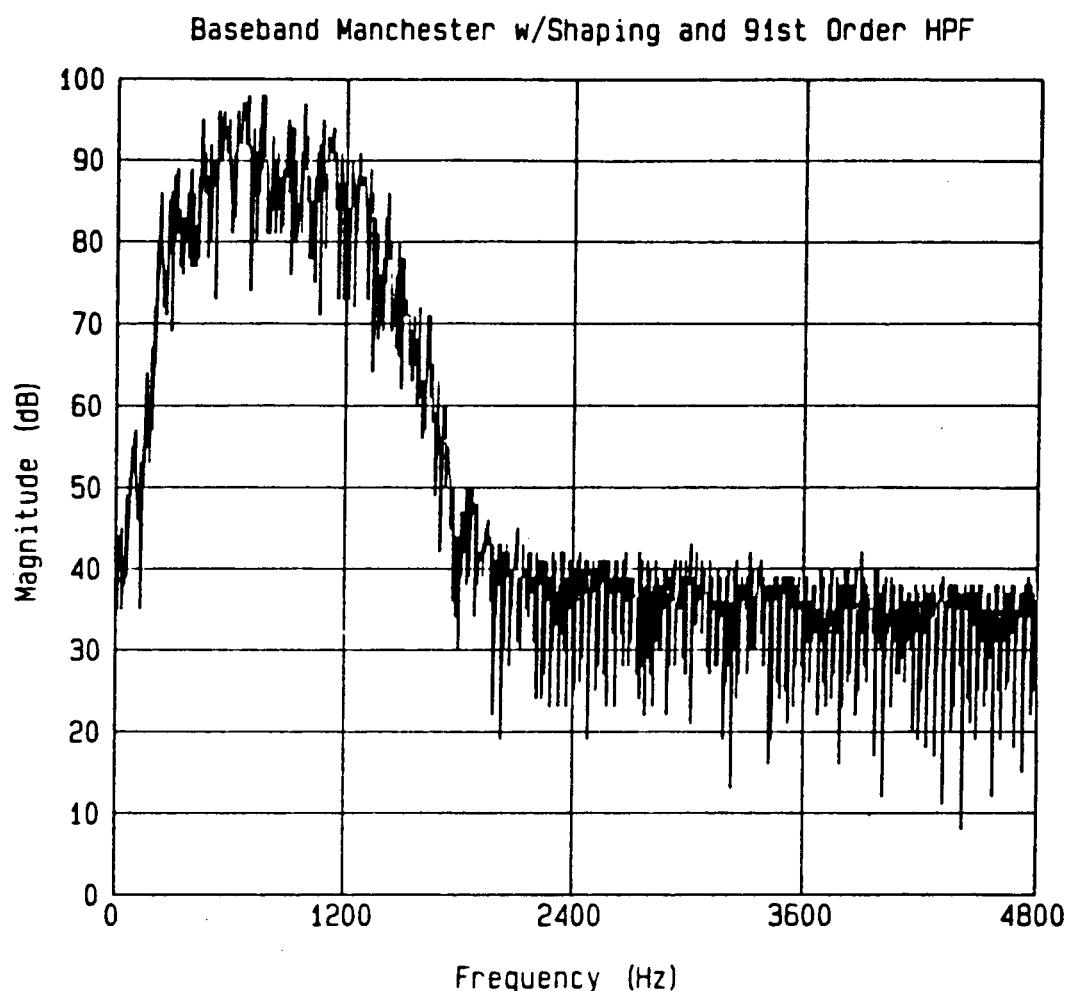


FIGURE 3.2(b) FREQUENCY SPECTRUM OF FIGURE 3.2(a)

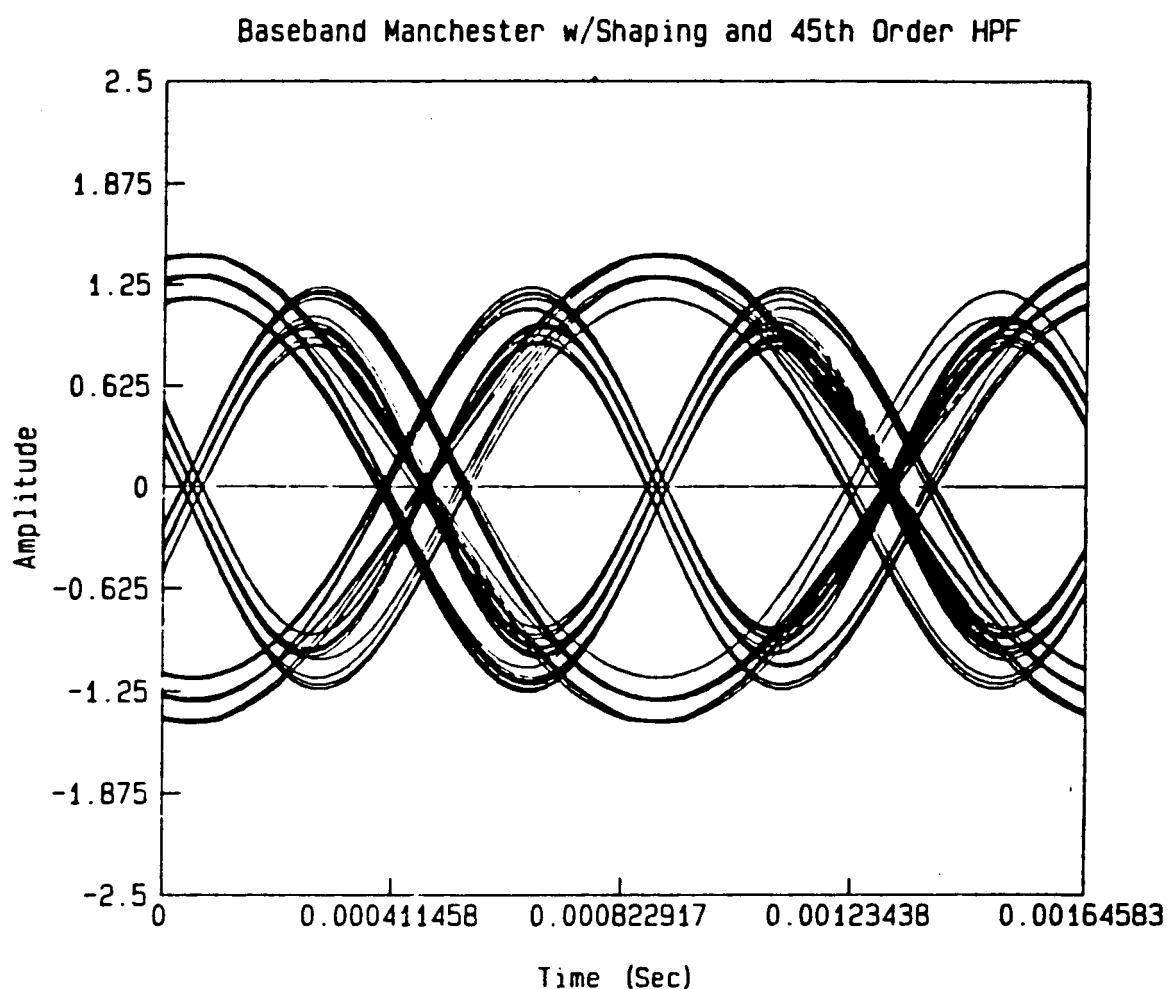


FIGURE 3.3(a) SHAPED MANCHESTER ENCODED DATA WITH HIGHPASS FILTERING
(45th ORDER)

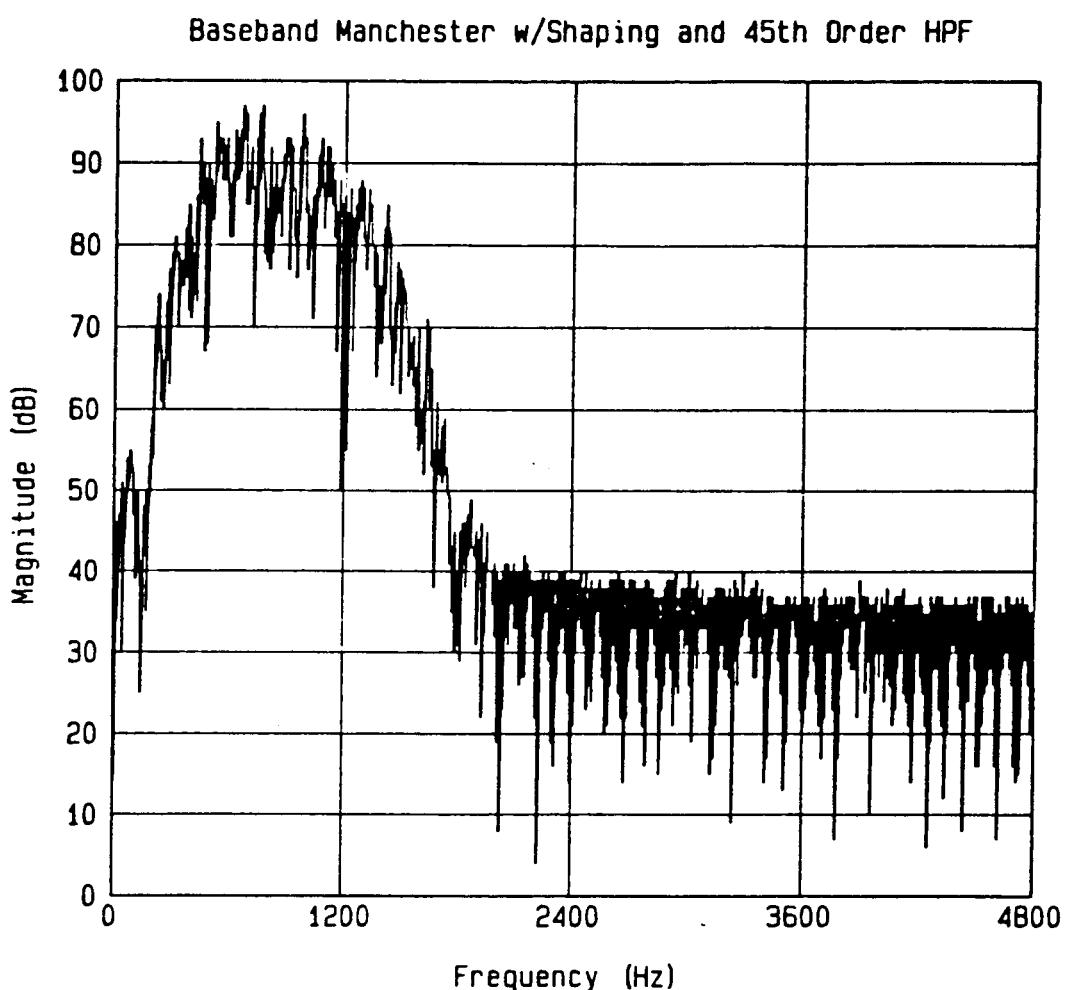


FIGURE 3.3(b) FREQUENCY SPECTRUM OF FIGURE 3.3(a)

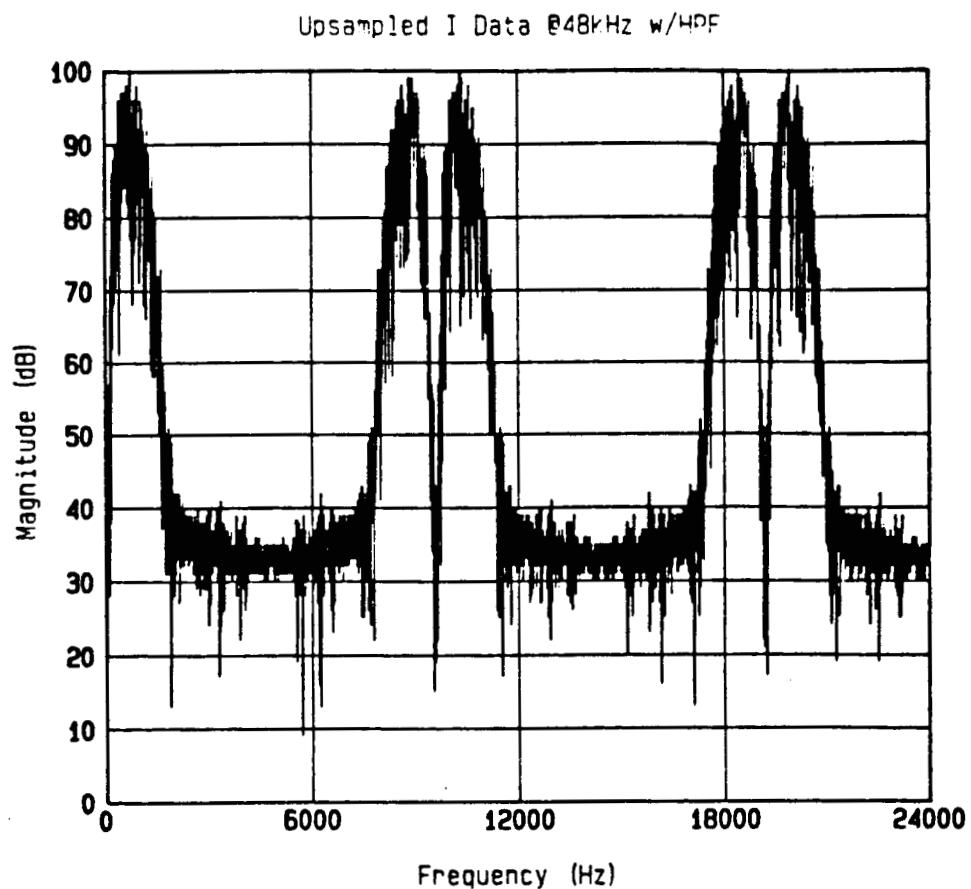


FIGURE 3.4(a) SPECTRUM OF 1:5 UPSAMPLED 9.6 kHz
INPHASE SIGNAL

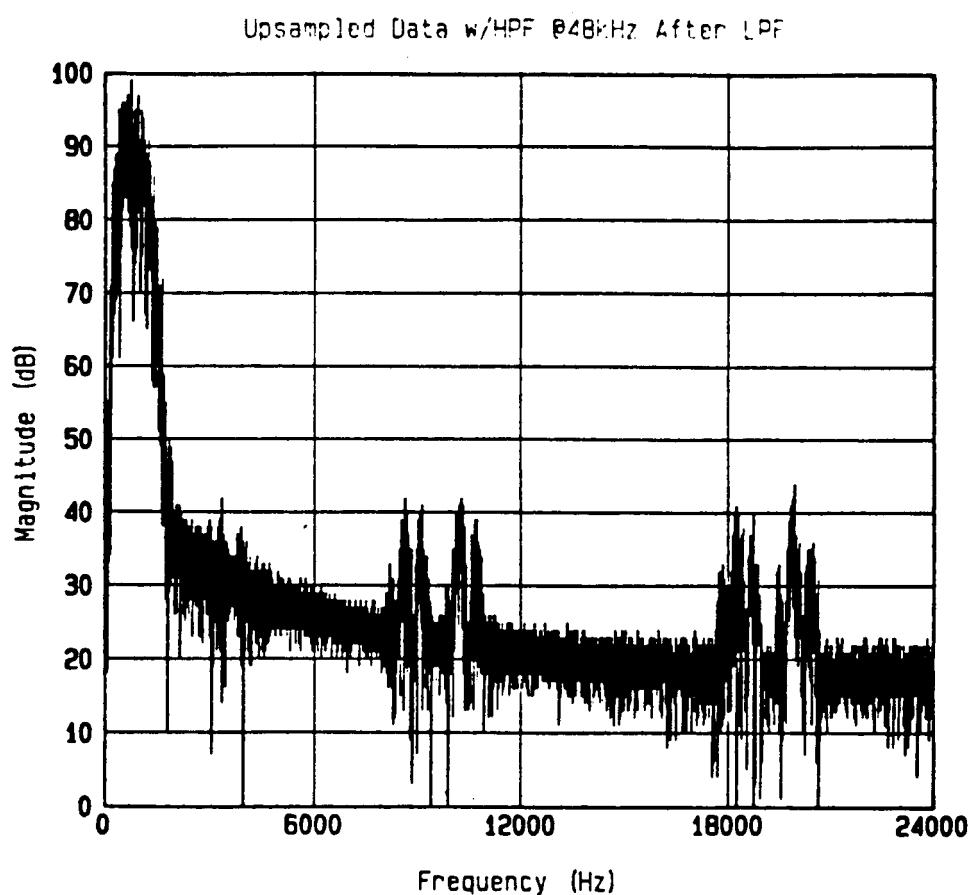


FIGURE 3.4 (b) LOWPASS FILTERED SPECTRUM OF
1:5 UPSAMPLED 9.6 kHz INPHASE SIGNAL

3.1.2 Demodulator

The demodulator of Figure 3.5 was simulated in modular form with each block representing a different signal processing task that could be tested separately for functionality. A specific effort was made during simulation development to excercise system parameters for optimization of the real-time demodulator design. The efficiencies of multi-rate processing were emphasized.

Since the analog-to-digital converter is operating at a sampling frequency of 48 kHz, four times the IF frequency, all adjacent samples are in time quadrature. Translation to baseband is achieved by multiplying with a square wave a four sample period which, in the digital domain, is spectrally identical to a sinusoid of the same frequency. Every other sample of the baseband signal is then separated into in-phase and quadrature components sampled at a 24 kHz rate. Each component is divided into two streams. One undergoes pilot recovery and the other is delay equalized to match the lowpass filtering in the pilot processing.

The advantage of lowering the sampling frequencies clearly results in reduced digital processing cost. Decimation in the signal paths leading to the pilot recovery lowpass filters significantly eases both the processing burden and the digital filter design. A decimation ratio of 5:1 causes no aliasing and improves the lowpass cut-off to sampling frequency ratio, allowing a much lower order filter implementation. The recovered pilot streams are subtracted off from the delayed data and estimates of the channel phase perturbations are passed to the detection algorithm. The pilot processing and data detection are simulated essentially as described in section 2.1.2; however, since there are different processing rates in the demodulator, some method must be chosen to handle the different rate boundaries. A full interpolation to reconstruct the lower rate signal is expensive in processing cost. A zero-order hold is simple to implement but has a poor frequency characteristic as higher frequency images roll off with only a $\sin(x)/x$ response. As a result, a first-order hold is implemented providing much better attenuation of images. The processing cost is relatively low requiring only a one sample delay in the pilot path and a linear interpolation.

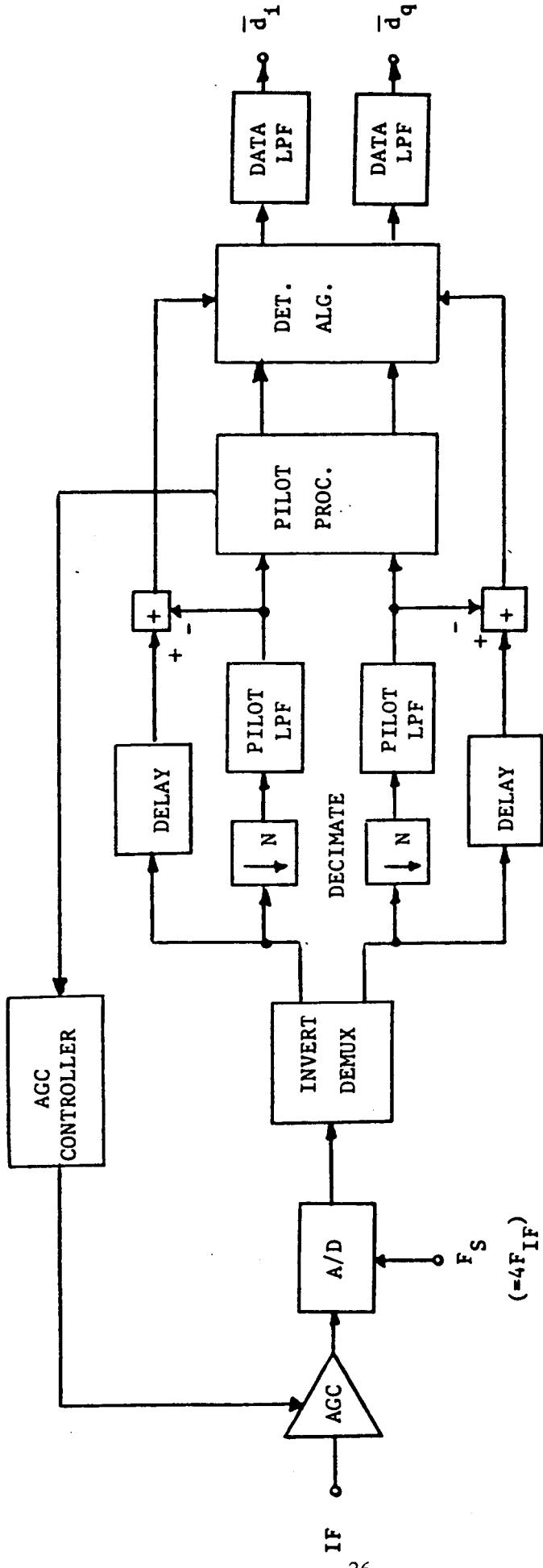


FIGURE 3.5 DIGITAL MTCT DEMODULATOR

The results of the simulated demodulator output are compared with respect to two performance criteria : recovered pilot quality and data eye quality. Two different pilot recovery filters were used with 3 dB cut-off frequencies representing maximum desired pilot bandwidth, 150 Hz, and minimum usable bandwidth, 80 Hz. The filter characteristics are summarized in table 3.1. The transmitted pilot level is 0.5 and the nominal eye opening is 2.0.

Figure 3.6(a) shows the recovered pilot using the 150 Hz lowpass filter without the benefit of a highpass filter on the transmit end. The large variation from the transmitted level is due solely to data modulation of the pilot. If the pilot of Figure 3.7(a) is compared to this one, a significant decrease in variance is observed. Although data energy continues to leak into the pilot recovery channel, the amount is greatly reduced at the transmit side by the Manchester encoding. The large reduction in pilot variance suggests that there is little data energy remaining in the frequency band below 80 Hz.

Figures 3.6(b) and 3.7(b) show the eye diagrams corresponding to the recovered pilots. Both show the ISI introduced by the demodulator at the detection algorithm. The eye pattern generated from the system employing the 150 Hz recovery filter is particularly bad due to the large data modulation induced variance.

With the addition of a transmit highpass filter, the demodulator recovered pilots more closely approach the transmitted levels. Figure 3.8(a) shows the pilot obtained with the 150 Hz recovery filter and Figure 3.9(a) shows the pilot recovered through the 80 Hz lowpass filter. Both pilots exhibit considerable improvement due to the inclusion of the highpass filter.

The respective data eye patterns are shown in Figures 3.8(b) and 3.9(b). A comparison between the detected eye diagram obtained with the 80 Hz recovery filter and the transmitted data eyes of Figures 3.2(a) and 3.3(a) indicates negligible distortion introduced by the demodulator.

A configuration which was not simulated but potentially results in reduced ISI at the demodulator consists of transmit highpass filtering at a frequency of 80 Hz and also employing an 80 Hz pilot recovery filter. This

TABLE 3.1
PILOT RECOVERY FILTER CHARACTERISTICS

150 Hz Pilot Recovery Filter:

3 dB bandwidth	150 Hz
40 dB bandwidth	300 Hz
passband ripple	0.1 dB
sampling frequency	4.8 kHz

80 Hz Pilot Recovery Filter:

3 dB bandwidth	80 Hz
40 dB bandwidth	160 Hz
passband ripple	0.1 dB
sampling frequency	4.8 kHz

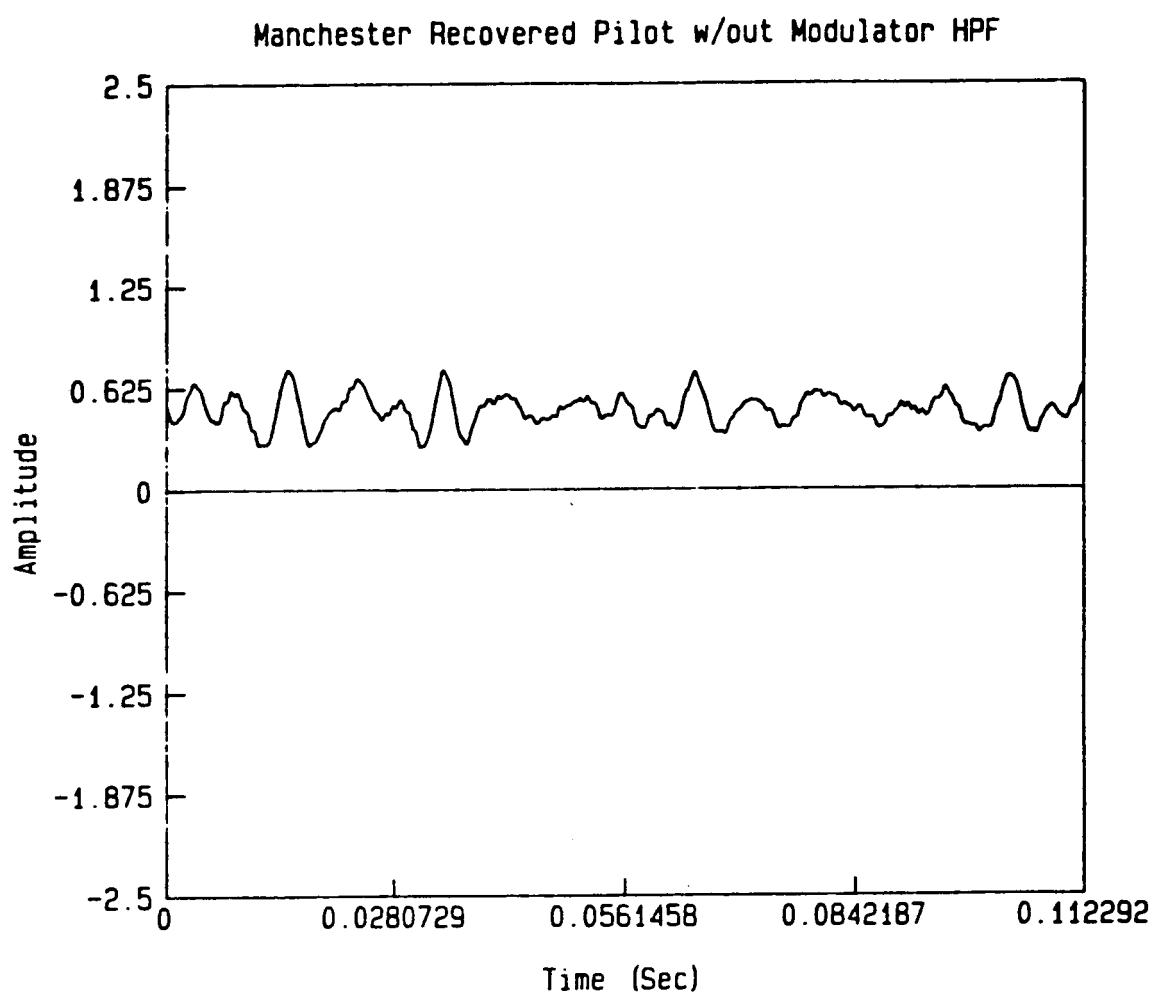


FIGURE 3.6 (a) MTCT RECOVERED PILOT, 150 HZ PILOT
LOWPASS FILTER, NO TRANSMIT HIGHPASS FILTER

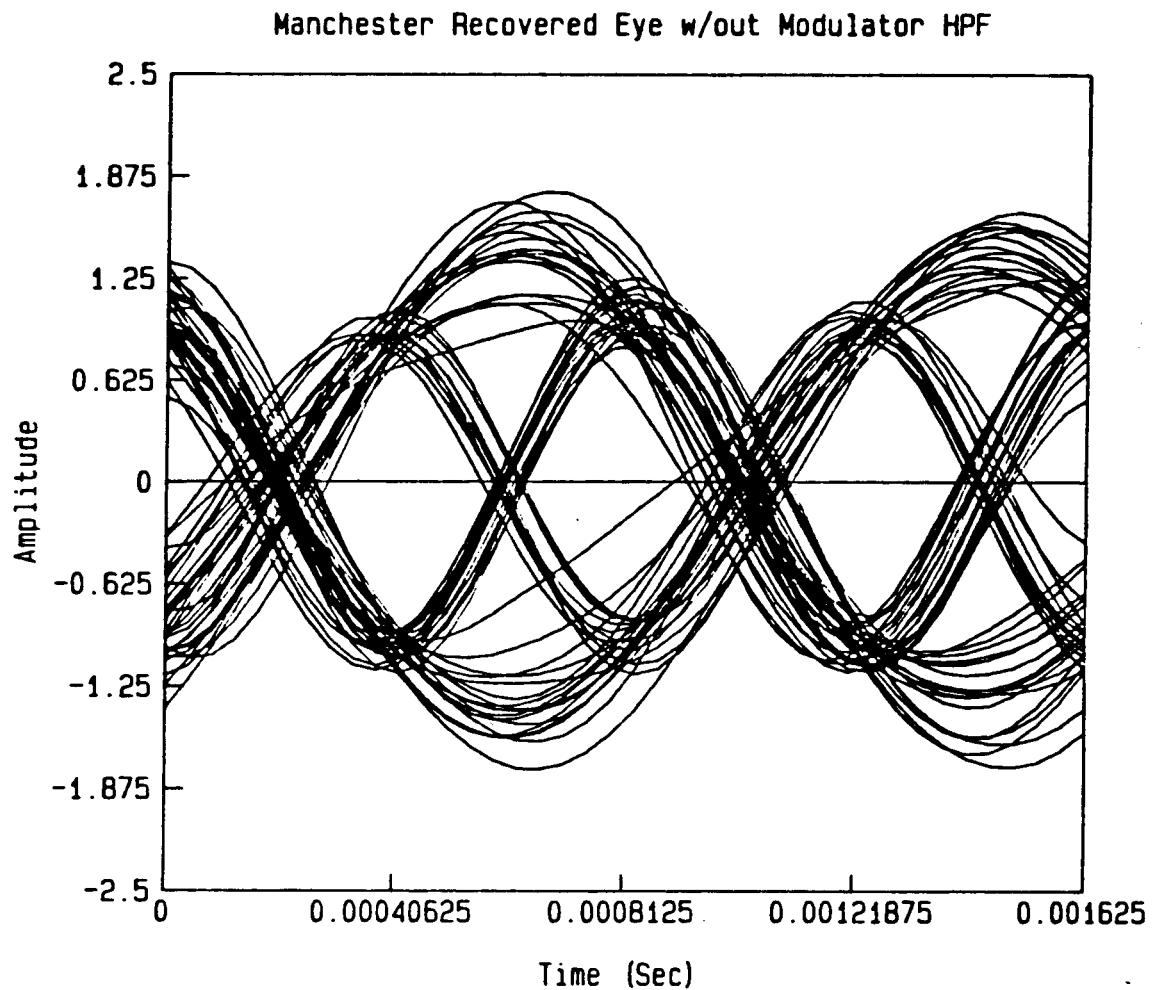


FIGURE 3.6 (b) MTCT RECOVERED EYE FOR THE PILOT OF

FIGURE 3.6 (a)

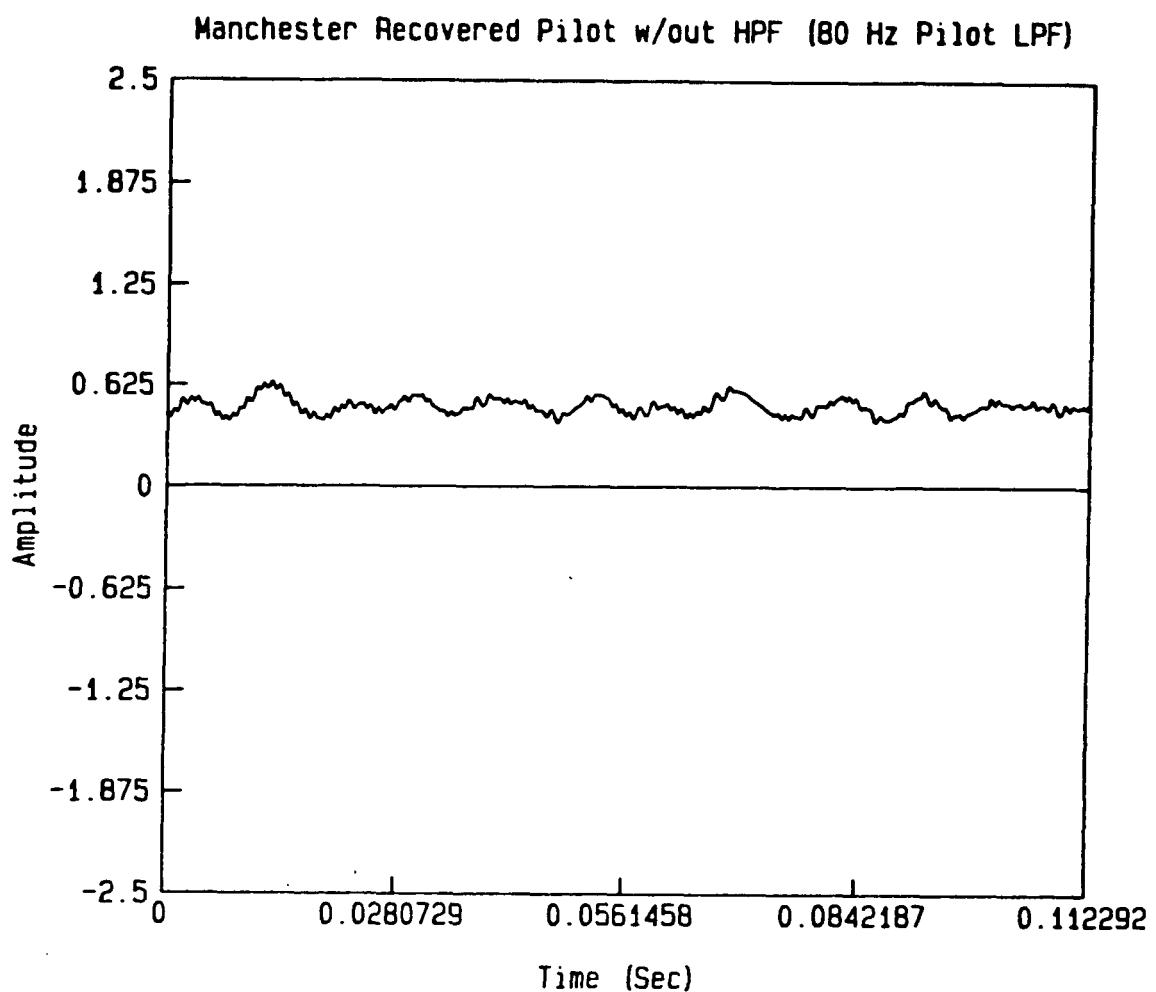


FIGURE 3.7 (a) MTCT RECOVERED PILOT, 80 HZ PILOT LOWPASS FILTER, NO TRANSMIT HIGHPASS FILTER

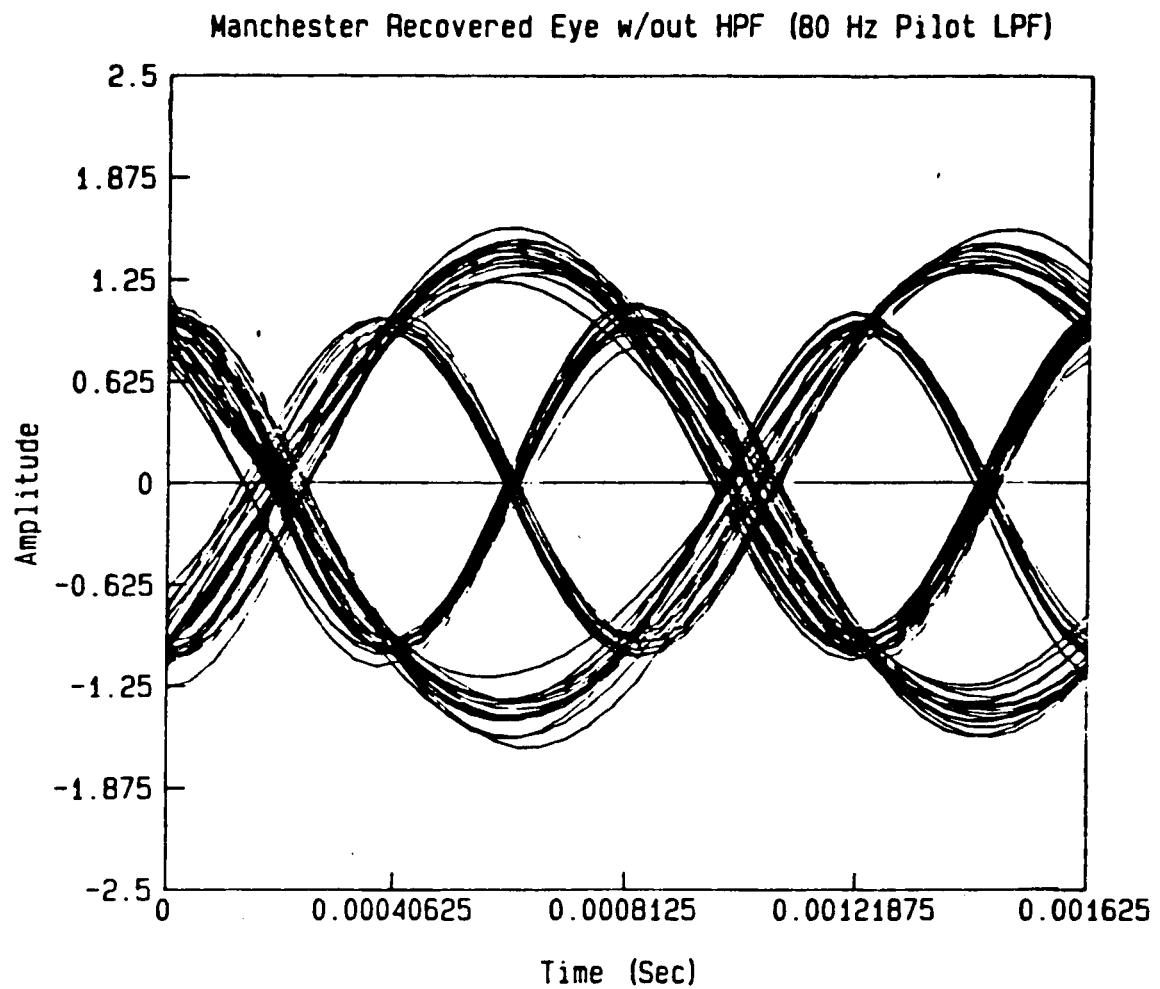


FIGURE 3.7 (b) MTCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.7 (a)

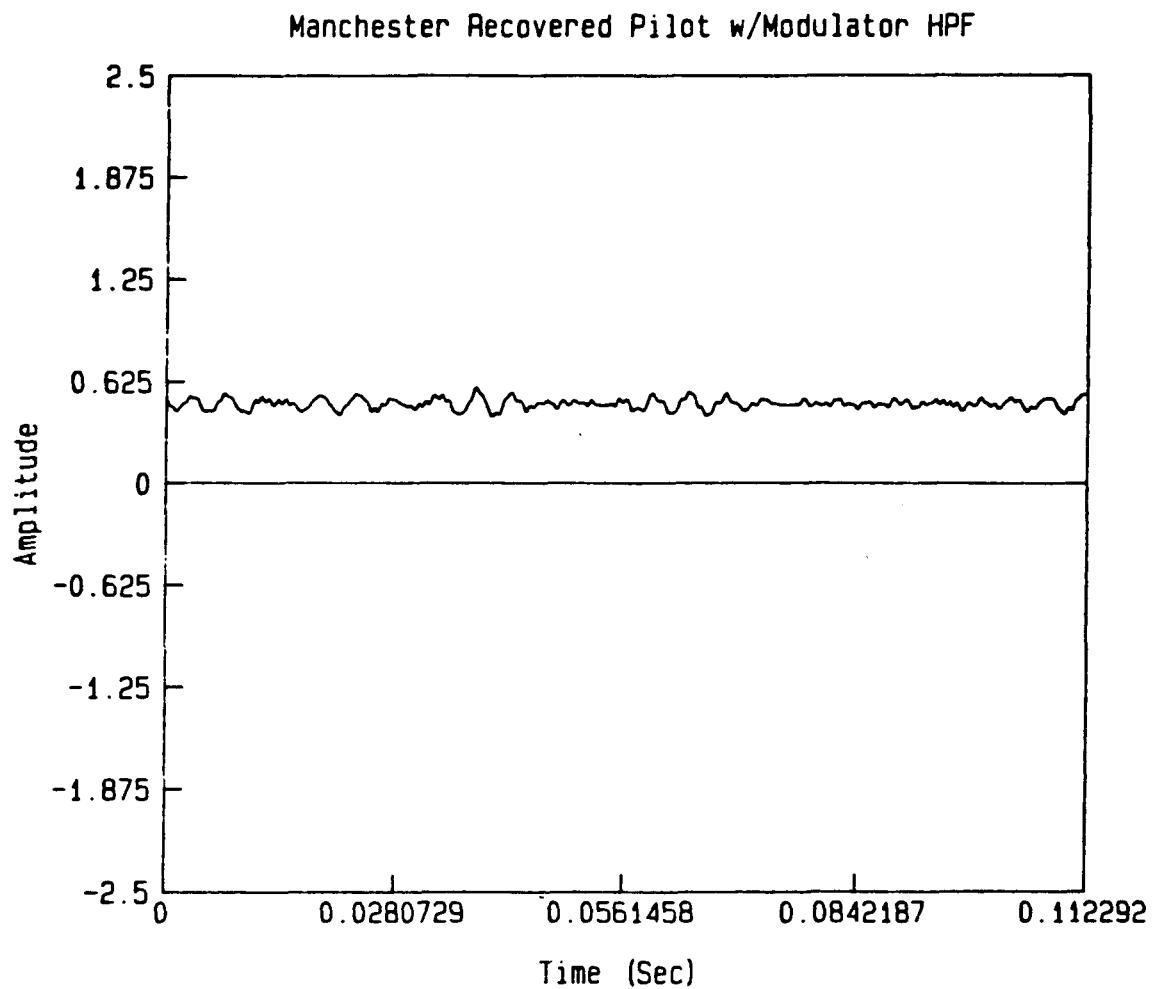


FIGURE 3.8(a) MTCT RECOVERED PILOT, 150 HZ LOWPASS FILTER AND
TRANSMIT HIGHPASS FILTER

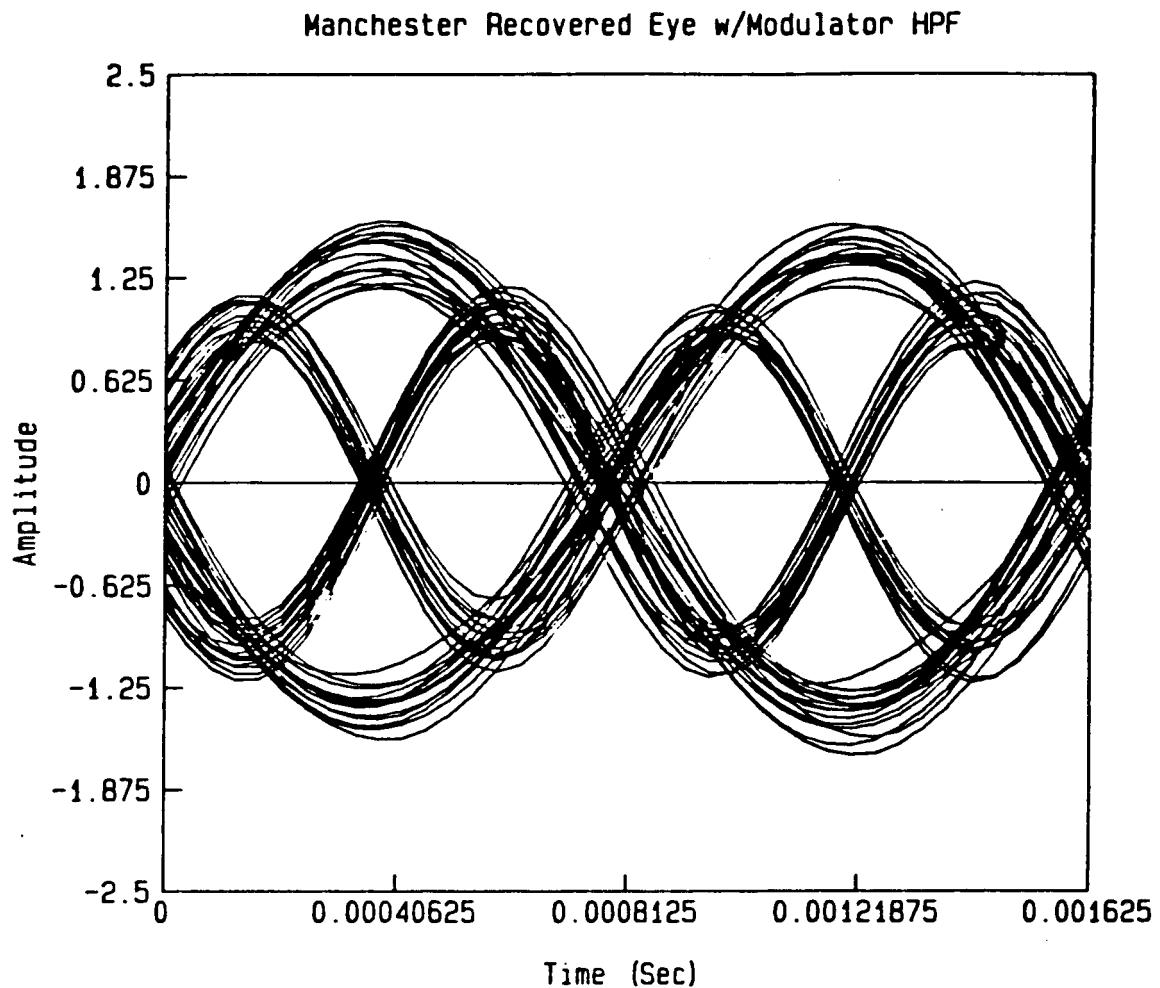


FIGURE 3.8 (b) MTCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.8 (a)

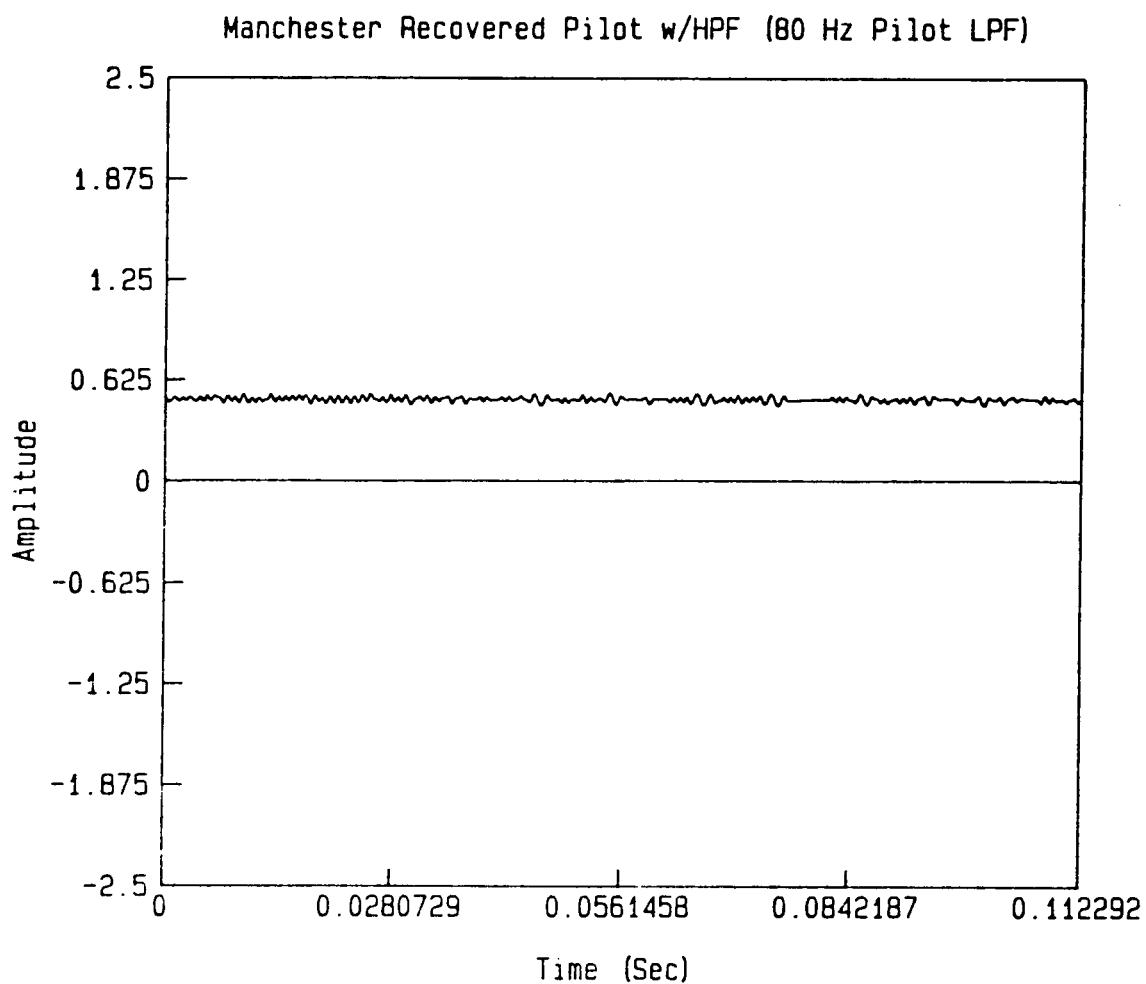


FIGURE 3.9(a) MTCT RECOVERED PILOT, 80 HZ LOWPASS FILTER AND HIGHPASS TRANSMIT FILTER

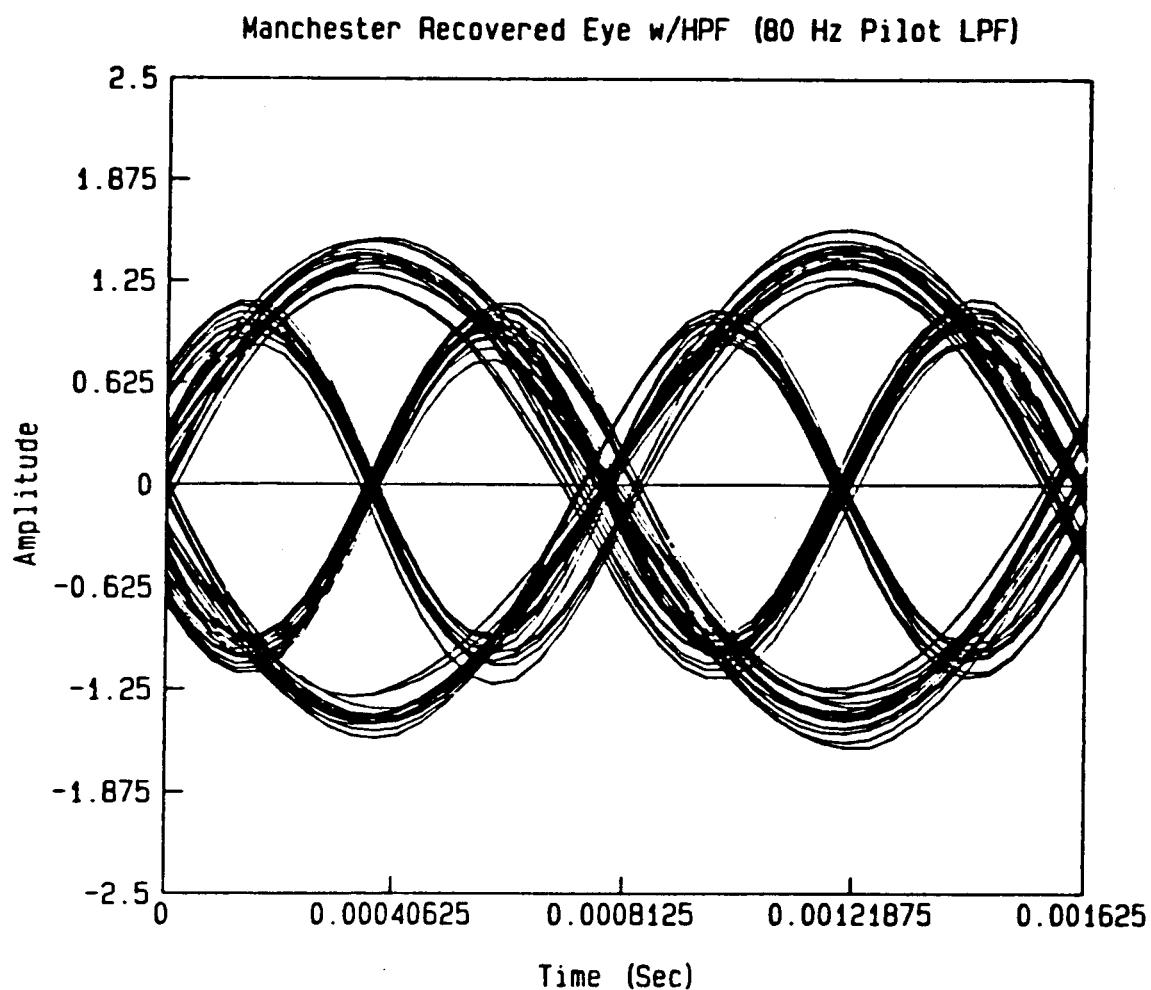


FIGURE 3.9(b) MTCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.9(a)

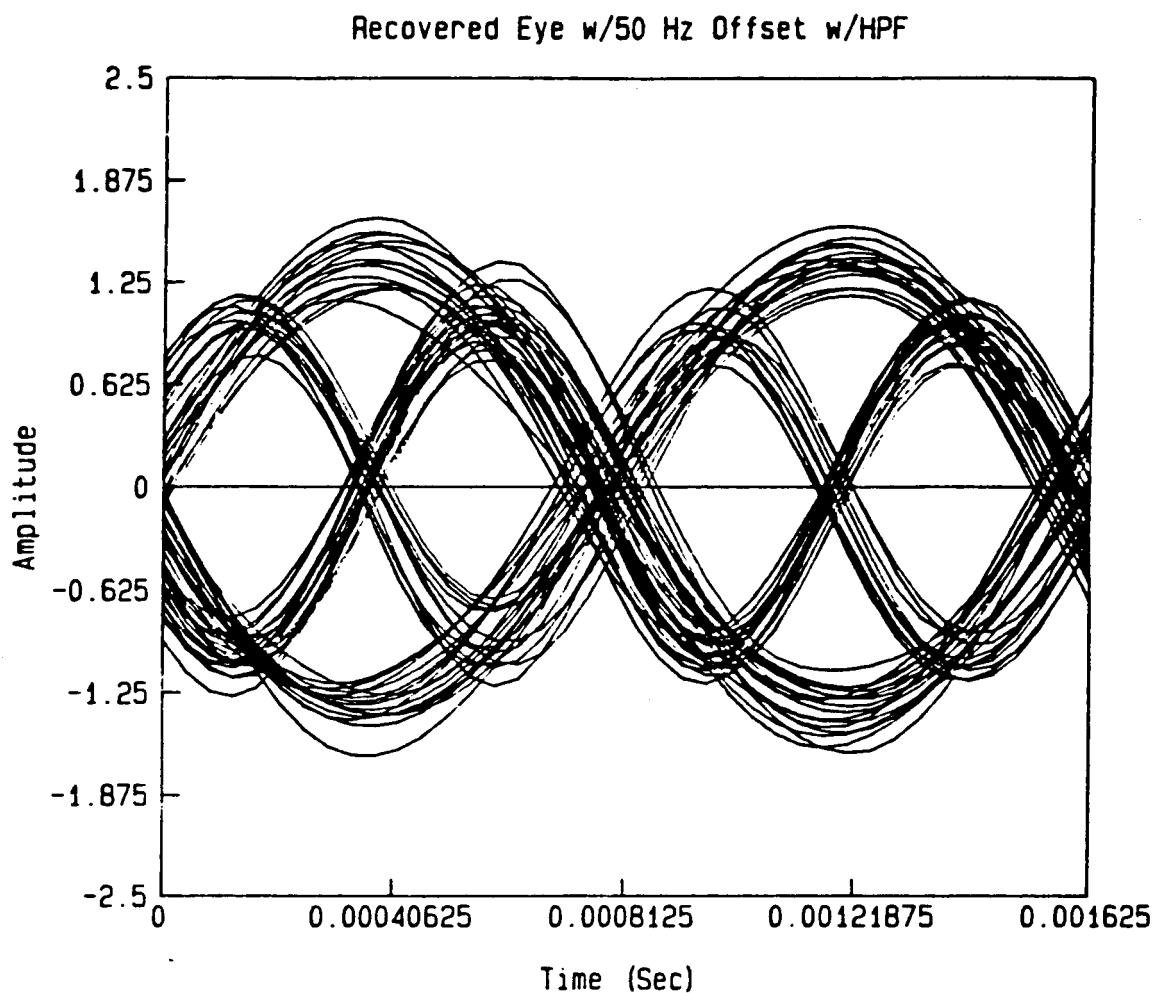


FIGURE 3.10(a) MTCT RECOVERED EYE FOR A 50 HZ FREQUENCY OFFSET AND
A 150 HZ PILOT LOWPASS FILTER

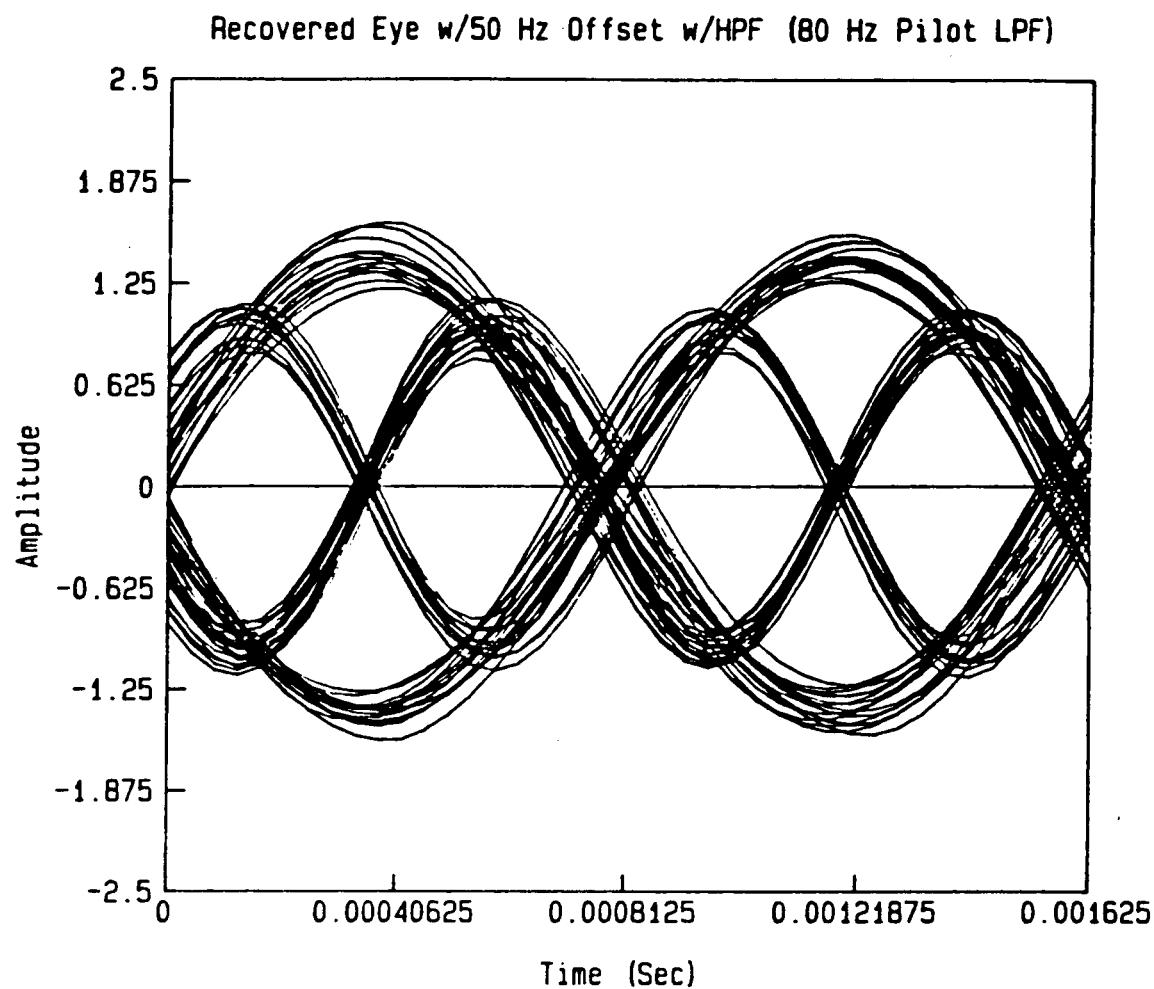


FIGURE 3.10(b) MTCT RECOVERED EYE FOR A 50 HZ FREQUENCY OFFSET AND AN 80 HZ LOWPASS FILTER

would result in a recovered pilot with slightly more variance than the one of Figure 3.9(a); however, the data eye should display less ISI since a significant part of the data spectrum (80-150 Hz) is left intact.

The demodulator performance was also examined after introducing a 50 Hz frequency offset to the modulated signal. Figures 3.10(a-b) show the detected data eyes obtained with the 150 Hz and 80 Hz lowpass filters respectively. The performance exhibited by the MTCT configuration indicates the ability to correct for a considerable frequency displacement.

3.2 Subcarrier TCT

3.2.1 Modulator

As an alternative to the MTCT transmitter, the STCT modulator of Figure 2.4 was fully simulated. The STCT modulator relies on the subcarrier modulation to create the spectral null for pilot insertion; therefore, its design is considerably simplified by omitting both the Manchester encoding and the highpass filters. Frequency domain raised-cosine pulse shaping is again used in the STCT system. An excess bandwidth fraction of 0.4 is employed for pulse shaping and a 960 Hz subcarrier, for QPSK modulation in order to meet the single-sided spectral occupancy requirement of a 40 dB attenuation at 1.8 kHz from the center frequency. The modulator output is a 48 kHz sampled stream translated to a 12 kHz IF.

The baseband data eye is shown in Figure 3.11(a) and 3.11(b) shows the corresponding spectrum. Figure 3.12 shows both the QPSK modulated data onto the subcarrier and the spectral null. Since no energy has been removed from the data signal, unlike the MTCT system, the transmitted data is free of ISI.

3.2.2 Demodulator

The translation process from IF to baseband in the STCT demodulator was changed slightly from the one used in the MTCT system. Demodulation was achieved without a local reference by taking advantage of the fact that the data bandwidth is small in comparison to the sampling frequency. In the STCT

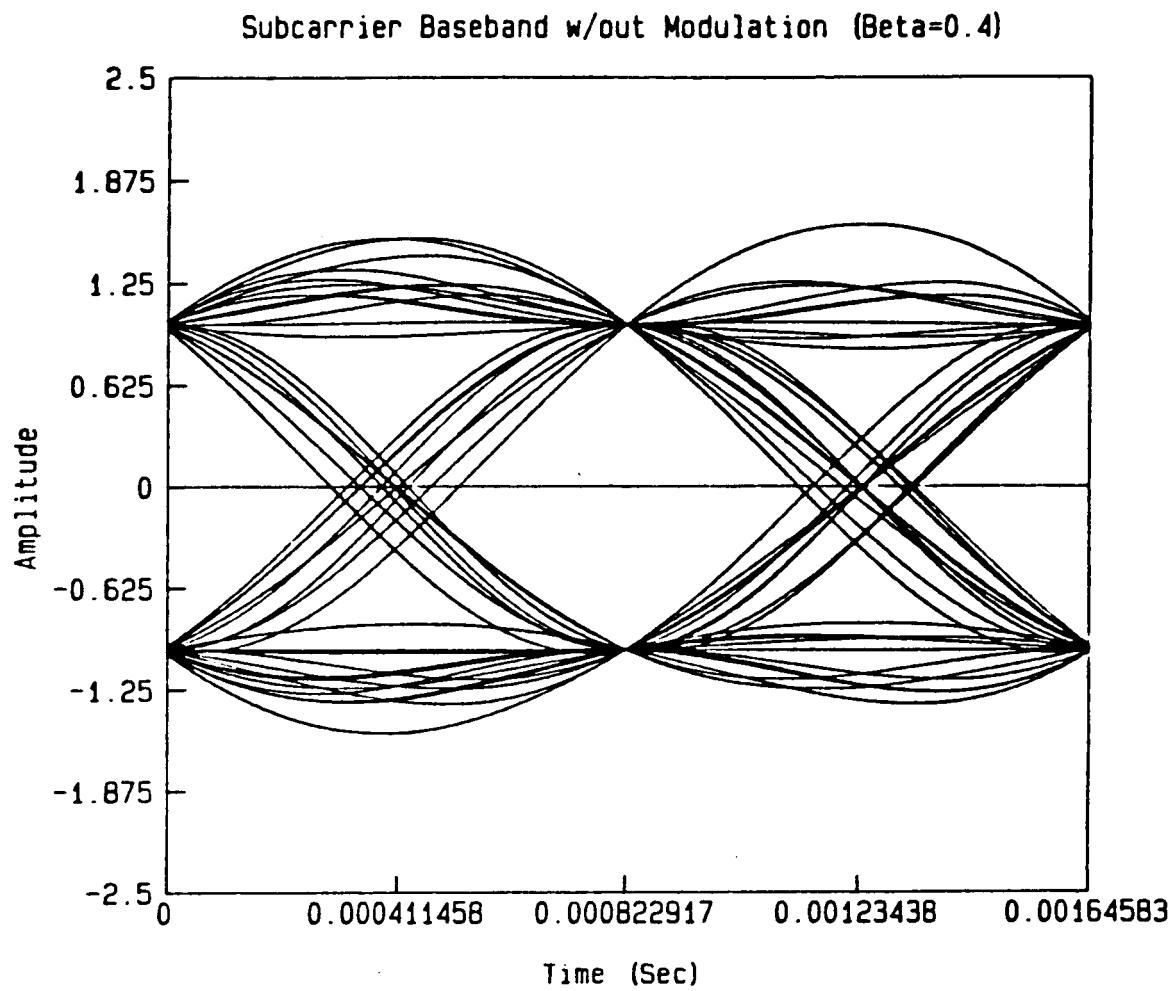


FIGURE 3.11(a) STCT TRANSMIT DATA EYE

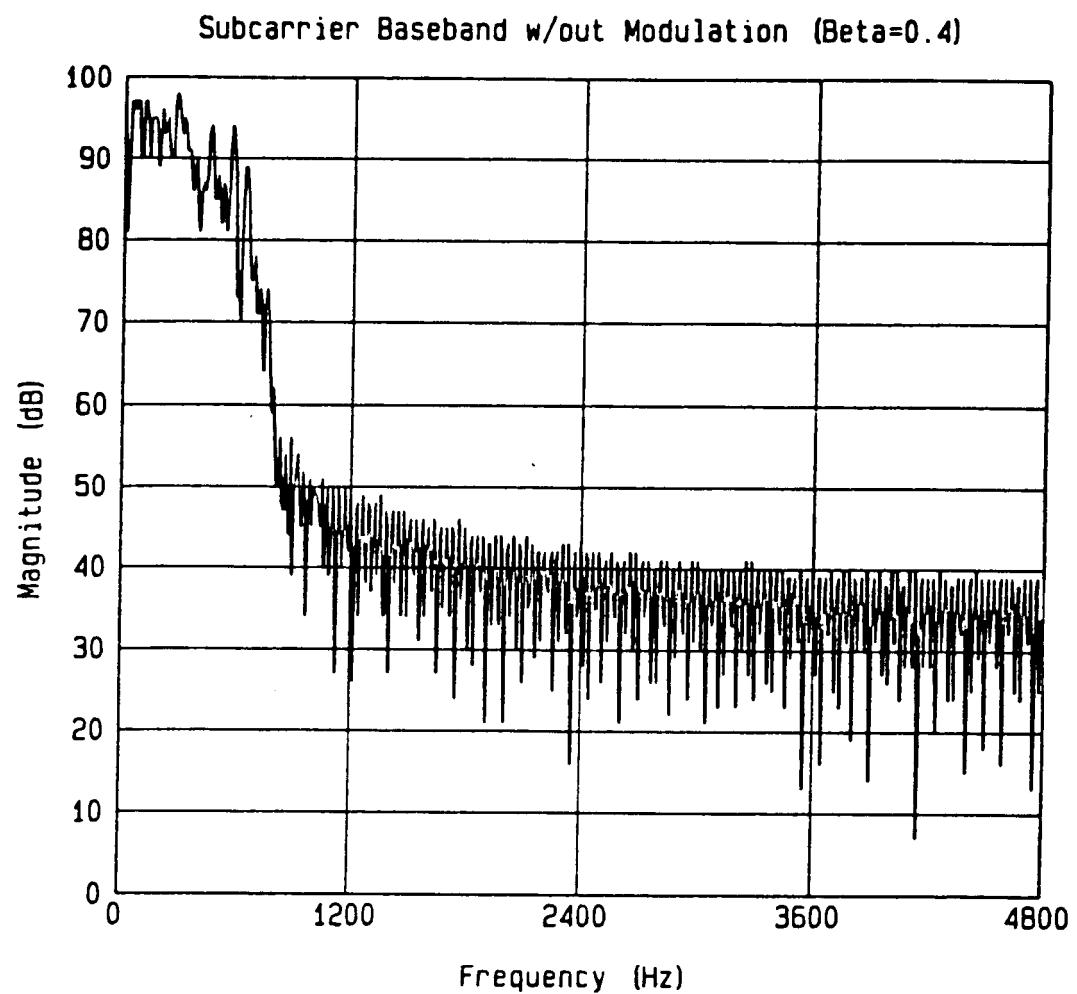


FIGURE 3.11(b) FREQUENCY SPECTRUM OF FIGURE 3.11(a)

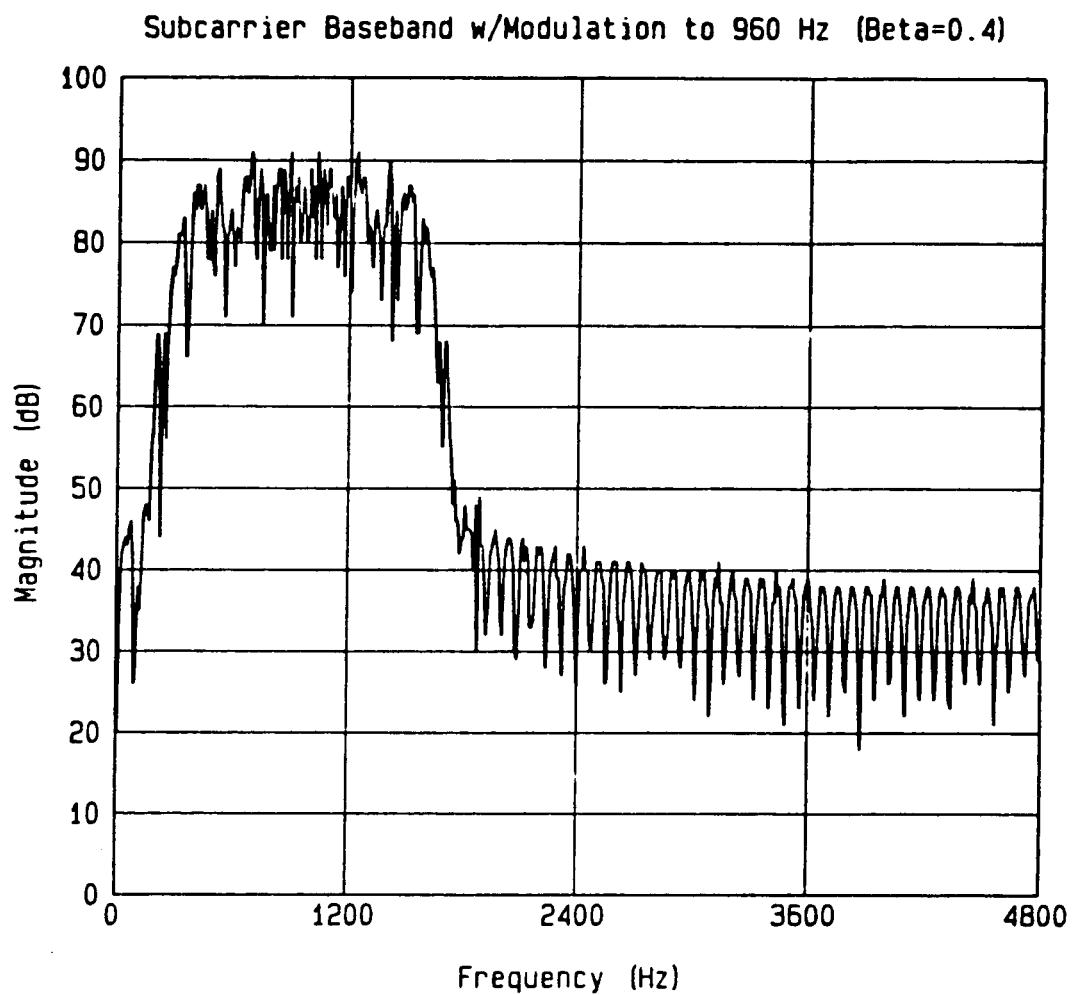


FIGURE 3.12 SUB-CARRIER QPSK FREQUENCY SPECTRUM

simulation, a ratio of 4:1 was employed and adjacent IF input sample pairs were translated to 12 kHz in-phase and quadrature baseband components. Figures 3.13(a-c) detail the demodulation process. A further decimation of 5:1 in the signal paths leading to the pilot recovery lowpass filters was used causing aliasing in the data but not in the pilot. The aliased portion of the spectrum is located in the stopband of the recovery filter and contributes no negative effects, see Figures 3.14(a-b). The final processing rates in the STCT simulation were 12 kHz for the data arms and 2.4 kHz for the pilot channels (these rates can be applied to the MTCT simulation as well).

The results of the subcarrier demodulator simulation are summarized in Figures 3.15(a-b) and 3.16. Figure 3.15(a) shows a recovered pilot with virtually no data modulation corrupting it, resulting in the corresponding recovered eye pattern of Figure 3.15(b) which shows no ISI. A frequency offset test was also performed with the subcarrier simulation. Figure 3.16 shows the recovered data eye which displays noticeable distortion. Some preliminary investigation seemed to indicate that ISI is produced by imperfect cancellation of the frequency offset double term product in the detection algorithm. The distortion introduced by this term is assumed also to be present in the MTCT demodulator.

Table 3.2 compares the recovered pilot variances for both the MTCT and STCT systems. All variances are referenced to the recovered subcarrier pilot variance level.

4. MODEM HARDWARE IMPLEMENTATION

4.1 Manchester Encoded TCT

The Manchester encoded TCT was the method chosen by JPL to be followed through to a hardware realization. Consequently, the MTCT modem is the major topic of this section. To date a stand-alone board that serves as the digital modulator for both the MTCT and STCT systems has been completed and is fully tested and functional. The required RF circuitry for the modulator and demodulator has also been designed and tested. The transmitter RF portion has

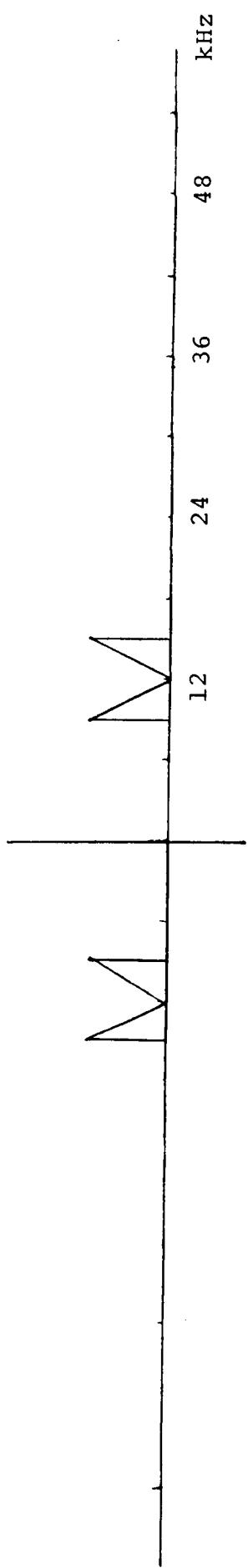


Figure 3.13(a) Analog IF Spectrum

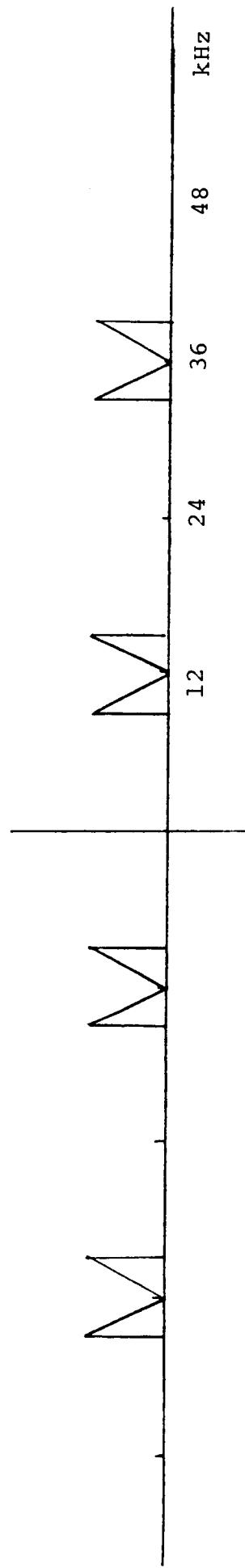


Figure 3.13(b) Spectrum Sampled at 48 kHz

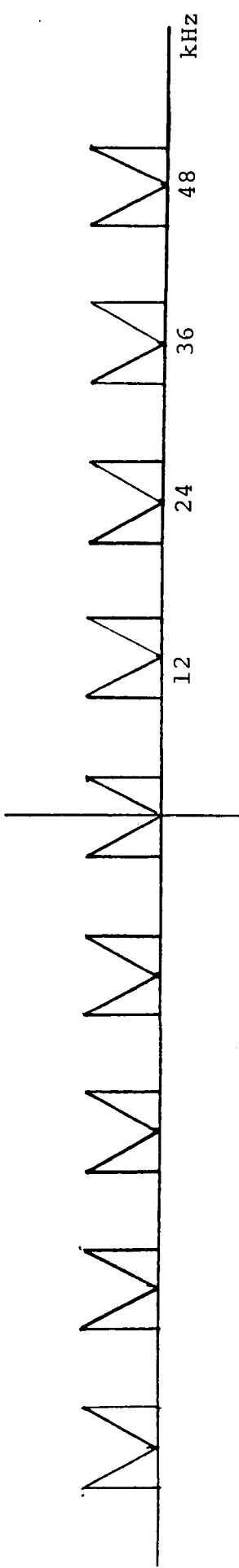


Figure 3.13(c) Demodulated Spectrum Through 4:1 Decimation

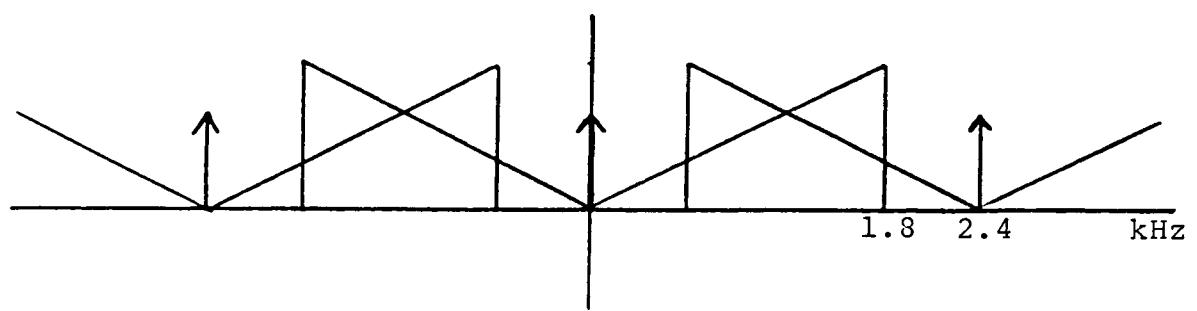


Figure 3.14(a) Aliased Baseband Spectrum

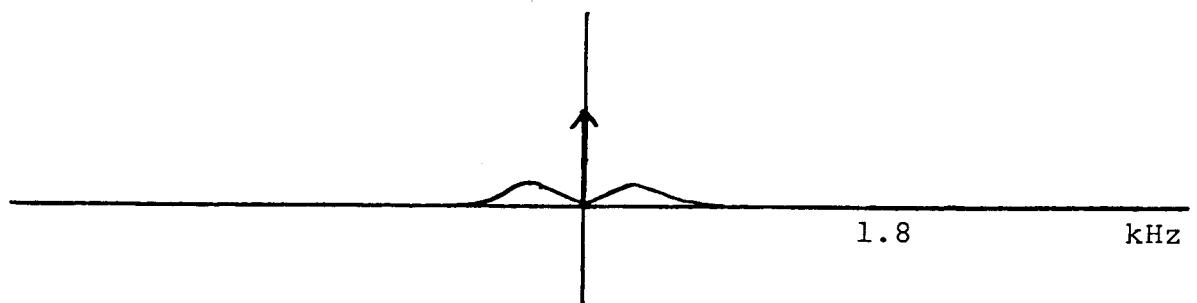


Figure 3.14(b) Recovered Pilot After Lowpass Filtering

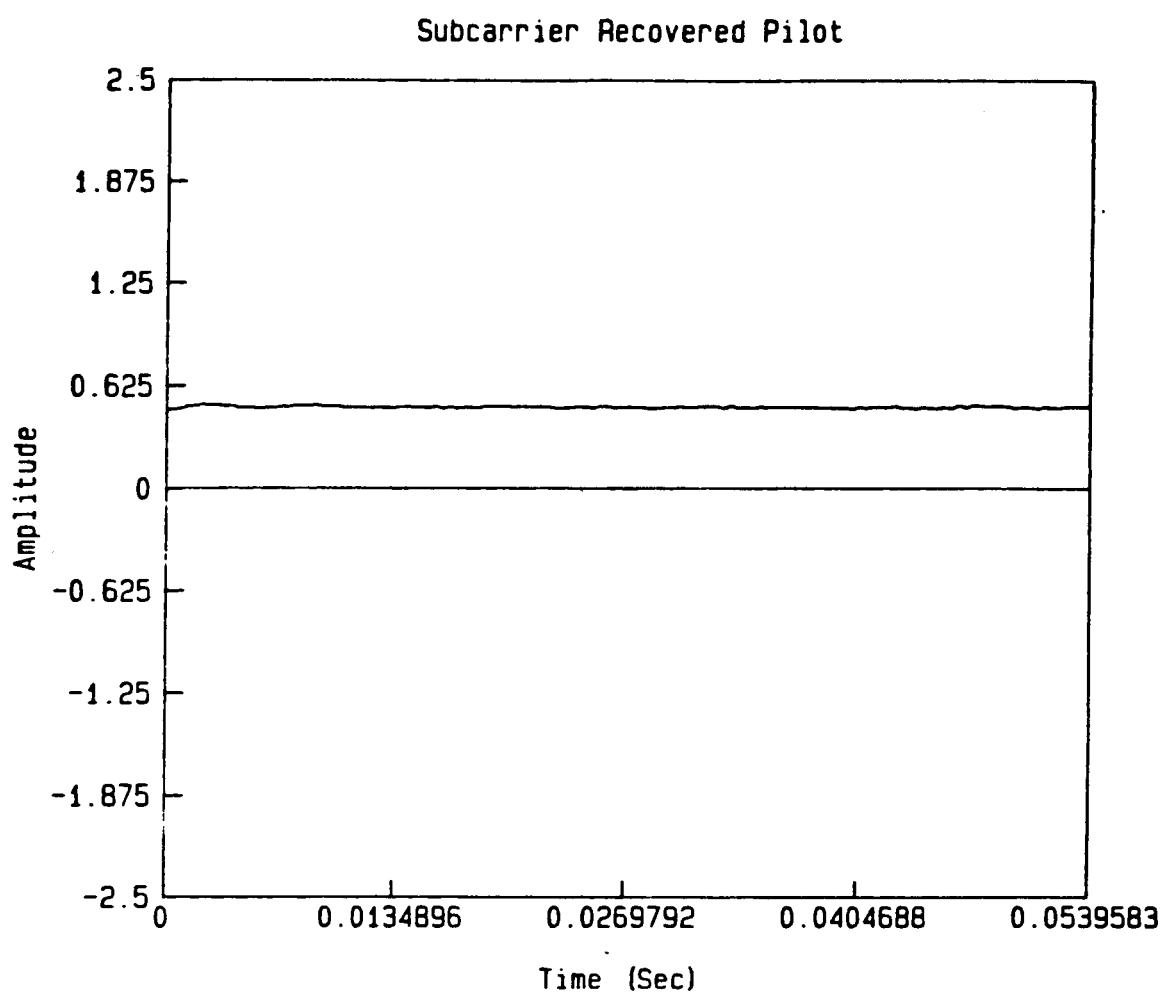


FIGURE 3.15(a) STCT RECOVERED PILOT, 150 HZ PILOT LOWPASS FILTER

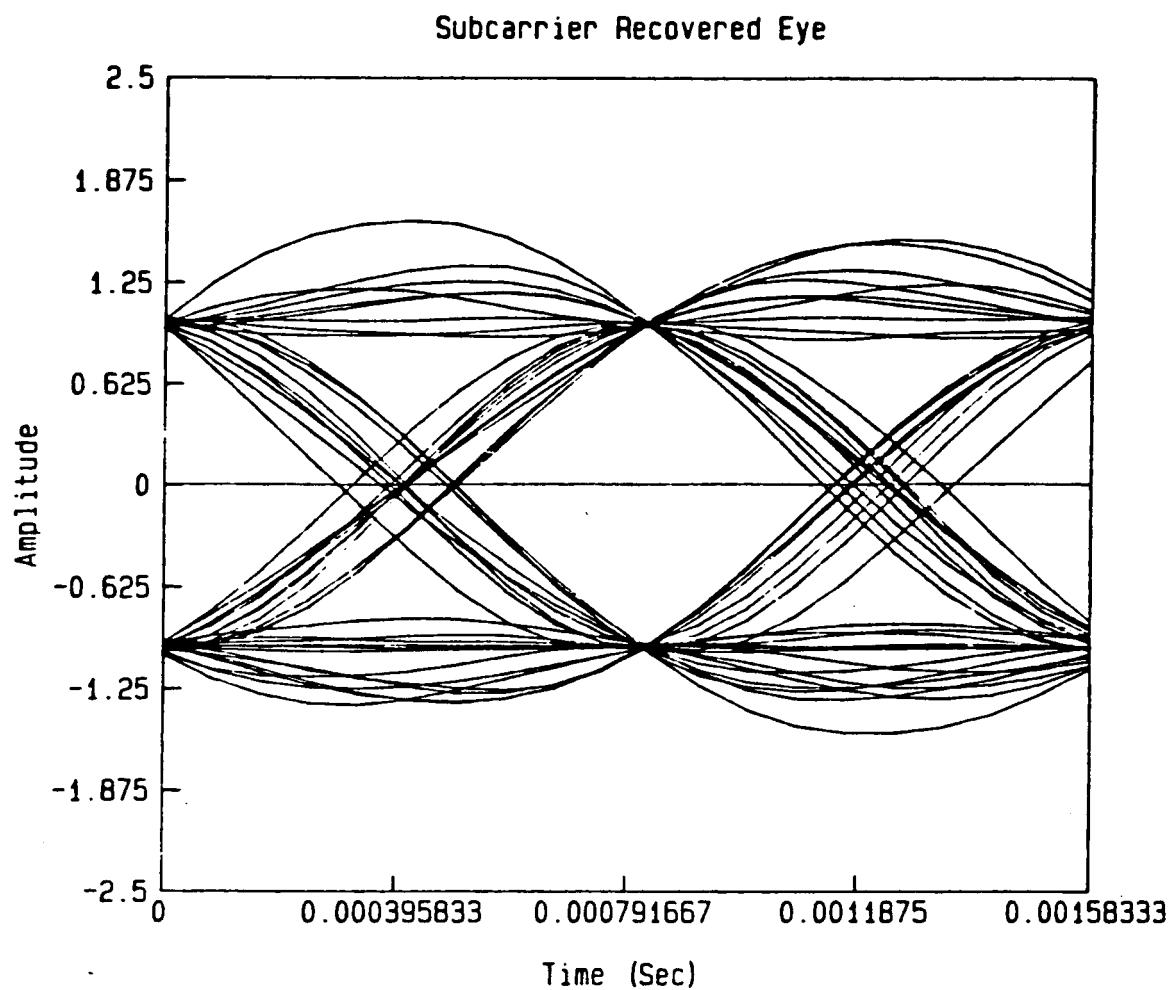


FIGURE 3.15 STCT RECOVERED EYE FOR THE PILOT OF FIGURE 3.15(b)

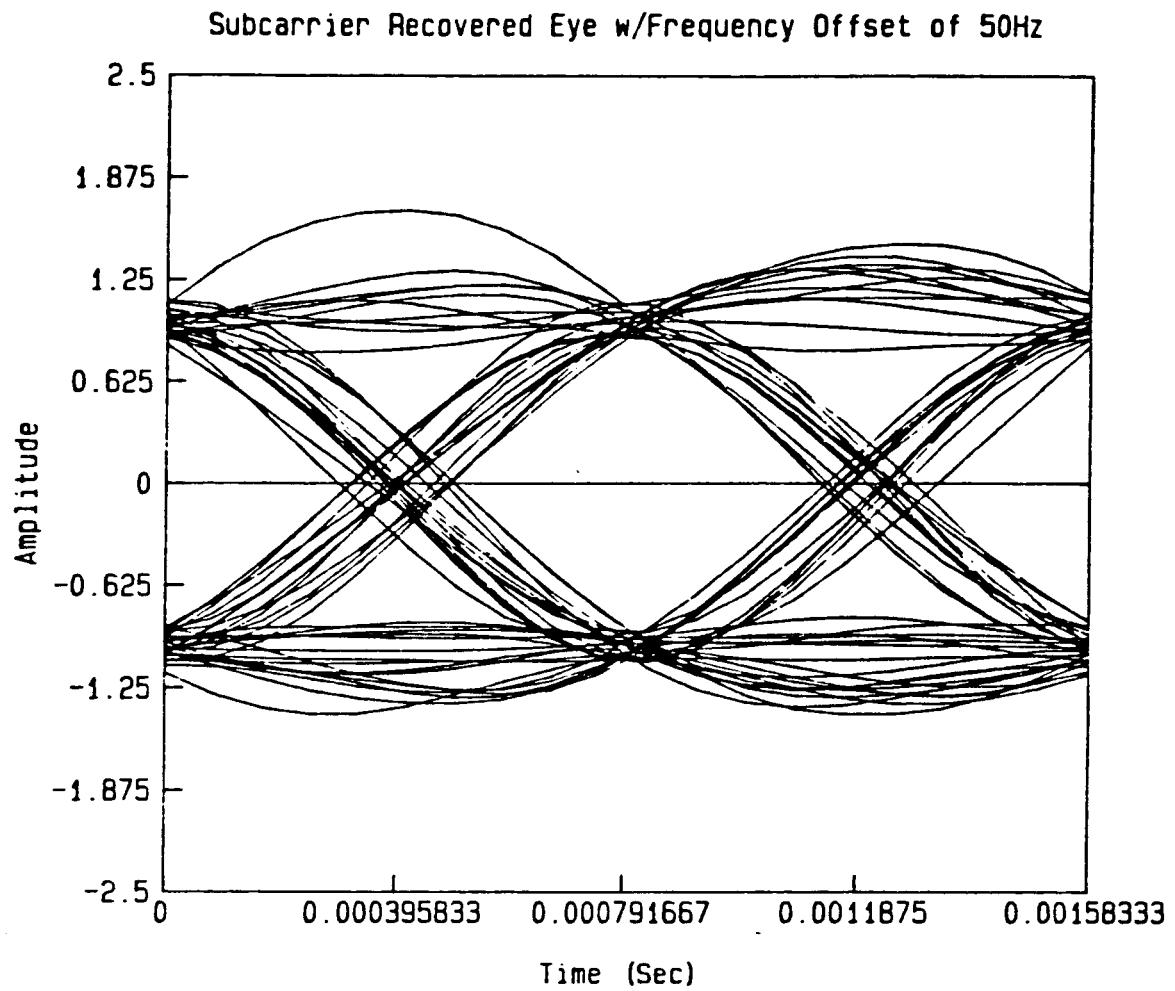


FIGURE 3.16 STCT RECOVERED EYE FOR A 50 HZ FREQUENCY OFFSET

MANCHESTER TCT

TX HPF	PILOT REC. LPF	RELATIVE PILOT LEVEL
NO	150 HZ	22.8 DB
YES	150 HZ	17.5 DB
NO	80 HZ	16.1 DB
YES	80 HZ	6.2 DB

SUB-CARRIER TCT

NO	150 HZ	0.0 DB
----	--------	--------

Table 3.2 Recovered Pilot Variances in dBs

been integrated with the stand-alone modulator board and is operative, as will be shown later. A circuit board design had been initiated for the MTCT demodulator and the TMS320 code is written, however, due to insufficient time to complete construction within the project schedule, it was decided by JPL not to follow it through to completion. The MTCT TMS320 software used in the premodulation processing is included in Appendix II.

Since the hardware implementation of the modulator was discussed previously in both the first and second interim reports, only the salient features will be presented in the following section.

4.1.1 MTCT Modulator Implementation

A block diagram of the final stand-alone digital modulator is shown in Figure 4.1. All processing tasks are performed by the Texas Instruments TMS320, the remaining components of the board are necessary for the proper function of the TMS320. The program code is held in the 2K of EPROM and is read into the 2K of RAM upon the booting of the system. In this way, a slow access time, UV erasable PROM can be used in conjunction with fast RAM to avoid usage of once-only programmable bipolar PROM. The I/O block consists of three latches which control the two system outputs and single system input. The two remaining blocks pertain to the control timing of the processing. The Master Timing block includes a 20 MHz clock for the TMS32010 processor chip, while the other I/O timer strobes the TMS320 at a rate of 9.6 kHz., indicating that it is time for the system to release an inphase and quadrature sample pair to the QPSK modulator. Also, on every fourth set of outputs, a new data bit is read in.

The details of the modulator code were presented in the First Interim report [1] and will only be briefly summarized here. The TMS320 accepts a binary input at a rate of 2.4 kbps. These input bits are split into even and odd data streams prior to Manchester encoding. Encoding is performed only after two data bits have been input which has the effect of synchronizing the inphase and quadrature streams. The next step in the modulation process is to shape these encoded bits.

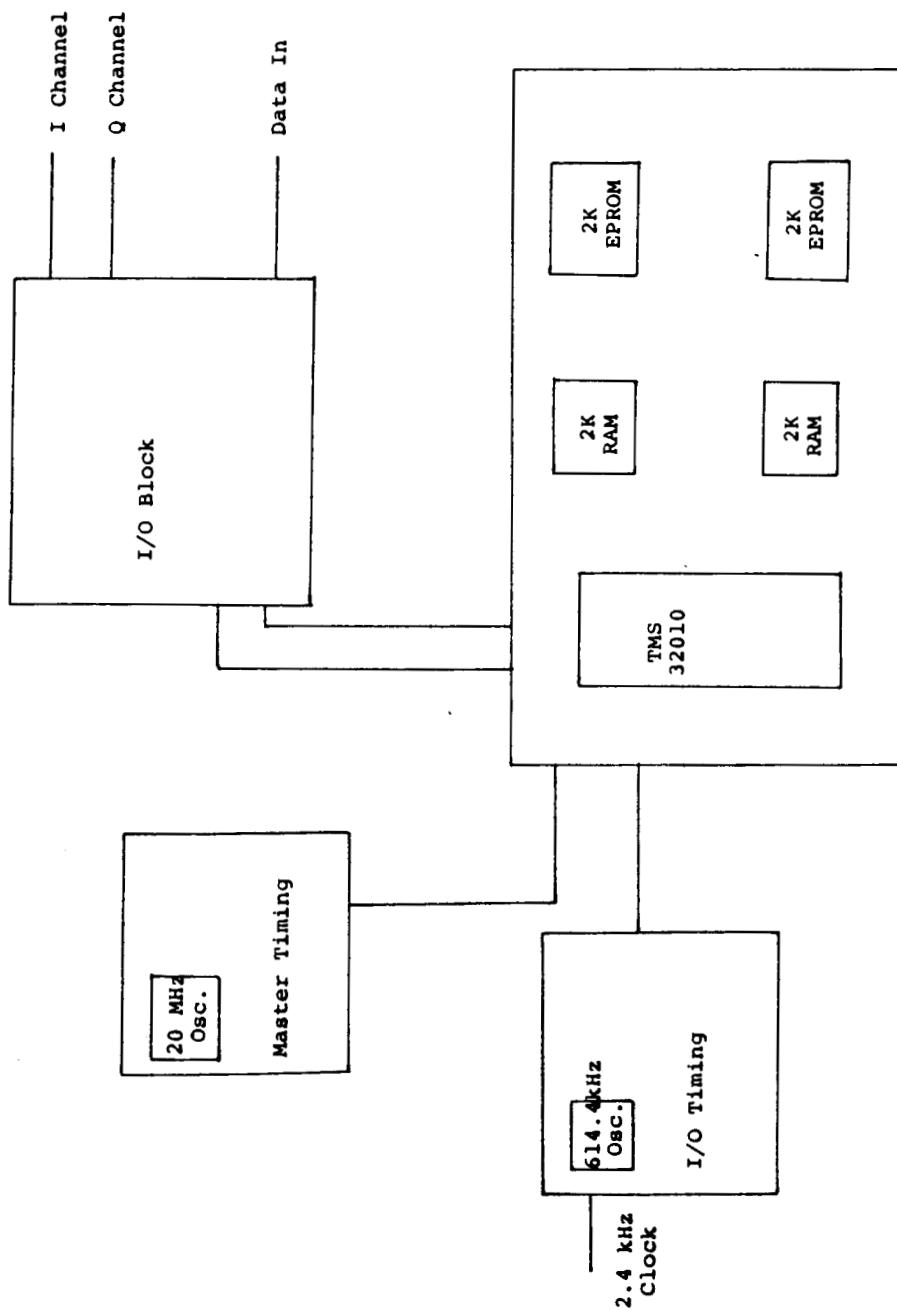


FIGURE 4.1 MTCT MODULATOR BOARD CONFIGURATION

The pulse-shaping chosen for implementation is the raised-cosine shape with an excess bandwidth fraction, β , of 0.5, as discussed in section 2.1. The raised-cosine pulse-shape is truncated such that it spans eight Manchester encoded data bits and is represented digitally by four evenly spaced samples per bit, for a total of thirty-two samples per pulse waveform. As will be shown presently, this representation of the raised-cosine pulse is sufficient to produce a transmit data 'eye' of the desired quality and spectral occupancy.

These thirty-two pulse-shape coefficients are stored in ROM and listed in Table 4.1. This table includes both the actual values of the coefficients as well as the scaled values used in the TMS320 implementation. The encoded data bits are pulse-shaped by simply multiplying these coefficients by the code bit in question. Therefore, a +1 is represented by the thirty-two coefficients that appear in Table 4.1, a -1 by their inverse. At any point in time, the output of the pulse-shaping section is simply the sum of the samples from all waveshapes that are non-zero at that instant in time. Due to the truncation of the pulse-shape, only the waveforms representing the eight most recent Manchester bits are non-zero and, hence, taken into consideration. Since there are four samples of the pulse-shape per Manchester bit period, there will be four outputs per I/Q stream from the processor chip per Manchester bit. The inphase and quadrature shaping is identical and operates independently on the separated even and odd data bit streams. Hence the I and Q shaping can be represented by the general equation:

$$s(t_i + j) = \sum_{n=t_i-7}^{t_i} cb_n * P(4(n-t_i + 8) + j) \quad j = 1,2,3,4 \quad (4.1)$$

where t_i is the time index of the most recent Manchester bit, cb_n refers to the encoded data bits (even or odd), the index j is an output pointer which indicates which of the four outputs for this particular set of code bits is under consideration, and the $P(.)$ terms are the raised-cosine pulse-shape samples listed in table 4.1. After all four output samples have been generated, a new code bit enters into play, and the oldest bit of the last nine is

Table 4.1
Pulse Shaping Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
P(1) = P(32)	.00219	36
P(2) = P(31)	.00555	91
P(3) = P(30)	.00464	76
P(4) = P(29)	.000867	14
P(5) = P(28)	.00114	19
P(6) = P(27)	.01056	173
P(7) = P(26)	.0221	363
P(8) = P(25)	.01599	262
P(9) = P(24)	-.02533	-415
P(10) = P(23)	-.09172	-1503
P(11) = P(22)	-.1334	-2186
P(12) = P(21)	-.07953	-1303
P(13) = P(20)	.1159	1899
P(14) = P(19)	.4289	7028
P(15) = P(18)	.7587	12431
P(16) = P(17)	.9709	15908

discarded. Figure 4.2(a) shows the resulting eye diagram after Manchester encoding and raised-cosine pulse shaping. Note that at the sampling instants there is no intersymbol interference. Figure 4.2(b) shows the shaped spectrum corresponding to the eye diagram of Figure 4.2(a). Observe that, due to the addition of the Manchester coding, a shallow notch in the spectrum has appeared at d.c. In the next section of the modulator, this notch will be enlarged to facilitate pilot insertion and pilot processing at the receiver.

After the pulse-shaping has been completed, the shaped I and Q streams are sent on to be highpass filtered. This is done to accentuate the notch at d.c., which was initialized by the Manchester coding. Two FIR highpass filters were considered for implementation: one with 91 taps and the other with 45. Close inspection of the resulting eye diagrams and spectra indicated that the 45 tap filter was sufficient for the desired purposes and was implementable within the DSP chip. The actual and scaled values of the 45 tap weights used in the TMS320 implementation are listed in table 4.2. The filter design specifications used in the computer-aided design of this filter are as follows:

Stopband:	0 to 100 Hz
Passband:	≥ 250 Hz
3 dB Point:	150 Hz
0.5 dB Ripple:	≥ 250 Hz
20 dB Attenuation at d.c.	

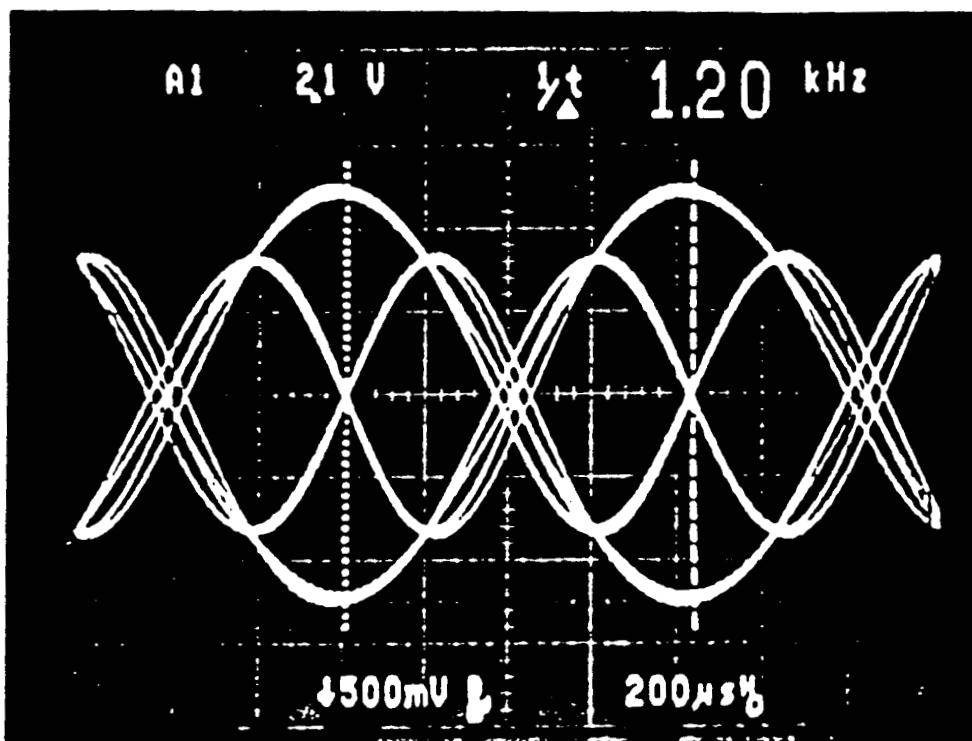
Linear Phase Response

The impulse response of the TMS320 version of this high pass filter is shown in Figure 4.3.

The pre-modulation processor output can be represented by the following constant coefficient difference equation:

$$x(k) = \sum_{\ell=0}^{44} s_k z^{-\ell} H(\ell) \quad (4.2)$$

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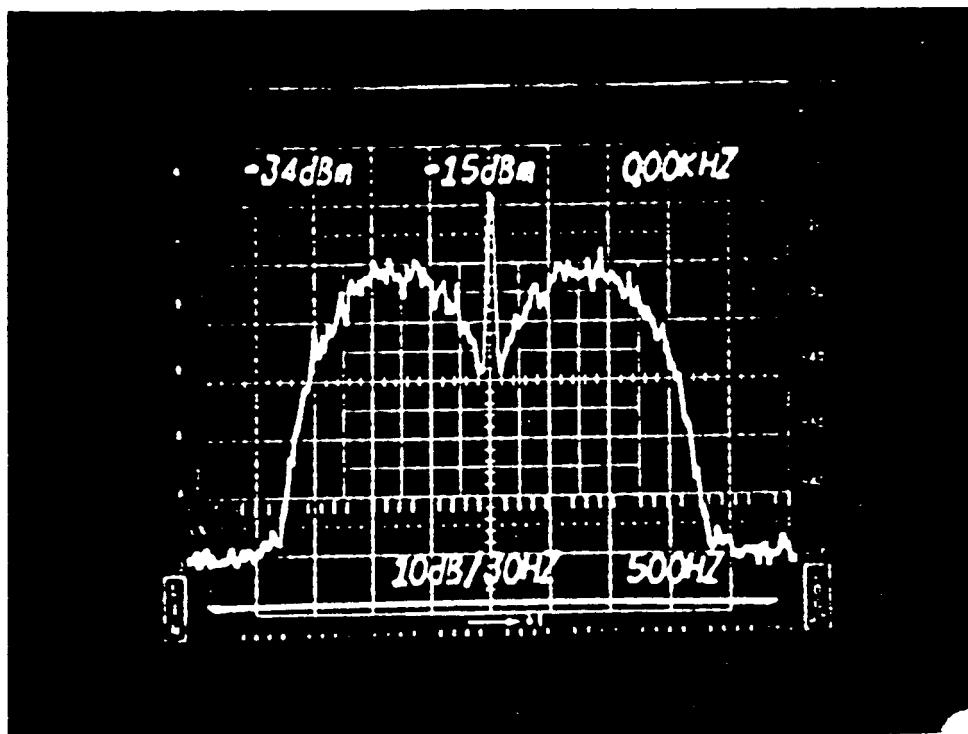


EYE DIAGRAM - 1.2 kbps

MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,
8-BIT DAC, BETA = 0.5

FIGURE 4.2(a)

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PULSE SHAPED SPECTRUM - 1.2 kbps

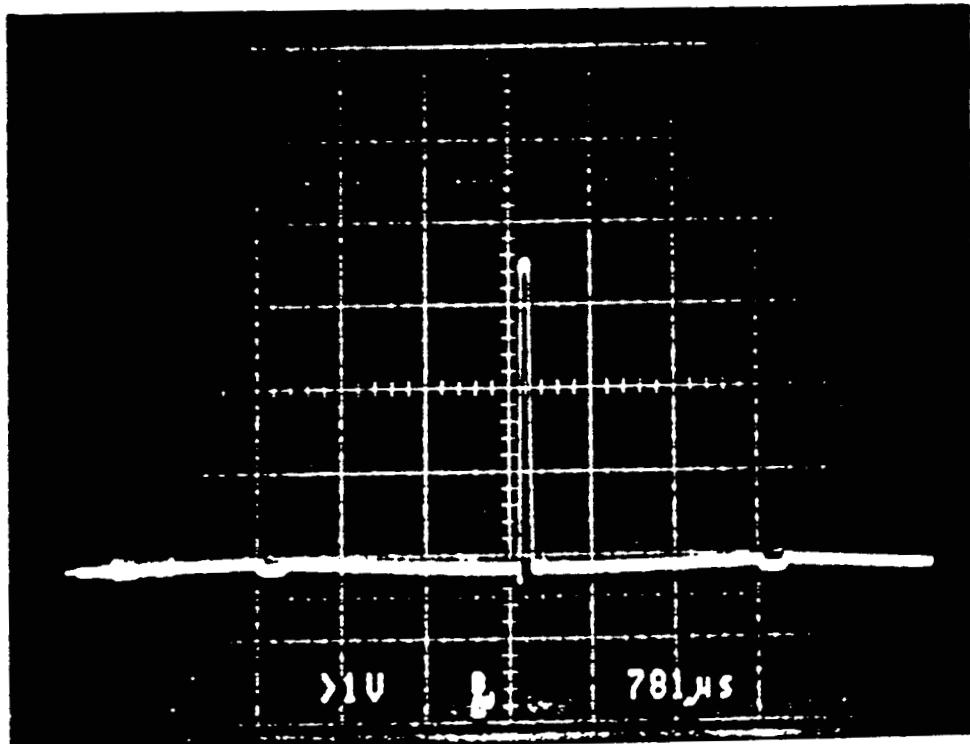
MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,
8-BIT DAC, BETA = 0.5

FIGURE 4.2 (b)

Table 4.2
Tap Weights - 45 Order Filter

	<u>Actual Value</u>	<u>Scaled Value</u>
H(0) = H(44)	-.0281	-115
H(1) = H(43)	-.0083	-34
H(2) = H(42)	-.0094	-39
H(3) = H(41)	-.0106	-43
H(4) = H(40)	-.0118	-48
H(5) = H(39)	-.0130	-53
H(6) = H(38)	-.0142	-58
H(7) = H(37)	-.0155	-63
H(8) = H(36)	-.0167	-68
H(9) = H(35)	-.0179	-73
H(10) = H(34)	-.0191	-78
H(11) = H(33)	-.0202	-83
H(12) = H(32)	-.0213	-87
H(13) = H(31)	-.0223	-92
H(14) = H(30)	-.0232	-95
H(15) = H(29)	-.0241	-99
H(16) = H(28)	-.0249	-102
H(17) = H(27)	-.0255	-104
H(18) = H(26)	-.0261	-107
H(19) = H(25)	-.0265	-109
H(20) = H(24)	-.0268	-110
H(21) = H(23)	-.0270	-111
H(22)	.9829	3985

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IMPULSE RESPONSE
45 TAP HIGH PASS FILTER

FIGURE 4.3

where $x(k)$ is the system output, $s_k = s(t_i + j)$ are the shaped samples from equation 4.1, and the $H(\text{script1})$ terms are the high pass filter coefficients listed in Table 4.2. Highpass filtered inphase and quadrature samples are output simultaneously at a rate of 9.6 ksps. To generate the data staggering of OQPSK, the odd stream output is delayed by two output sample periods, or one-half of a Manchester bit period. Figure 4.4(a) shows the highpass filtered Manchester eye diagram. Note that intersymbol interference has been introduced at the sampling instants by the action of the highpass filter, as predicted in the software simulation. The frequency spectrum of the processed data for a random data input source is shown in Figure 4.4(b), and shows that the notch at d.c. has in fact been accentuated. However, this technique removes low frequency data energy as well, which results in the introduction of ISI into the transmit eye diagram.

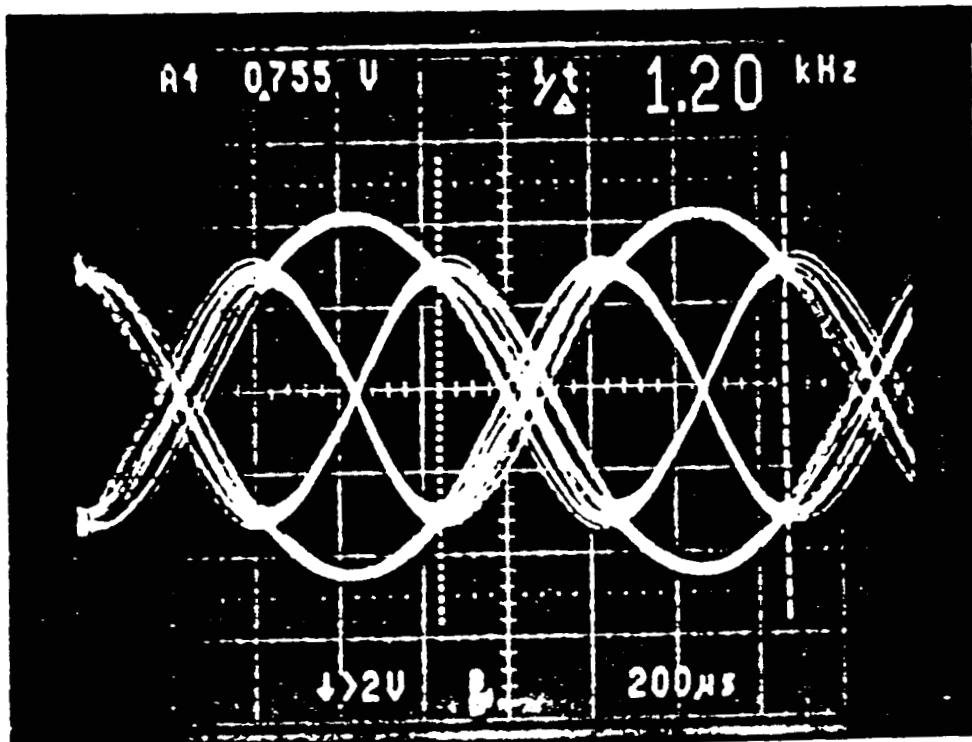
4.1.2 Demodulator

This section describes the final state of the hardware implementation of the MTCT baseband demodulator. As with the modulator, the main processing element in the demodulator is the TMS32010 DSP chip. The stand-alone digital demodulator circuitry has been designed at the schematic level and requires two TMS320 processor chips to implement in its entirety. The RF receiver circuitry, see [7], has been designed, built and tested. The demodulator code has been written for both TMS320 processors, and has been debugged to the extent possible with the available software simulation packages. The TMS320 demodulator software has been included in Appendix III.

A block diagram of the digital MTCT demodulator appears in Figure 4.5. It is necessary to employ two TMS320 processors due to the complexity of the demodulation scheme; the partitioning of the signal processing requirements between the two processors is as indicated in Figure 4.5.

The received signal is translated to a suitable IF frequency by the RF circuitry and then converted to a digital signal prior to demodulation. The RF circuitry includes a step attenuator and bandpass filter which are used to accurately set carrier-to-noise ratios. The bandpass filter is also used to reject unwanted mixer products.

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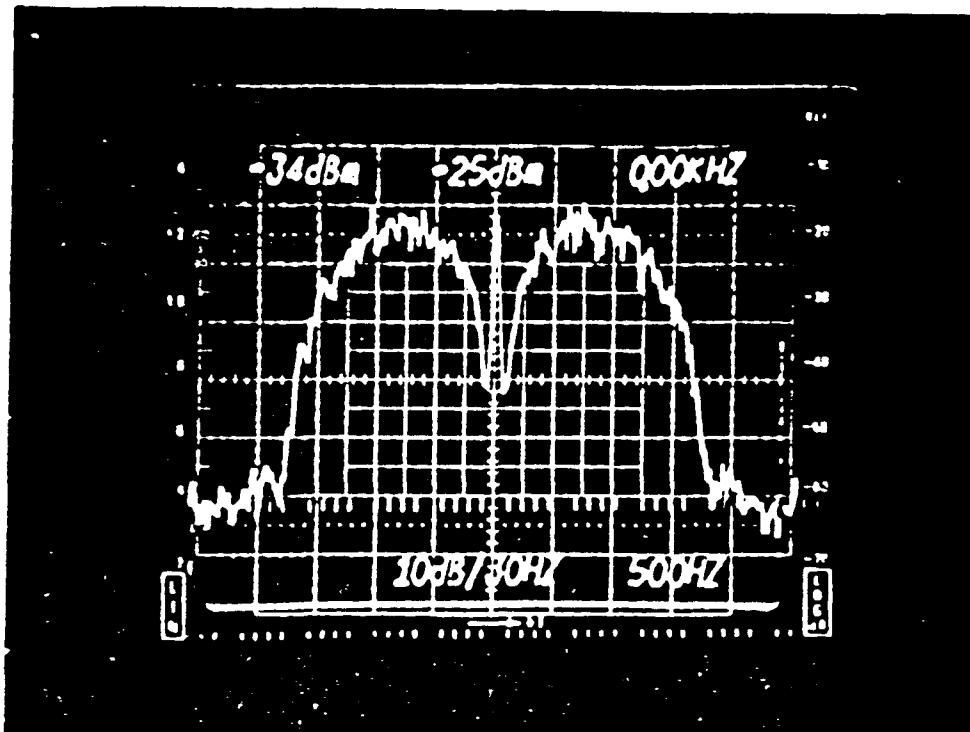


FILTERED EYE DIAGRAM - 1.2 kbps

MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,
8-BIT DAC, BETA = 0.5,
FOLLOWED BY A 45 TAP HIGH PASS FILTER

FIGURE 4.4 (a)

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FILTERED PULSE SHAPED SPECTRUM - 1.2 kbps

MANCHESTER CODING, 4 SAMPLES PER BIT SHAPING,
8-BIT DAC, BETA = 0.5,
FOLLOWED BY A 45 TAP HIGH PASS FILTER

FIGURE 4.4 (b)

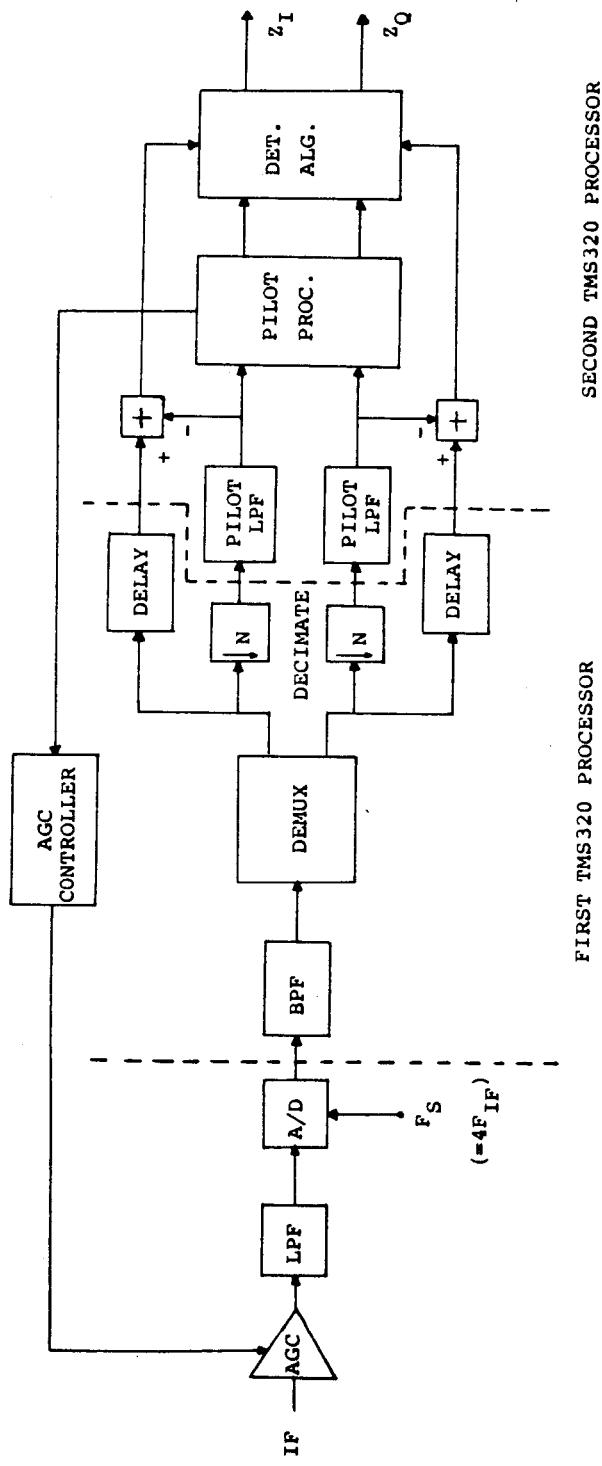


FIGURE 4.5 MTCT DEMODULATOR

The received signal is fed to the RF port of a double balanced mixer where it is mixed with the LO signal. A low-side mix arrangement is used with a 149.999988 MHz LO, producing an intermediate frequency of 12 kHz. The resulting IF signal is filtered and amplified by a fixed gain stage. Automatic Gain Control has not been considered in this implementation, due to its added complexity, however, if it was to be included, it would be introduced after the IF filtering as part of the IF gain stage. The output of the gain stage is then fed to the input of a 14-bit A/D converter, operating at 48 ksamples/second, i.e. four times the IF frequency, to generate the digital input to the baseband MTCT demodulator. This sample rate will eventually produce 10 samples per Manchester code bit or 20 per raw data bit, which, as shown by computer simulation, is more than sufficient for the demodulation and detection processes.

Due to this particular choice of sampling frequency, four times the intermediate frequency, it is apparent that quadrature sample pairs have been produced. This can be directly compared to the conventional generation of I and Q signals which employs quadrature analog mixing. As a direct result of the 4*IF sampling frequency, the sampled IF signal emanating from the A/D is such that every other pair of samples are phase inverted. Translation to baseband is accomplished by simply changing the sign of these inverted quadrature pairs. This is equivalent to mixing the IF signal with a square wave of the same frequency.

The amount of processing necessary for implementation of the digital demodulator cannot be performed at a rate of 48 ksamples per second by a single TMS320. To ease the implementation requirements, multirate processing has been used. This requires that the input signal be bandpass filtered to meet the Nyquist criterion for the maximum decimation signal processing path to avoid adjacent channel and noise aliasing (foldover). The bandpass filter meeting these requirements has the following specifications:

Passband Center: 12 kHz.
-3 dB points: 10.2 and 13.8 kHz.
-45 dB points: 6.24 and 17.74 kHz.

Linear Phase Response

The filter coefficients are listed in Table 4.3 along with the scaled values which are used in the TMS320 implementation. The bandpass filter code was tested using the TI TMS320 EVM (Evaluation Module) board; however, due to the limitation of the on-board A/D, the filter was implemented with a sample rate of 39 kHz. The amplitude and phase responses of the 39 kHz version of this bandpass filter are shown in Figures 4.6 and 4.7. These correspond to the desired 48 kHz sample rate filter when the above specifications are scaled by the factor (39/48).

The next step undertaken following the bandpass filter is to split the input data stream into inphase and quadrature channels. Recall that the I and Q streams are generated by sampling the IF signal at four times the IF frequency and processing the samples as discussed above. However, in the implementation considered, only every other sample pair is used thus avoiding the need for the inversion of alternate sample pairs without any loss of information. The remaining pairs are demultiplexed, with the first sample of each pair being placed in the I channel and the second in the Q channel. As a result of this demodulation and subsequent splitting of the received data stream, the rate of each of these channels is 12 ksamples per second, or 5 samples per Manchester code bit.

The remainder of the processing in the first TMS32010 is the same for both the inphase and quadrature channels and, therefore, only one channel will be described. The I (or Q) signal is first reproduced to form two duplicate streams. One of these duplicate streams is decimated by five, which reduces the sampling rate to 2.4 kHz, and is immediately sent on to the second TMS320 processor, where it will be low pass filtered as part of the pilot processing. It is important to note that this decimation does not cause aliasing in the

Table 4.3
Bandpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(1) = H(31)	- .1193 E-5	0
H(2) = H(30)	- .5156 E-3	-34
H(3) = H(29)	- .3013 E-6	0
H(4) = H(28)	- .01183	-775
H(5) = H(27)	- .2559 E-6	0
H(6) = H(26)	.0304	1994
H(7) = H(25)	- .7395 E-6	0
H(8) = H(24)	- .0302	-1980
H(9) = H(23)	.8667 E-6	0
H(10) = H(22)	- .0237	-1551
H(11) = H(21)	.1482 E-5	0
H(12) = H(20)	.1346	8822
H(13) = H(19)	- .8743 E-6	0
H(14) = H(18)	- .2524	-16544
H(15) = H(17)	.1010 E-5	0
H(16) =	.3035	19888

REF LEVEL /DIV MARKER 9 750.000Hz
20.000dB 10.000dB MAG(A/R) 7.302dB

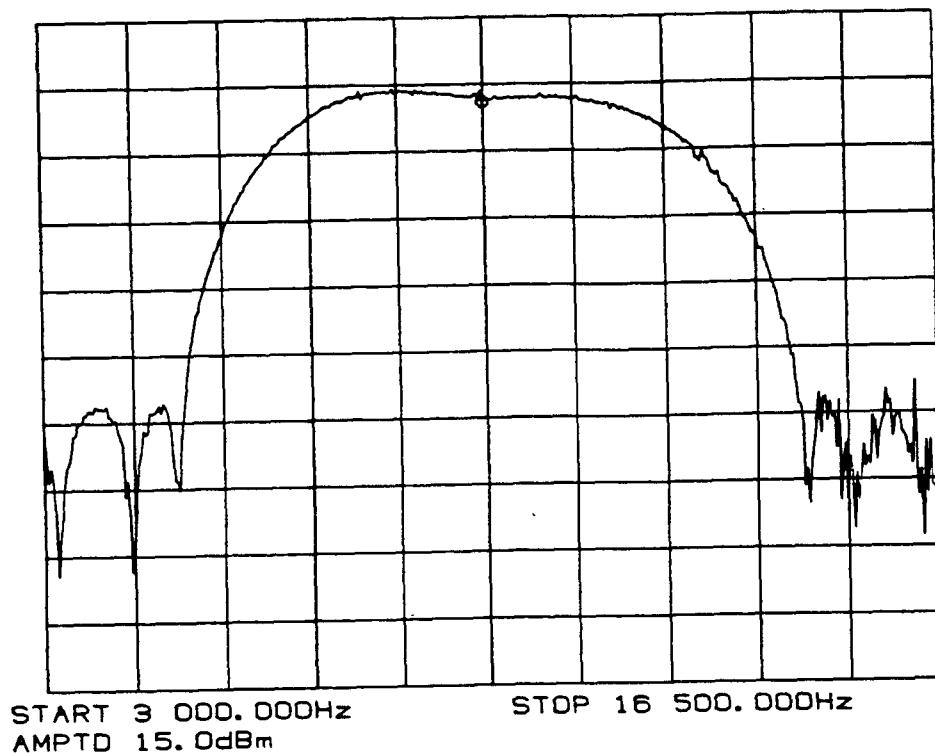


FIGURE 4.6 MAGNITUDE RESPONSE OF BANDPASS FILTER, 16 BIT COEFFICIENTS, SAMPLING FREQUENCY = 39 kHz

REF LEVEL /DIV MARKER 9 750.000Hz
0.0deg 45.000deg PHASE (A/R) 45.312deg

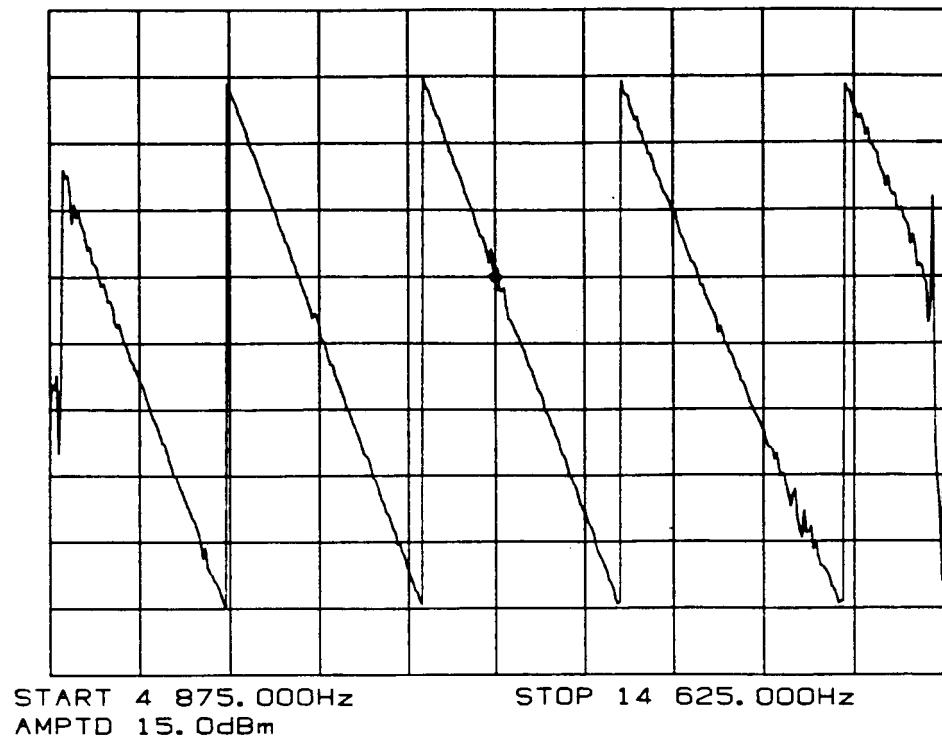


FIGURE 4.7 PHASE RESPONSE OF BANDPASS FILTER IN FIGURE 4.6

pilot filter passband but does improve the filter cut-off to sampling ratio, making it possible to use a lower order filter.

The other sample stream is placed into an external RAM, which functions as a delay buffer to compensate for the pilot processing input/output delay, thereby maintaining synchronization between the two streams. The external RAM stores the samples until it is time to send them on to the second TMS320 processor, where the pilot tone component will be removed from these appropriately delayed samples. The remaining functions of the demodulator are performed in the second processor which, conceptually, consists of two parallel paths, one dedicated to the pilot processing and the other to the delayed data. These paths converge at the detection algorithm, where fade compensation and synchronous data detection are performed. As stated above, the I and Q data streams undergo identical processing, as do the inphase and quadrature baseband pilot components.

The first operation performed in the processing of the pilot is to lowpass filter the undelayed, decimated I and Q sample trains in order to recover the pilot tone components. Assuming an expected worst case fading frequency of 80 Hz at the receiver, the lowpass filter design specifications are as follows:

- 3 dB at 80 Hz.
- 39 dB at 160 Hz.

Linear Phase Response

The pilot lowpass filter coefficients are listed in table 4.4. Included are the 13 bit scaled integer values used in the TMS320 software. The pilot digital filter was designed to operate at 2.4 kHz to achieve its desired frequency response; however, it was tested on the TMS320 EVM board at a 39 kHz sampling rate for better frequency resolution. The resulting magnitude and phase responses, of Figures 4.8 and 4.9, are therefore scaled by the factor (39/2.4). Responses are not shown to zero frequency due to leakage from the local oscillator of the network analyzer.

Table 4.4
Pilot Lowpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(0) = H(64)	-.00623	-204
H(1) = H(63)	-.00079	-26
H(2) = H(62)	-.00031	-10
H(3) = H(61)	.00052	17
H(4) = H(60)	.00164	54
H(5) = H(59)	.00294	96
H(6) = H(58)	.00426	139
H(7) = H(57)	.00538	176
H(8) = H(56)	.00609	200
H(9) = H(55)	.00619	203
H(10) = H(54)	.00550	180
H(11) = H(53)	.00393	129
H(12) = H(52)	.00148	49
H(13) = H(51)	-.00173	-57
H(14) = H(50)	-.00550	-179
H(15) = H(49)	-.00936	-307
H(16) = H(48)	-.01297	-425
H(17) = H(47)	-.01578	-517
H(18) = H(46)	-.01728	-566
H(19) = H(45)	-.01696	-556
H(20) = H(44)	-.01443	-473
H(21) = H(43)	-.00945	-310
H(22) = H(42)	-.00193	-63

Table 4.4
Pilot Lowpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(23) = H(41)	.00799	262
H(24) = H(40)	.01994	654
H(25) = H(39)	.03338	1094
H(26) = H(38)	.04758	1559
H(27) = H(37)	.06169	2021
H(28) = H(36)	.07483	2452
H(29) = H(35)	.08613	2822
H(30) = H(34)	.09480	3107
H(31) = H(33)	.10028	3286
H(32)	.10215	3347

REF LEVEL /DIV MARKER 997. 000Hz
30. 000dB 10. 000dB MAG (A/R) 10. 529dB

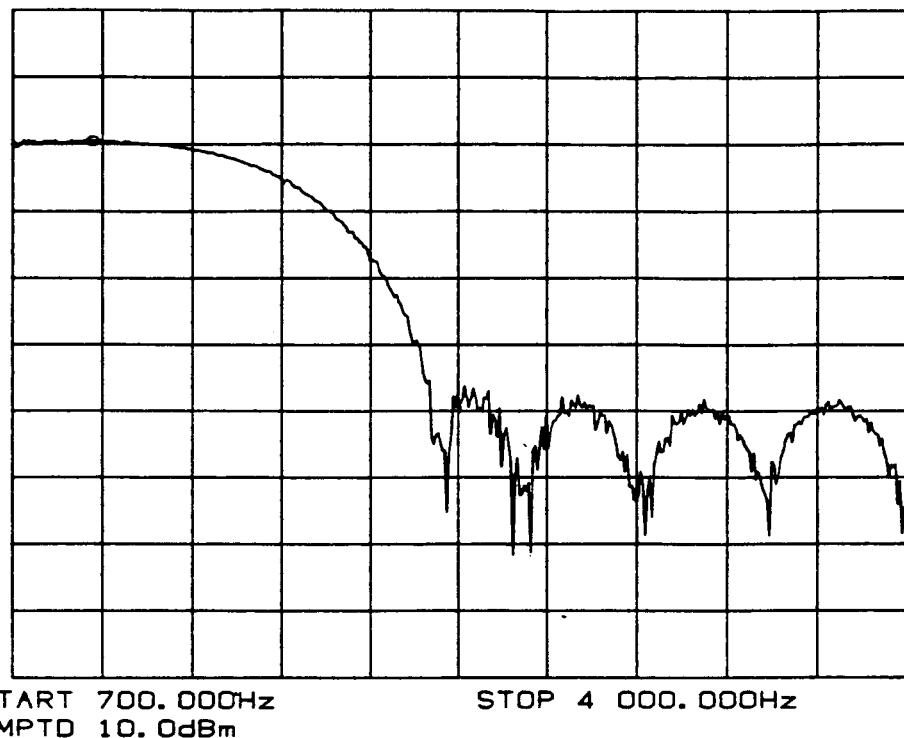


FIGURE 4.8 MAGNITUDE RESPONSE OF THE PILOT LOWPASS FILTER,
13 BIT COEFFICIENTS, SAMPLING FREQUENCY = 39 kHz

REF LEVEL /DIV MARKER 754. 000Hz
0. 0deg 45. 000deg PHASE (A/R) -97. 500deg

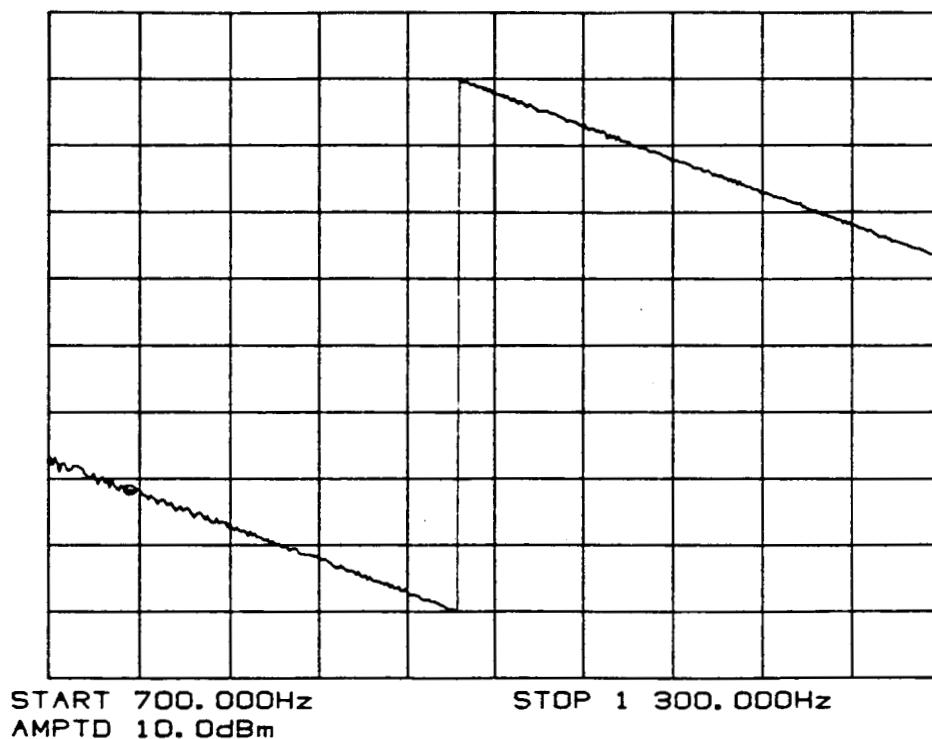


FIGURE 4.9 PHASE RESPONSE OF THE PILOT LOWPASS FILTER IN
FIGURE 4.8

The filtered I and Q streams are utilized in two ways: (1) they are passed on to the pilot processor and (2) they are subtracted from their respective delayed I/Q sample train. The latter operation removes the pilot from the unfiltered 12 kHz sample stream and the result is sent to the detection algorithm.

The subtraction of the lowpass filtered signal from the delayed sample stream may at first appear to be straightforward, however it is complicated by the multirate processing. Specifically, the unfiltered stream has a sample rate of 12 kHz, while the filtered stream, having been decimated by five, has a sample rate of only 2.4 kHz. In order to perform the subtraction, a linear interpolation of the sample values of the 2.4 kHz stream is used to raise the sample rate. Linear interpolation was selected over the less complex zero-order hold method because the software simulation of this demodulator indicated that the additional accuracy afforded by the interpolation method is necessary.

The I and Q recovered pilot components, at 2.4 ksamples/sec, are passed onto the pilot processor block which extracts the fading phase information. This, in turn, is passed onto the detection algorithm where it is used to mitigate the fading effects on the data sidebands. This process is based on the assumption that the pilot has been exposed to the same channel perturbations as the data, e.g. Rician or Rayleigh multipath fading. The I and Q outputs of the the pilot processor are used in the detection algorithm as coherent phase references. The pilot processing function is detailed in equation 4.3.

$$\tan^{-1}(\phi) = Q_p/I_p = \cos(\phi)/\sin(\phi) \quad (4.3)$$

In the actual implementation, the inverse tangent is not evaluated, rather, the result of the Q_p/I_p division is used to determine the corresponding sine and cosine values via a look-up table. The periodicity and symmetry of the trigonometric functions are exploited to minimize the size of this look-up table, only $\cos(\phi)$ and $\sin(\phi)$ values for ϕ in the range $[0, \pi/4]$ need be stored in order to implement this function. Therefore, this processing block will

first divide a quadrature sample by its corresponding inphase sample, then simply use this look-up table to locate the appropriate cosine and sine values. The $[0, \pi/4]$ angle range is subdivided into 128 levels. Software simulations have shown that this is of sufficient accuracy. These cosine and sine terms are sent on to the next phase in the demodulator, the detection algorithm.

The last section of the demodulator is the detection algorithm. This function block uses the sine and cosine of the pilot angle, which at this point should consist of the pilot tone with amplitude variations removed, as coherent phase references for the simultaneous operations of data recovery and the removal of channel phase perturbations. The algorithm is as follows:

$$Z_I = 2I_D \cos(\varphi) + 2Q_D \sin(\varphi) \quad (4.4)$$

and

$$Z_Q = 2Q_D \cos(\varphi) - 2I_D \sin(\varphi) \quad (4.5)$$

where I_D and Q_D are the inphase and quadrature samples from the 12 kHz streams. The demodulated signals, Z_I and Z_Q , are then fed off chip to analog integrate-and-dump data detectors to produce an estimate of the transmitted data.

As in the case of the removal of the pilot signal from the received signal, the detection process is complicated by the multirate processing. Here, the I and Q streams are sampled at 12 kHz while the cosine and sine signals are sampled at only 2.4 kHz. As before, linear interpolation is employed to match the rates of the two streams. The outputs of the detector consist of one inphase and one quadrature data channel, which are filtered to remove out-of-band noise before they are sent on to the detector/decoder board. The specifications for this final data filter are

-3 dB at 2.0 kHz.
-30 dB at 2.4 kHz.

Linear Phase Response

The coefficients and their scaled integer values for the data lowpass filter are listed in table 4.5. The designed sampling frequency is 12 kHz. The tested sampling frequency is 19.52 kHz, yielding a scaling factor of (19.52/12) for the magnitude and phase frequency responses of Figures 4.10 and 4.11.

4.2 Subcarrier TCT Modulator

In section 2, the subcarrier method of TCT was presented, and proved to be similar, in many respects, to the Manchester encoded TCT. The basic difference between the two approaches is the way in which they create the spectral null at d.c. The STCT version creates this null by simply modulating the data onto a very low frequency subcarrier. The similarities between the two approaches carry through to their hardware implementation. A hardware version of the STCT modulator was also completed. It utilizes the same stand-alone board and RF circuitry employed in the MTCT modulator. In order to change modulation methods, it is only necessary to replace the two EPROM's used for program memory with those containing the subcarrier code.

The TMS320 implementation of the STCT modulator, outlined previously in Figure 2.3, is quite similar to the MTCT version described previously. The data is input at the same rate, 2.4 kbps, and is immediately split into separate inphase and quadrature channels. The Manchester coding is replaced here by a simpler bipolar coding scheme, and the code bits are then sent on at a rate of 1.2 kbps to the pulse shaping section.

The pulse shape used for the STCT modulator is the same as that employed in the MTCT modulator, a raised-cosine waveform with a β of 0.5, truncated to eight code bits. The subcarrier version, however, represents this waveform in the digital domain by eight samples per bit, instead of the four which were

Table 4.5
Data Lowpass Filter Coefficients

	<u>Actual Value</u>	<u>Scaled Value</u>
H(0) = H(40)	-.00453	-37
H(1) = H(39)	-.00306	-25
H(2) = H(38)	.01315	108
H(3) = H(37)	-.00009	-1
H(4) = H(36)	-.00535	-44
H(5) = H(35)	-.01099	-90
H(6) = H(34)	-.00104	-8
H(7) = H(33)	.01268	104
H(8) = H(32)	.01460	120
H(9) = H(31)	-.00315	-26
H(10) = H(30)	-.02296	-188
H(11) = H(29)	-.01866	-153
H(12) = H(28)	.01308	107
H(13) = H(27)	.03960	324
H(14) = H(26)	.02212	181
H(15) = H(25)	-.03587	-294
H(16) = H(24)	-.07452	-610
H(17) = H(23)	-.02444	-200
H(18) = H(22)	.12216	1001
H(19) = H(21)	.28662	2348
H(20)	.35858	2937

REF LEVEL /DIV MARKER 1 960.000Hz
33.000dB 10.000dB MAG (A/R) 10.313dB

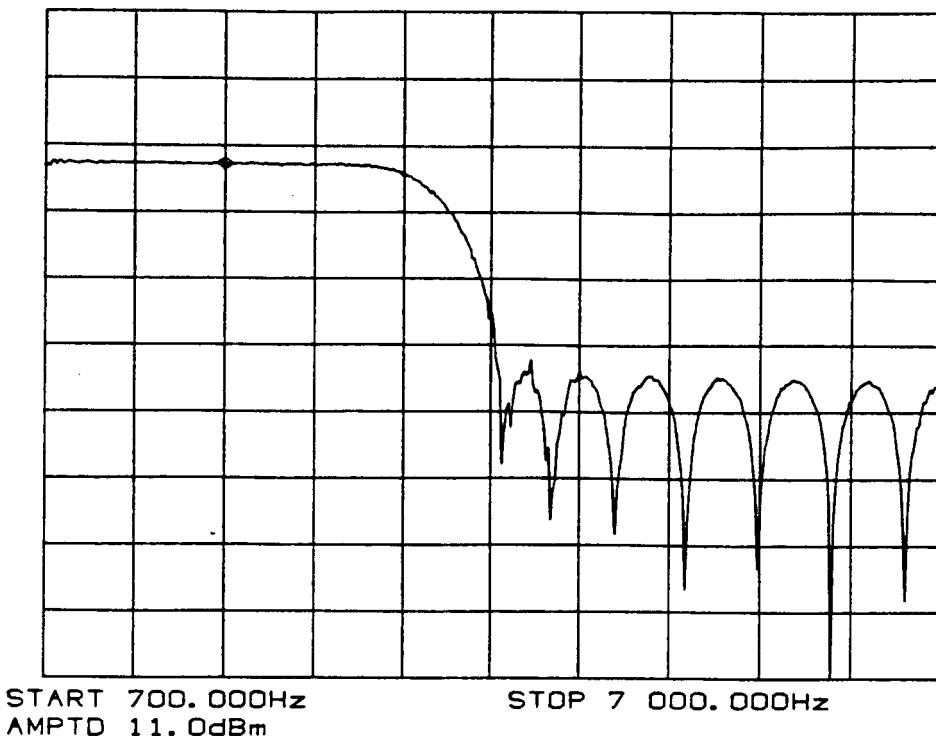


FIGURE 4.10 MAGNITUDE RESPONSE OF THE DATA LOWPASS FILTER
13 BIT COEFFICIENTS, SAMPLING FREQUENCY = 19.52 kHz

REF LEVEL /DIV MARKER 1 146.000Hz
0.0deg 45.000deg PHASE (A/R) 93.158deg

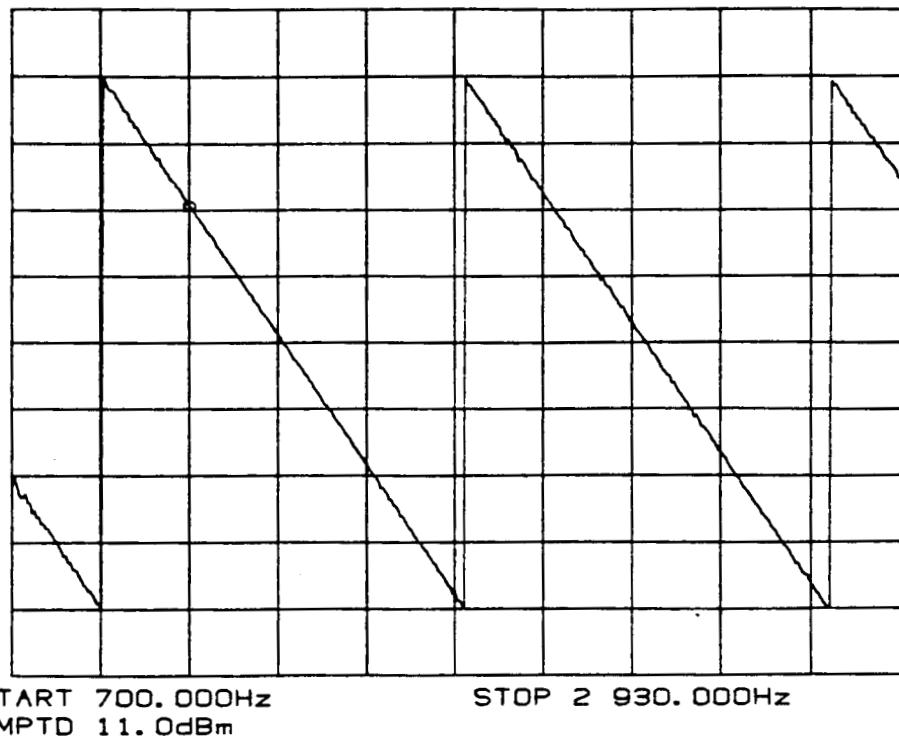


FIGURE 4.11 PHASE RESPONSE OF THE DATA LOWPASS FILTER IN

FIGURE 4.10

used earlier. This doubling of the number of samples per bit insures that the output of the pulse shaping section has a rate of 9.6 ksamples per second, the same rate the output waveform has in the MTCT implementation.

The eye diagram produced by the STCT pulse shaping section is shown in Figure 4.12(a). Note, once more, that at the sampling instants there is negligible intersymbol interference. The spectrum of this waveform is shown in the following illustration, Figure 4.12(b), and is the required 40 dBc at 1.8 kHz.

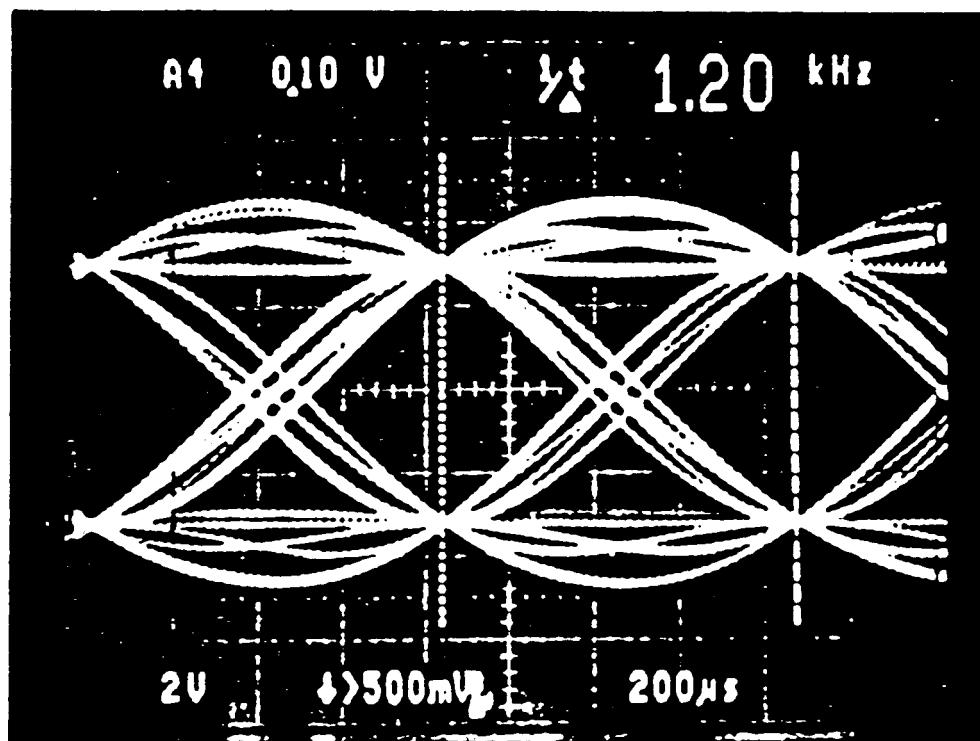
The final block of the STCT processor is the modulation section. Here, the shaped even stream is multiplied by a cosine term, the odd stream by a sine term, they are summed and then passed to the RF circuitry. The subcarrier frequency of these sine and cosine terms was chosen to be 960 Hz because it is an integer submultiple of the data rate 9.6 kHz. This means that only ten sample values of each sinusoid need to be stored in order to implement the modulator. The result of this modulation is then sent on to the D/A on the RF board.

The spectrum produced by the STCT modulator is shown in Figure 4.13. The modulation has produced a deep null at zero frequency, where the pilot would be placed. This null is deeper than that created by the MTCT modulator, as expected. The null width could be increased and the bandwidth reduced to the specified 3.6 kHz by simply changing the pulse shape to have a β value of 0.4.

5. CONCLUSIONS

The two major goals of this program were the design of an improved, all digital, Manchester encoded based TCT modulator as well as the investigation of a baseband I/Q demodulator and detector. It is believed that both of these goals were achieved and, in addition, a viable alternative to the Manchester system, the subcarrier technique, was derived.

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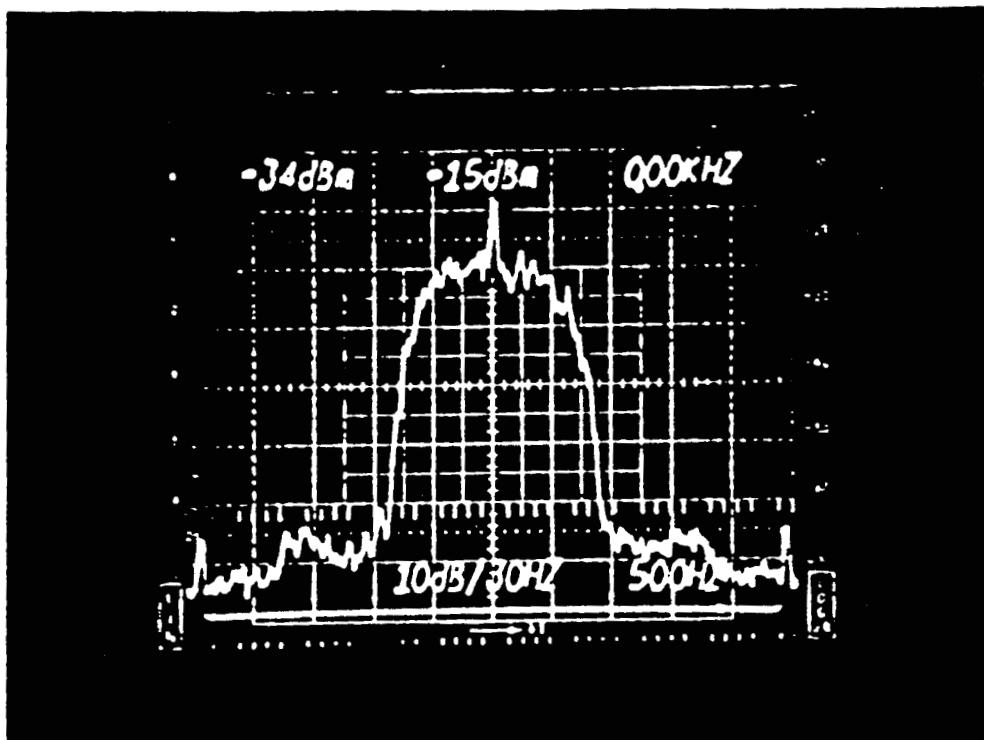


EYE DIAGRAM - 1.2 Kbps

NRZ CODING, 8 SAMPLES PER BIT SHAPING,
8 BIT DAC, BETA = .5

FIGURE 4.12 (a)

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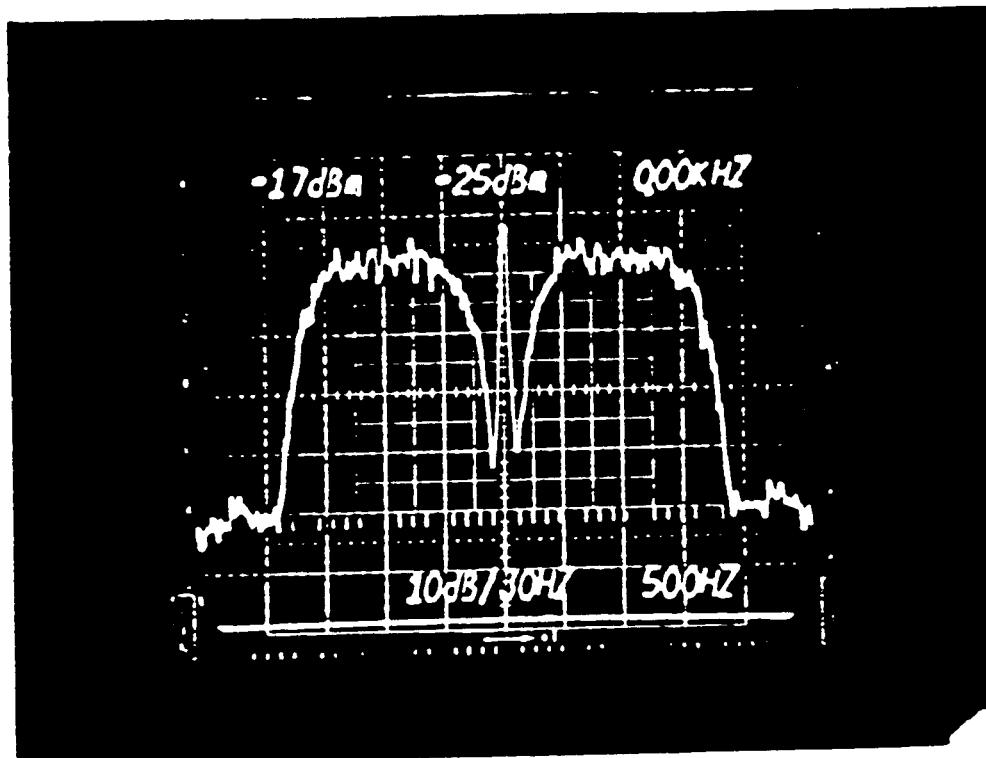


PULSE SHAPED SPECTRUM - 1.2 Kbps

NRZ CODING, 8 SAMPLES PER BIT SHAPING,
8 BIT DAC, BETA = .5

FIGURE 4.12(b)

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MODULATED PULSE SHAPED SPECTRUM - 1.2 Kbps

NRZ CODING, 8 SAMPLES PER BIT SHAPING,
8 BIT DAC, BETA = .5

FIGURE 4.13

Computer simulation and hardware implementation were employed to investigate the Manchester TCT modulator proposed by Davarian [2] which included a highpass filter to improve the spectral null created by the Manchester source encoding. The results obtained showed that the spectral null at zero frequency could be enlarged by the filtering, however, the removal of the low frequency data energy introduced intersymbol interference of approximately 18% into the transmit data eye. This was considered to be a significant disadvantage given the amount of additional filtering that was required in both the inphase and quadrature paths. It is apparent that this technique is less than optimum especially since no advantage was being derived from the raised-cosine shaping in the critical area of the spectral null.

To gain the advantage of the pulse-shaping and simultaneously remove the need for the highpass filters, it was clear that a subcarrier modulation technique should be explored. This would permit the arbitrary location of the upper and lower data sidebands at a point where they would be symmetrical around the transmit band center. This would also allow for equal sideband roll-off without incurring an ISI penalty, by virtue of the excess bandwidth fraction. In this way the shape of the data spectrum around zero frequency can be easily controlled. In addition, the premodulation processing is simplified, as was shown in section 2.2.1. It has also been demonstrated that, using the STCT processor, it is now possible to perform fully digital QPSK modulation with all the attendant advantages, such as improved carrier suppression, pilot insertion and adjustment free operation. The subcarrier TCT modulator was simulated and constructed, and demonstrated superior performance to that of the MTCT counterpart. The use of the subcarrier, however, slightly complicates the demodulator arrangement over that of the MTCT system but this is not considered to be a serious problem, as has been borne out by computer simulation.

Considerable effort was directed towards the design, computer simulation and implementation of a baseband TCT compatible demodulator. The salient features of the selected configuration are: a pilot phase-recovery-only scheme, used to reduce implementation complexity; inband pilot components in the I and Q data paths, removed by a simple subtraction process; multi-rate

processing, also for reduced complexity; and a provision for a long term AGC function.

Computer simulation of both the Manchester and subcarrier demodulators, in conjunction with their respective modulators, revealed no conceptual problems, however, neither system was tested with either simulated noise or fading. The results of the software simulation did show that for a 16 bit processor architecture, the demodulator processing should not significantly degrade the overall system performance. This was confirmed by preliminary results of the real-time implementation. Direct comparisons of digital filter frequency responses between the simulation and the hardware indicated little difference in both magnitude and phase. As a result, the increase in complexity for floating point arithmetic processing is not considered an acceptable alternative. The same reasoning applies to any discrete hardware approach. The TMS320 provides sufficient processing power and the shortest critical path time in system development.

The additional processing required by the subcarrier demodulator, the remodulation and phase estimation processes, do not appear to impact the system performance and are readily implementable in the DSP chip. The simulations show that the subcarrier phase estimation loop acquires synchronization rapidly, as would be expected from a first order loop, and, consequently, would have little impact on the system throughput.

Given the RF channel allocation and eventual data rate of 4.8 kbps in 5 kHz, it would appear that neither Manchester nor the subcarrier techniques offer a viable solution. Even with expected performance gain of the subcarrier technique, it is clear that the system is very wasteful in terms of bandwidth and as a result requires excessively large M-ary signalling schemes for data transmission.

A potential candidate TCT scheme which approaches the system bandwidth goals is the dual-pilot method proposed by General Electric [8], and subsequently analyzed by Simon [9]. In this scheme, the bandwidth requirements can be reduced by a factor of two, however, there is a power performance penalty incurred due to the use of two pilots. This penalty may tend to ultimately

balance out the performances of the single and dual pilot schemes.

The dual-pilot scheme is slightly more complicated than either single pilot scheme but is still amenable to digital implementation using similar techniques to those developed during this program. Consequently, this scheme would be a worthwhile subject for future work in an attempt to derive the optimum TCT transceiver for the satellite fading mobile communication link.

6. REFERENCES

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- [2] F. Davarian, "High Performance Communication in Mobile Channels", IEEE 34th Vehicular Technology Conference, Pittsburgh, Pa. Session C5, May 1984.
- [3] J. McGeehan, A. Bateman, "Theoretical and Experimental Investigation of Feedforward Signal Regeneration", IEEE Trans. Vehicular Technology, Vol. VT-32, pp. 106-120, Feb. 1983.
- [4] F. Davarian, M. Simon, J. Sumida, "DMSK: A Practical 2400 bps Satellite Receiver for Mobile Satellite Service", JPL Publication 85-51, MSAT-X Report No. 111, June 15, 1985.
- [5] General Electric Corporate Research and Development, "An Additional Study and Implementation of Tone Calibrated Technique of Modulation - First Interim Report", Prepared for JPL Contract No. 957190, August 1985.
- [6] Jet Propulsion Lab, "Baseband Implementation of a Tone Calibrated Receiver", Exhibit I, JPL Contract No. 957190, June 1985.

- [7] General Electric Corporate Research and Development, "An Additional Study and Implementation of Tone Calibrated Technique of Modulation - Second Interim Report", Prepared for JPL Contract No. 957190, August 1985.
- [8] General Electric Corporate Research and Development, "Design of a MSAT-X Mobile Transceiver and Related Ground Segment Technology", Technical Proposal to JPL, GE No. 1C-6-0357-215, September 1984.
- [9] M. K. Simon, "Dual Pilot Tone Calibration Technique (DPTCT)", Internal JPL Document.

APPENDIX I

TMS320 BANDPASS FILTER SOFTWARE

```

0001      ICT      "BPF"
0002 ****
0003 *
0004 *      SOFTWARE FOR BOARD 1 OF THE REAL TIME
0005 *      IMPLEMENTATION OF THE MANCHESTER TCT
0006 *      DEMODULATOR
0007 *
0008 *      Written by - Norman E. Lay
0009 *      Last Updated : 8/30/85
0010 *
0011 *      General Electric Company
0012 *      Corporate Research & Development
0013 *      Schenectady, N.Y.
0014 *
0015 *-----*
0016 *
0017 *      The following TMS-320 assembler code
0018 *      implements a bandpass filter at a samp-
0019 *      ling frequency of 48kHz with a center
0020 *      frequency of 12kHz and a passband width
0021 *      of 3.6kHz. Additional overhead functions
0022 *      are also performed, including decimation
0023 *      by 4:1 (data) and by 20:1 (pilot) and de-
0024 *      lay equalization to compensate for the
0025 *      pilot lowpass filter in the demodulator.
0026 *      The output of this board will be 2 12kHz
0027 *      data streams, 2 2.4kHz pilot streams and
0028 *      a synchronization pulse to align the pilot
0029 *      and data streams.
0030 *
0031 *-----*
0032 *
0033 0000 INPUT EQU    >0      )
0034 0001 Z1   EQU    >1      ) Beginning of Ram
0035 0002 Z2   EQU    >2      ) for Delay Storage
0036 0003 Z3   EQU    >3      )
0037 0004 Z4   EQU    >4      )
0038 0005 Z5   EQU    >5      )
0039 0006 Z6   EQU    >6      )
0040 0007 Z7   EQU    >7      )
0041 0008 Z8   EQU    >8      )
0042 0009 Z9   EQU    >9      )
0043 000A Z10  EQU    >A      )
0044 000B Z11  EQU    >B      )
0045 000C Z12  EQU    >C      )
0046 000D Z13  EQU    >D      )
0047 000E Z14  EQU    >E      )
0048 000F Z15  EQU    >F      )
0049 0010 Z16  EQU    >10     )
0050 0011 Z17  EQU    >11     )
0051 0012 Z18  EQU    >12     )
0052 0013 Z19  EQU    >13     )
0053 0014 Z20  EQU    >14     )
0054 0015 Z21  EQU    >15     )
0055 0016 Z22  EQU    >16     )
0056 0017 Z23  EQU    >17     )
0057 0018 Z24  EQU    >18     )

```

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0058	0019	225	EQU	>19	>	.
0059	001A	226	EQU	>1A	>	.
0060	001B	227	EQU	>1B	>	.
0061	001C	228	EQU	>1C	>	.
0062	001D	229	EQU	>1D	>	End of Ram for
0063	001E	230	EQU	>1E	>	Delay Storage
0064	*					
0065	001F	TAP2	EQU	>1F	>	Beginning of Ram
0066	0020	TAP4	EQU	>20	>	Storage for Coeffs.
0067	0021	TAP5	EQU	>21	>	.
0068	0022	TAP8	EQU	>22	>	.
0069	0023	TAP1C	EQU	>23	>	.
0070	0024	TAP12	EQU	>24	>	.
0071	0025	TAP14	EQU	>25	>	Half of the filters
0072	0026	TAP16	EQU	>26	>	coefficients are
0073	0027	TAP18	EQU	>27	>	coded as zeros
0074	0028	TAP20	EQU	>28	>	.
0075	0029	TAP22	EQU	>29	>	.
0076	002A	TAP24	EQU	>2A	>	.
0077	002B	TAP26	EQU	>2B	>	.
0078	002C	TAP2E	EQU	>2C	>	End of Ram Storage
0079	002D	TAP30	EQU	>2D	>	for Coefficients
0080	*					
0081	003E	BPF1	EQU	>3E	>	Input Buffer to
0082	003F	BPF2	EQU	>3F	>	Delay.
0083	0040	PILOT2	EQU	>40	>	
0084	0041	PILOT1	EQU	>41	>	Output Buffers to 2nd
0085	0042	DBPF1	EQU	>42	>	Demodulator Board
0086	0043	DBPF2	EQU	>43	>	
0087	0044	TWO	EQU	>44	>	Constants = 1,2
0088	0045	CNE	EQU	>45	>	
0089	0046	DUTFLG	EQU	>46	>	Decimation and Sync.
0090	0047	SNCFLG	EQU	>47	>	Flags
0091	0048	CLYACX	EQU	>48	>	External Ram Address Pointer
0092	0049	DLYBEG	EQU	>49	>	
0093	004A	FIFOND	EQU	>4A	>	Stored Address Constants
0094	*					
0095	007E	IACH	EQU	>7E	>	Accumulator Storage
0096	007F	IACL	EQU	>7F	>	During an Interrupt
0097	*					
0098	0340	CLYSIZ	EQU	>340	>	MPYK Constant
0099	0200	BUFBEG	EQU	>200	>	Definitions
0100	0400	CDEFFS	EQU	>400	>	
0101	*					
0102	*					Begin TMS-320 Code
0103	*					
0104	0000		AORG	>0		
0105	*					
0106	0000 F900		B	600T		
	0001 0700					
0107	*					
0108	*					Begin Interrupt Routine
0109	*					
0110	0002 4000	INTRPT	IN	INPUT,0		
0111	0003 587E		SACH	IACH	>	Store only the
0112	0004 507F		SACL	IACL	>	accumulator.
0113	0005 693E		DMOV	BPF1		

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0114 *
 0115 * Begin 31-tap FIR BPF
 0116 *
 0117 * Only 15 multiplies are
 0118 * needed because 16 of
 0119 * the coefficients are
 0120 * coded as zeros.
 0121 *

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0122	0006	7FB9	ZAC
0123	0007	6A1D	LT Z29
0124	0008	6D2D	MPY TAP30
0125	0009	691C	DMOV Z28
0126	000A	681B	LTD Z27
0127	000B	6D2C	MPY TAP28
0128	000C	691A	DMOV Z26
0129	000D	6819	LTD Z25
0130	000E	6D2B	MPY TAP26
0131	000F	6918	DMOV Z24
0132	0010	6817	LTD Z23
0133	0011	6D2A	MPY TAP24
0134	0012	6916	DMOV Z22
0135	0013	6815	LTD Z21
0136	0014	6D29	MPY TAP22
0137	0015	6914	DMOV Z20
0138	0016	6813	LTD Z19
0139	0017	6D28	MPY TAP20
0140	0018	6912	DMOV Z18
0141	0019	6811	LTD Z17
0142	001A	6D27	MPY TAP18
0143	001B	6910	DMOV Z16
0144	001C	6B0F	LTD Z15
0145	001D	6D26	MPY TAP16
0146	001E	690E	DMOV Z14
0147	001F	6B0D	LTD Z13
0148	0020	6D25	MPY TAP14
0149	0021	690C	DMOV Z12
0150	0022	6B08	LTD Z11
0151	0023	6D24	MPY TAP12
0152	0024	690A	DMOV Z10
0153	0025	6909	LTD Z9
0154	0026	6D23	MPY TAP10
0155	0027	6908	DMOV Z8
0156	0028	6B07	LTD Z7
0157	0029	6D22	MPY TAP8
0158	002A	6906	DMOV Z6
0159	002B	6B05	LTD Z5
0160	002C	6D21	MPY TAP6
0161	002D	6904	DMOV Z4
0162	002E	6B03	LTD Z3
0163	002F	6D20	MPY TAP4
0164	0030	6902	DMOV Z2
0165	0031	6B01	LTD Z1
0166	0032	6D1F	MPY TAP2
0167	0033	6B00	LTD INPUT
0168	0034	0F45	ADD ONE,15
0169	0035	583E	SACH BPF1,0

* Add for roundoff.

0170 *

0171 * End of BPF Code
 0172 *
 0173 0036
 0174 0036 6980 CONT LARP 0
 0175 0037 F400 BANZ RETURN
 0038 0043
 0176 0039 7003 LARK 0,3
 0177 003A 6945 DMOV ONE } Set OUTFLG.
 0178 *
 0179 003B 6881 LARP 1
 0180 003C F400 BANZ RETURN
 003D 0043
 0181 003E 7104 LARK 1,4
 0182 003F 693F DMOV BPF2
 0183 0040 203E LAC BPF1
 0184 0041 5041 SACL PILOT1
 0185 0042 6946 DMOV OUTFLG } Set SNCFLG.
 0186 *
 0187 * Restore Accumulator for
 0188 * Return from Interrupt
 0189 *
 0190 0043 657E RETURN ZALH IACH
 0191 0044 617F ACDS IACL
 0192 0045 7F82 EINT
 0193 0046 7F8D RET
 0194 *
 0195 * Start of Non-Interrupt Code for
 0196 * Modifying Delay Buffer Pointers
 0197 * and Transmitting Data to Main
 0198 * Processing Board.
 0199 *
 0200 0047 2046 WAIT LAC OUTFLG } Test for time to send.
 0201 0048 FF00 BZ WAIT
 0049 0047
 0202 004A 2048 LAC DLYADX
 0203 004B 6742 TBLR DBPF1 }
 0204 004C 7D3E TBLW BPF1 } Read in delayed data
 0205 004D 0045 ADD ONE } and read out present
 0206 004E 6743 TBLR DBPF2 } filter output.
 0207 004F 7D3F TBLW SPF2 }
 0208 0050 0045 ADD ONE
 0209 0051 5048 SACL DLYADX
 0210 *
 0211 0052 7F89 ZAC
 0212 0053 5046 SACL OUTFLG } Clear flag.
 0213 0054 2047 LAC SNCFLG } Test for time to send
 0214 0055 FF00 BZ NOSYNC } pilot.
 0056 005E
 0215 *
 0216 0057 4B47 OUT SNCFLG,3 }
 0217 0058 4F42 OUT DBPF1,7 } Output pilot/data
 0218 0059 4E41 OUT PILOT1,6 } sync, data & pilot
 0219 005A 4D43 OUT DBPF2,5 } streams.
 0220 005B 4C40 OUT PILOT2,4 }
 0221 005C F900 B MODPTR
 005D 0060
 0222 *

0223 005E 4F42	NOSYNC	OUT	DBPF1,7	> Output only data
0224 005F 4D43		OUT	DBPF2,5	> streams.
0225 *				
0226 0060 2048	MOCPTR	LAC	DLYADX	> Wrap delay buffer
0227 0061 104A		SUB	FIFOND	> pointer if needed.
0228 0062 FE00		BNZ	WAIT	
0063 0047				
0229 *				
0230 0064 2049		LAC	DLYBEG	
0231 0065 5048		SACL	DLYADX	
0232 0066 F900		B	WAIT	
0067 0047				
0233 *				
0234 *				Reset Code for Initialization
0235 *				of Constants and Pointers
0236 *				
0237 0068 7F81	RESET	DINT		
0238 0069 6E00		LDPK	0	
0239 006A 4000		IN	0,0	
0240 006B 7F8B		SOVM		
0241 006C 707F		LARK	0,>7F	
0242 006D 6880		LARP	0	
0243 006E 7F89		ZAC		
0244 006F 5088	CLRRAM	SACL	*	> Zero internal
0245 0070 F400		BANZ	CLRRAM	> ram.
0071 006F				
0246 0072 7E01		LACK	>1	
0247 0073 5045		SACL	ONE	
0248 0074 6A45		LT	ONE	
0249 0075 8340		MPYK	DLYSIZ	
0250 0076 7F8E		PAC		> Store constants.
0251 0077 504A		SACL	FIFOND	
0252 0078 8200		MPYK	BUFBEG	
0253 0079 7F8E		PAC		
0254 007A 5049		SACL	DLYBEG	
0255 *				
0256 007B 8400		MPYK	CGEFFS	
0257 007C 7F8E		PAC		
0258 007D 700E		LARK	0,14	
0259 007E 711F		LARK	1,>1F	
0260 007F 6881	LOAD	LARP	1	> Load BPF
0261 0080 67A0		TBLR	*+,0	> coefficients.
0262 0081 0045		ADD	ONE	
0263 0082 F400		BANZ	LOAD	
0083 007F				
0264 *				
0265 0084 7003		LARK	0,3	> Initialize
0266 0085 7104		LARK	1,4	> AR's.
0267 *				
0268 0086 7F82		EINT		
0269 0087 F900		B	WAIT	
0088 0047				
0270 *				
0271 *				Filter Coefficients for 48kHz BPF
0272 *				Coded into 16 bits.
0273 *				
0274 0400		AORG	>400	

0275 *
0276 0400 FFDE DATA -34,-775,1994,-1980,-1551,8822,-16544,19888
0401 FCF9
0402 07CA
0403 F844
0404 F9F1
0405 2276
0406 BF60
0407 4D80
0277 0408 BF60 DATA -16544,8822,-1551,-1980,1994,-775,-34
0409 2276
040A F9F1
040B F844
040C 07CA
040D FCF9
040E FFDE
0278 *
0279 * Boot Routine for Loading Program
0280 * Memory from EPROM to RAM
0281 *
0282 0700 AORG >700
0283 *
0284 0700 7E01 B00T LACK >1
0285 0701 5000 SACL >0
0286 0702 6A00 LT >0
0287 0703 87FF MPYK >7FF
0288 0704 7F8E PAC
0289 0705 670A NOTDNL TBLR >A
0290 0706 700A TBLW >A
0291 0707 1000 SUB >0
0292 0708 FD00 BGEZ NOTDUN
0709 0705
0293 070A 8068 MPYK RESET
0294 070B 7F8E PAC
0295 070C 500A SACL >A
0296 070D 7E01 LACK >1
0297 070E 700A TBLW >A
0298 070F F900 B RESET
0710 0068
0299 *
0300 END

NO ERRORS, NO WARNINGS

APPENDIX II

TMS320 MICT PREMODULATION PROCESSING SOFTWARE

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0001           IDT      "MODUL"
0002           *
0003 0000       AORG    >0
0004           *
0005 0000 F900   B       BOOT
0001 020E
0006           *
0007           * PROGRAM TO IMPLEMENT TCT TRANSMIT BASEBAND PROCESSING.
0008           * THIS CONTAINS THE TWO PATHS NEEDED TO
0009           * IMPLEMENT THE ENTIRE SYSTEM. DATA IS INPUT AS 0 OR 1,
0010           * IS THEN MANCHESTER ENCODED, RAISED COSINE PULSE SHAPED,
0011           * AND FINALLY HIGH PASS FILTERED. WE ASSUME HERE THAT
0012           * DATA IS BEING RECEIVED INTO TRANSMITTER AT 2.4 KBPS.
0013           * THE DATA IS SPLIT INTO ODD AND EVEN STREAM, AND THEN
0014           * MANCHESTER ENCODED, SO THE RATE STAYS AT 2.4 KBPS.
0015           * RAISED COSINE PULSE SHAPING IS DONE USING LAST EIGHT
0016           * CODE BITS, WITH 4 SAMPLES BEING OUTPUT FOR EACH CODE
0017           * BIT. THE OUTPUT IS THEREFORE CLOCKING OUT AT 9.6 KPBS,
0018           * AND A NEW INPUT IS TAKEN ONCE EVERY FOUR OUTPUTS.
0019           *
0020           * INPUT COEFFICIENTS NEEDED FOR PULSE SHAPING, CLOCK, ETC.
0021           *
0022 0010       AORG    >10
0023           *
0024 0010 0024   C1      DATA    36      * PULSE SHAPING COEFFICIENT P(1)
0025 0011 0058   C2      DATA    91      * P(2) ALL PULSE SHAPING COEFFICIENTS
0026 0012 004C   C3      DATA    76      * P(3) ARE SCALED BY 16384
0027 0013 000E   C4      DATA    14      * P(4)
0028 0014 0013   C5      DATA    19      * P(5)
0029 0015 00AD   C6      DATA    173     * P(6)
0030 0016 016B   C7      DATA    363     * P(7)
0031 0017 0106   C8      DATA    262     * P(8)
0032 0018 FE61   C9      DATA   -415     * P(9)
0033 0019 FA21   C10     DATA   -1503    * P(10)
0034 001A F776   C11     DATA   -2186    * P(11)
0035 001B FAE9   C12     DATA   -1303    * P(12)
0036 001C 0768   C13     DATA    1899    * P(13)
0037 001D 1874   C14     DATA    7028    * P(14)
0038 001E 308F   C15     DATA   12431    * P(15)
0039 001F 3E24   C16     DATA   15908    * P(16)
0040 0020 FFFF   C17     DATA    -1      * HOLDS -1 FOR MANCHESTER CODING
0041 0021 8000   C18     DATA   >8000    * BIAS TERM FOR INTERFACE TO BIPOLAR
0042 0022 000A   C19     DATA    10      * AIB BOARD CLOCK PARAMETER
0043 0023 0200   C20     DATA    512     * AIB BOARD CLOCK PARAMETER
0044           *
0045           * WRITE CONSTANTS TO DATA MEMORY
0046           *
0047           *
0048           *
0049 0024 7F80   RESET   NOP
0050 0025 7F80   NOP
0051 0026 7F81   DINT
0052 0027 7F83   SOVM
0053 0028 6E00   LOPK   0
0054 0029 7E10   LACK   C1      * P(1)
0055 002A 6700   TBLR   0
0056 002B 7E11   LACK   C2      * P(2)

```

0057 002C 6701	TBLR	1	
0058 002D 7E12	LACK	C3	* P(3)
0059 002E 6702	TBLR	2	
0060 002F 7E13	LACK	C4	* P(4)
0061 0030 6703	TBLR	3	
0062 0031 7E14	LACK	C5	* P(5)
0063 0032 6704	TBLR	4	
0064 0033 7E15	LACK	C6	* P(6)
0065 0034 6705	TBLR	5	
0066 0035 7E16	LACK	C7	* P(7)
0067 0036 6706	TBLR	6	
0068 0037 7E17	LACK	C8	* P(8)
0069 0038 6707	TBLR	7	
0070 0039 7E18	LACK	C9	* P(9)
0071 003A 6708	TBLR	8	
0072 003B 7E19	LACK	C10	* P(10)
0073 003C 6709	TBLR	9	
0074 003D 7E1A	LACK	C11	* P(11)
0075 003E 670A	TBLR	10	
0076 003F 7E1B	LACK	C12	* P(12)
0077 0040 670B	TBLR	11	
0078 0041 7E1C	LACK	C13	* P(13)
0079 0042 670C	TBLR	12	
0080 0043 7E1D	LACK	C14	* P(14)
0081 0044 670D	TBLR	13	
0082 0045 7E1E	LACK	C15	* P(15)
0083 0046 670E	TBLR	14	
0084 0047 7E1F	LACK	C16	* P(16)
0085 0048 670F	TBLR	15	
0086 0049 6E01	LDPK	1	
0087 004A 7E20	LACK	C17	* -1
0088 004B 6705	TBLR	5	
0089 004C 7E21	LACK	C18	* BIAS
0090 004D 6706	TBLR	6	
0091 004E 7E22	LACK	C19	* CLOCK CONSTANT
0092 004F 6708	TBLR	8	
0093 0050 7E23	LACK	C20	* CLOCK CONSTANT
0094 0051 6709	TBLR	9	
0095 *			
0096 0052 7E00	LACK	0	
0097 0053 5003	SACL	3	
0098 0054 5004	SACL	4	
0099 0055 F900	B	MAN	
0056 0057			
0100 *			
0101 * MAIN CODE LOOP			
0102 * MANCHESTER CODING SECTION			
0103 *			
0104 * CODE ODD BIT.			
0105 *			
0106 0057 6E01	MAN	LDPK	1
0107 0058 2003		LAC	3
0108 0059 FF00		BZ	ZERO
005A 0062			*LOAD ODD DATA BIT INTO ACCUMULATOR
			*BRANCH TO ZERO SECTION IF ZERO
0109 *			
0110 * HERE, A 1 BECOMES -1,1			
0111 *			

0112 0058 2005 LAC 5 *LOAD ACCUM. WITH -1
 0113 005C 6E00 LDPK 0
 0114 005D 5070 SACL 112 *STORE FIRST MANCHESTER BIT, OMB(N) IN HERE, IT WILL BE READY FOR PULSE SHAPING.
 0115 *
 0116 005E 7E01 LACK 1 *LOAD ACCUM. WITH 1, SECOND MANCHESTER BIT.
 0117 005F 6E01 LDPK 1
 0118 *
 0119 0060 F900 8 DONE
 0061 0067
 0120 *
 0121 * HERE, A 0 BECOMES 1,-1
 0122 *
 0123 0062 7E01 ZERO LACK 1 *LOAD ACCUM. WITH 1
 0124 0063 6E00 LDPK 0
 0125 0064 5070 SACL 112 *STORE OMB(N) IN 112, WHERE IT WILL BE USED IMMEDIATELY FOR PULSE SHAPING.
 0126 0065 6E01 LDPK 1
 0127 0066 2005 LAC 5 *LOAD ACCUM. WITH -1, SECOND MANCHESTER BIT.
 0128 *
 0129 0067 5000 DONE SACL 0 *STORE SECOND MAN. BIT, OMB(N+1) IN THIS WILL BE USED IN NEXT PULSE SHAPE.
 0130 *
 0131 *
 0132 * NOW CODE EVEN BIT
 0133 *
 0134 0068 2004 LAC 4 *LOAD DATA BIT INTO ACCUMULATOR
 0135 0069 FF00 BZ ZERO1 *BRANCH TO ZERO SECTION IF ZERO
 006A 0072
 0136 *
 0137 * HERE, A 1 BECOMES -1,1
 0138 *
 0139 006B 2005 LAC 5 *LOAD ACCUM. WITH -1
 0140 006C 6E00 LDPK 0 *STORE FIRST MANCHESTER BIT, EMB(N) IN HERE, IT WILL BE USED IMMEDIATELY FOR PULSE SHAPING.
 0141 006D 5078 SACL 120 *WHERE IT WILL BE USED IMMEDIATELY FOR PULSE SHAPING.
 0142 006E 6E01 LDPK 1
 0143 *
 0144 006F 7E01 LACK 1 *LOAD ACCUM. WITH 1, SECOND MANCHESTER BIT.
 0145 *
 0146 0070 F900 8 DONE1
 0071 0077
 0147 *
 0148 * HERE, DATA BIT 0 BECOMES 1,-1
 0149 *
 0150 0072 7E01 ZERO1 LACK 1 *LOAD ACCUM. WITH 1
 0151 0073 6E00 LDPK 0
 0152 0074 5078 SACL 120 *STORE EMB(N) IN 120 FOR PULSE SHAPING.
 0153 0075 6E01 LDPK 1
 0154 0076 2005 LAC 5 *LOAD ACCUM. WITH -1, SECOND MANCHESTER BIT.
 0155 *
 0156 0077 5001 DONE1 SACL 1 *STORE SECOND MAN. BIT, EMB(N+1) IN THIS WILL BE STORED FOR ONE CYCLE.
 0157 *
 0158 *
 0159 0078 7E01 LACK 1 *INITIALIZE MAN. BIT COUNTER (MCOUNT)
 0160 0079 5007 SACL 7 *COUNTER STORE IN 135.
 0161 *
 0162 * FIND FIRST OF FOUR ODD OUTPUTS CORRESPONDING TO ONE MANCHESTER BIT.
 0163 * PULSE SHAPING IS DONE CHRONOLOGICALLY. THE LAST EIGHT ODD * OMB(N-7) TO OMB(N), ARE STORED IN DMA'S 112-119, WITH 112 * THE MOST RECENT.

0166		*				
0167		*				
0168	007A	6E00	MAIN1	LDPK	0	
0169		*				
0170	007B	7F89		ZAC		
0171	007C	6A77		LT	119	
0172	007D	6D03		MPY	3	* OMB(N-7)*P(4)
0173		*				
0174	007E	6C76		LTA	118	
0175	007F	6D07		MPY	7	* + OMB(N-6)*P(8)
0176		*				
0177	0080	6C75		LTA	117	
0178	0081	6D08		MPY	11	* + OMB(N-5)*P(12)
0179		*				
0180	0082	6C74		LTA	116	
0181	0083	6D0F		MPY	15	* + OMB(N-4)*P(16)
0182		*				
0183	0084	6C73		LTA	115	
0184	0085	6D0C		MPY	12	* + OMB(N-3)*P(13)
0185		*				
0186	0086	6C72		LTA	114	
0187	0087	6D08		MPY	8	* + OMB(N-2)*P(9)
0188		*				
0189	0088	6C71		LTA	113	
0190	0089	6D04		MPY	4	* + OMB(N-1)*P(5)
0191		*				
0192	008A	6C70		LTA	112	
0193	0088	6D00		MPY	0	* + OMB(N)*P(1)
0194	008C	7F8F		APAC		
0195		*				
0196	008D	5010		SACL	16	* STORE RESULT, DRCC(M), IN DMA 16
0197	008E	7007		LARK	0,7	* STORE FLAG IN AUX0, TO KEEP TRACK OUTPUT WE'RE ON.
0198		*				
0199	008F	713C		LARK	1,60	* INITIALIZE POINTER AUX1 TO OLDEST IN ODD FILTER BUFFER FOR HI PASS F WHICH IS THE NEXT STEP.
0200		*				
0201		*				
0202	0090	6881		LARP	1	* AUX1 POINTER PUT IN USE NOW.
0203		*				
0204	0091	F900			B	FILTER * BRANCH TO HIGH PASS FILTER SECTION
	0092	0195				
0205		*				
0206		*	NOW DO FIRST EVEN BIT. SAME PULSE SHAPING AS DONE FOR			
0207		*	PREVIOUS ODD BIT. MANCHESTER BIT BUFFER IS IN DMA'S			
0208		*	120-127, WITH 120 HOLDING MOST RECENT BIT.			
0209		*				
0210	0093	690C	SEVEN	DMOV	12	*MOVE ODD OUTPUTS THROUGH DELAY BUFF
0211	0094	6908		DMOV	11	* THIS BUFFER DELAYS ODD OUTPUT BY
0212	0095	690A		DMOV	10	* TWO CLOCK CYCLES.
0213		*		NOP		
0214	0096	6E00		LDPK	0	
0215	0097	7F89		ZAC		
0216	0098	6A7F		LT	127	
0217	0099	6D03		MPY	3	* EMB(N-7)*P(4)
0218		*				
0219	009A	6C7E		LTA	126	
0220	0098	6D07		MPY	7	* + EMB(N-6)*P(8)
0221		*				

0222	009C	6C7D	LTA	125	
0223	009D	6D0B	MPY	11	* + EMB(N-5)*P(12)
0224	*				
0225	009E	6C7C	LTA	124	
0226	009F	6D0F	MPY	15	* + EMB(N-4)*P(16)
0227	*				
0228	00A0	6C7B	LTA	123	
0229	00A1	6D0C	MPY	12	* + EMB(N-3)*P(13)
0230	*				
0231	00A2	6C7A	LTA	122	
0232	00A3	6D08	MPY	8	* + EMB(N-2)*P(9)
0233	*				
0234	00A4	6C79	LTA	121	
0235	00A5	6D04	MPY	4	* + EMB(N-1)*P(5)
0236	*				
0237	00A6	6C78	LTA	120	
0238	00A7	6D00	MPY	0	* + EMB(N)*P(1)
0239	00A8	7F8F	APAC		
0240	*				
0241	00A9	5030	SACL	61	*STORE RESULT, ERC(N) IN 61
0242	00AA	7006	LARK	0,6	*SET FLAG AUXO TO MARK OUTPUT WE'RE
0243	00AB	7169	LARK	1,105	*SET POINTER TO LAST ENTRY IN FILTER
0244	00AC	6881	LARP	1	*CHOOSE POINTER.
0245	*				
0246	00AD	F900	B		FILTER *BRANCH TO HI PASS FILTER SECTION.
	00AE	0195			
0247	*				
0248	*				SECOND OUTPUT OF FOUR. (ODD)
0249	*				
0250	00AF	F600	SIX	BIOZ	LOOP2 * WAIT UNTIL READY FOR OUTPUT
	0080	00B3			
0251	00B1	F900	B		SIX
	0082	00AF			
0252	*				
0253	00B3	4A0D	LOOP2	OUT	13,2 *OUTPUT DELAYED ODD SAMPLE TO PORT 2
0254	00B4	4B0A		OUT	10,3 *OUTPUT EVEN SAMPLE TO PORT 3.
0255	*				
0256	00B5	6E00	LDPK	0	
0257	00B6	7F89	ZAC		
0258	00B7	6A77	LT	119	
0259	00B8	6D02	MPY	2	* OMB(N-7)*P(3)
0260	*				
0261	00B9	6C76	LTA	118	
0262	00BA	6D06	MPY	6	* + OMB(N-6)*P(7)
0263	*				
0264	00BB	6C75	LTA	117	
0265	00BC	6D0A	MPY	10	* + OMB(N-5)*P(11)
0266	*				
0267	00BD	6C74	LTA	116	
0268	00BE	6D0E	MPY	14	* + OMB(N-4)*P(15)
0269	*				
0270	00BF	6C73	LTA	115	
0271	00C0	6D0D	MPY	13	* + OMB(N-3)*P(14)
0272	*				
0273	00C1	6C72	LTA	114	
0274	00C2	6D09	MPY	9	* + OMB(N-2)*P(10)
0275	*				

0276 00C3 6C71	LTA	113	
0277 00C4 6D05	MPY	5	* + OMB(N-1)*P(5)
0278 *			
0279 00C5 6C70	LTA	112	
0280 00C6 6D01	MPY	1	* + OMB(N)*P(2)
0281 00C7 7F8F	APAC		
0282 *			
0283 00C8 5010	SACL	16	* STORE RESULT ORC(M) IN DMA 16
0284 00C9 7005	LARK	0,5	*SET FLAG TO MARK OUTPUT.
0285 00CA 713C	LARK	1,60	*SET POINTER TO LAST SPOT IN FILTER
0286 00CB 6881	LARP	1	*CHOOSE POINTER.
0287 *			
0288 00CC F900 00CD 0195	B	FILTER	* BRANCH TO HIGH PASS FILTER.
0289 *			
0290	* SECOND OUTPUT - EVEN BIT		
0291 *			
0292 00CE 690C	FIVE	DMOV	12 *SHIFT ODD OUTPUTS THRU DELAY BUFFER
0293 00CF 690B		DMOV	11
0294 00D0 690A		DMOV	10
0295 00D1 6E00		LDPK	0
0296 00D2 7F89		ZAC	
0297 00D3 6A7F		LT	127
0298 00D4 6D02		MPY	2 * EMB(N-7)*P(3)
0299 *			
0300 00D5 6C7E		LTA	126
0301 00D6 6D06		MPY	6 * + EMB(N-6)*P(7)
0302 *			
0303 00D7 6C7D		LTA	125
0304 00D8 6D0A		MPY	10 * + EMB(N-5)*P(11)
0305 *			
0306 00D9 6C7C		LTA	124
0307 00DA 6D0E		MPY	14 * + EMB(N-4)*P(15)
0308 *			
0309 00D8 6C7B		LTA	123
0310 00DC 6D0D		MPY	13 * + EMB(N-3)*P(14)
0311 *			
0312 00DD 6C7A		LTA	122
0313 00DE 6D09		MPY	9 * + EMB(N-2)*P(10)
0314 *			
0315 00DF 6C79		LTA	121
0316 00E0 6D05		MPY	5 * + EMB(N-1)*P(6)
0317 *			
0318 00E1 6C78		LTA	120
0319 00E2 6D01		MPY	1 * + EMB(N)*P(2)
0320 00E3 7F8F		APAC	
0321 *			
0322 00E4 5030		SACL	61 *STORE EVEN PULSE SAMPLE IN DMA 61
0323 00E5 7004		LARK	0,4 *SET FLAG SO WE KNOW WHERE WE ARE IN
0324 00E6 7169		LARK	1,105 *SET POINTER TO LAST VALUES IN FILTE
0325 00E7 6881		LARP	1 *SELECT POINTER.
0326 *			
0327 00E8 F900 00E9 0195	B	FILTER	*BRANCH TO HI PASS FILTER.
0328 *			
0329 *			
0330 *			THIRD OUTPUT OF FOUR ODD OUTPUTS

0331	*				
0332	00EA F600	FOUR	B102	LOOP3	* WAIT UNTIL READY FOR OUTPUT
	00EB 00EE				
0333	00EC F900		B	FOUR	
	00ED 00EA				
0334	*				
0335	00EE 4A0D	LOOP3	OUT	13,2	*OUTPUT DELAYED ODD SAMPLE TO PORT 2
0336	00EF 4B0A		OUT	10,3	*OUTPUT EVEN SAMPLE TO PORT 3.
0337	*				
0338	00F0 6E00		LDPK	0	
0339	00F1 7F89		ZAC		
0340	00F2 6A77		LT	119	
0341	00F3 6001		MPY	1	* OMB(N-7)*P(2)
0342	*				
0343	00F4 6C76		LTA	118	
0344	00F5 6005		MPY	5	* + OMB(N-6)*P(6)
0345	*				
0346	00F6 6C75		LTA	117	
0347	00F7 6009		MPY	9	* + OMB(N-5)*P(10)
0348	*				
0349	00F8 6C74		LTA	116	
0350	00F9 6D0D		MPY	13	* + OMB(N-4)*P(14)
0351	*				
0352	00FA 6C73		LTA	115	
0353	00FB 600E		MPY	14	* + OMB(N-3)*P(15)
0354	*				
0355	00FC 6C72		LTA	114	
0356	00FD 600A		MPY	10	* + OMB(N-2)*P(11)
0357	*				
0358	00FE 6C71		LTA	113	
0359	00FF 6006		MPY	6	* + OMB(N-1)*P(7)
0360	*				
0361	0100 6C70		LTA	112	
0362	0101 6002		MPY	2	* + OMB(N)*P(3)
0363	0102 7F8F		APAC		
0364	*				
0365	0103 5010		SACL	16	* STORE RESULT DRC(M) IN DMA 16
0366	0104 7003		LARK	0,3	*SET FLAG TO MARK WHERE WE ARE IN PU
0367	0105 713C		LARK	1,60	*SET POINTER TO LAST VALUE IN FILTER
0368	0106 6881		LARP	1	*SELECT POINTER.
0369	*				
0370	0107 F900		B	FILTER	* BRANCH TO HIGH PASS FILTER
	0108 0195				
0371	*				
0372	*	THIRD	OUT OF FOUR EVEN OUTPUTS		
0373	*				
0374	0109 690C	THIRD	DMOV	12	*SHIFT ODD OUTPUTS THRU DELAY BUFFER
0375	010A 6908		DMOV	11	
0376	010B 690A		DMOV	10	
0377	010C 6E00		LDPK	0	
0378	010D 7F89		ZAC		
0379	010E 6A7F		LT	127	
0380	010F 6001		MPY	1	* EMB(N-7)*P(2)
0381	*				
0382	0110 6C7E		LTA	126	
0383	0111 6D05		MPY	5	* + EMB(N-6)*P(6)
0384	*				

0385 0112 6C7D	LTA	125	
0386 0113 6D09	MPY	9	* + EMB(N-5)*P(10)
0387 *			
0388 0114 6C7C	LTA	124	
0389 0115 6D0D	MPY	13	* + EMB(N-4)*P(14)
0390 *			
0391 0116 6C7B	LTA	123	
0392 0117 6D0E	MPY	14	* + EMB(N-3)*P(15)
0393 *			
0394 0118 6C7A	LTA	122	
0395 0119 6D0A	MPY	10	* + EMB(N-2)*P(11)
0396 *			
0397 011A 6C79	LTA	121	
0398 011B 6D06	MPY	6	* + EMB(N-1)*P(7)
0399 *			
0400 011C 6C78	LTA	120	
0401 011D 6D02	MPY	2	* + EMB(N)*P(3)
0402 011E 7F8F	APAC		
0403 *			
0404 011F 503D	SACL	61	*STORE EVEN PULSE SAMPLE IN 61
0405 0120 7002	LARK	0,2	*SET FLAG TO MARK WHERE WE ARE IN PU
0406 0121 7169	LARK	1,105	*SET POINTER TO LAST VALUE IN FILTER
0407 0122 6881	LARP	1	*SELECT POINTER.
0408 *			
0409 0123 F900	B	FILTER	*BRANCH TO HI PASS FILTER SECTION.
0124 0195			
0410 *			
0411 *			
0412 *			FOURTH ODD OUTPUT OF FOUR.
0413 *			
0414 0125 F600	TWO	BICZ	LOOP4 *WAIT UNTIL READY FOR OUTPUT
0126 0129			
0415 0127 F900	B	TWO	
0128 0125			
0416 *			
0417 0129 4A0D	LOOP4	OUT	13,2 *OUTPUT DELAYED ODD SAMPLE TO PORT 2
0418 012A 480A		OUT	10,3 *OUTPUT EVEN SAMPLE TO PORT 3.
0419 *			
0420 012B 6E00	LDPK	0	
0421 012C 7F89	ZAC		
0422 012D 6A77	LT	119	
0423 012E 6000	MPY	0	* OMB(N-7)*P(1)
0424 *			
0425 012F 6C76	LTA	118	
0426 0130 6D04	MPY	4	* + OMB(N-6)*P(5)
0427 *			
0428 0131 6C75	LTA	117	
0429 0132 6D08	MPY	8	* + OMB(N-5)*P(9)
0430 *			
0431 0133 6C74	LTA	116	
0432 0134 6D0C	MPY	12	* + OMB(N-4)*P(13)
0433 *			
0434 0135 6C73	LTA	115	
0435 0136 6D0F	MPY	15	* + OMB(N-3)*P(16)
0436 *			
0437 0137 6C72	LTA	114	
0438 0138 6D0B	MPY	11	* + OMB(N-2)*P(12)

0439 *
0440 0139 6C71 LTA 113
0441 013A 6007 MPY 7 * + DMB(N-1)*P(8)
0442 *
0443 013B 6C70 LTA 112
0444 013C 6003 MPY 3 * + DMB(N)*P(4)
0445 013D 7F8F APAC
0446 *
0447 013E 5010 SACL 16 * STORE RESULT ORC(M) IN DMA 16
0448 013F 7001 LARK 0,1 *SET FLAG TO MARK WHERE WE ARE IN PU
0449 0140 713C LARK 1,60 *SET POINTER TO LAST VALUE IN FILTER
0450 0141 6881 LARP 1 *SELECT POINTER.
0451 *
0452 0142 F900 8 FILTER * BRANCH TO HIGH PASS FILTER.
0143 0195
0453 *
0454 * FOURTH EVEN OUTPUT OUT OF FOUR.
0455 *
0456 0144 690C ONE DMOV 12 *SHIFT ODD OUTPUTS THRU DELAY BUFFER
0457 0145 690B DMOV 11
0458 0146 690A DMOV 10
0459 0147 6E00 LDPK 0
0460 0148 7F89 ZAC
0461 0149 6A7F LT 127
0462 014A 6000 MPY 0 * EMB(N-7)*P(1)
0463 *
0464 014B 6C7E LTA 126
0465 014C 6D04 MPY 4 * + EMB(N-6)*P(5)
0466 *
0467 014D 6C7D LTA 125
0468 014E 6D08 MPY 8 * + EMB(N-5)*P(9)
0469 *
0470 014F 6C7C LTA 124
0471 0150 6D0C MPY 12 * + EMB(N-4)*P(13)
0472 *
0473 0151 6C78 LTA 123
0474 0152 6D0F MPY 15 * + EMB(N-3)*P(6)
0475 *
0476 0153 6C7A LTA 122
0477 0154 6D08 MPY 11 * + EMB(N-2)*P(12)
0478 *
0479 0155 6C79 LTA 121
0480 0156 6007 MPY 7 * + EMB(N-1)*P(8)
0481 *
0482 0157 6C78 LTA 120
0483 0158 6D03 MPY 3 * + EMB(N)*P(4)
0484 0159 7F8F APAC
0485 *
0486 015A 503D SACL 61 *STORE EVEN SAMPLE ERCC(N) IN DMA 61
0487 015B 7000 LARK 0,0 *SET FLAG TO MARK WHERE WE ARE IN PU
0488 015C 7169 LARK 1,105 *SET POINTER TO LAST VALUE IN FILTER
0489 015D 6881 LARP 1 *SELECT POINTER.
0490 *
0491 015E F900 8 FILTER *BRANCH TO HI PASS FILTER.
015F 0195
0492 *
0493 *

0494 * NOW, MOVE INPUT BUFFER TO PREPARE FOR NEXT INCOMING MAN. B
0495 *
0496 0160 6E00 PREP LDPK 0
0497 0161 6976 DMOV 118 * MOVE FIRST SEVEN VALUES OF MANCHES
0498 0162 6975 DMOV 117 * BIT BUFFERS UP ONE MEMORY LOCATION
0499 0163 6974 DMOV 116 * MAKE ROOM FOR MOST RECENT CODE BIT
0500 0164 6973 DMOV 115 * FOR NEXT PULSE SHAPING SEQUENCE.
0501 0165 6972 DMOV 114
0502 0166 6971 DMOV 113
0503 0167 6970 DMOV 112
0504 0168 697E DMOV 126
0505 0169 697D DMOV 125
0506 016A 697C DMOV 124
0507 016B 6978 DMOV 123
0508 016C 697A DMOV 122
0509 016D 6979 DMOV 121
0510 016E 6978 DMOV 120
0511 *
0512 *
0513 * WE ARE READY FOR NEXT ITERATION OF FOUR OUTPUTS CORRESPON
0514 * TO NEXT MANCHESTER BIT. CHECK COUNTER TO SEE IF WE NEED N
0515 * DATA BIT.
0516 *
0517 016F 6E01 LDPK 1
0518 0170 2007 LAC 7 *CHECK MCOUNT. ADD -1 TO COUNTER.
0519 0171 0005 ADD 5 * STORE RESULT AS MCOUNT
0520 0172 5007 SACL 7
0521 *
0522 * IF WE HAVE LOOPED ONCE, WE NEED TO LOAD SECOND MAN. BIT.
0523 * IF WE HAVE LOOPED TWICE, WE NEED TO INPUT A NEW DATA BIT.
0524 *
0525 0173 FF00 BZ LOAD *IF MCOUNT IS NOW ZERO, WE HAVE MOST
0526 0174 0181 * RECENT MAN. BITS ALREADY,
0527 * SO SKIP FOLLOWING INPUT SEQUENCE
0528 *
0529 0175 F600 WAITS BIOZ LOOPS * WAIT FOR CLOCK
0530 0177 F900 B WAITS
0531 0178 0175 *
0532 0179 4A0D LOOPS OUT 13,2 * OUTPUT DELAYED ODD SAMPLE TO PORT 2
0533 017A 4B0A OUT 10,3 * OUTPUT EVEN SAMPLE TO PORT 3.
0534 *
0535 017B 4104 IN 4,1 * INPUT NEXT EVEN DATA BIT FROM PORT
0536 017C 7E01 LACK 1
0537 017D 7904 AND 4 * AND WITH +1 TO OBTAIN 0 OR 1 FOR D
0538 017E 5004 SACL 4 * STORE DATA BIT IN DMA 132.
0539 *
0540 017F F900 B MAN * BRANCH TO MANCHESTER CODING SECTION
0541 0180 0057 *
0542 * IF ZERO, THEN LOAD NEXT MANCHESTER BITS INTO BUFFER,
0543 * INPUT NEXT ODD DATA BIT,
0544 * AND LOOP BACK TO BEGIN PULSE SHAPING AGAIN.
0545 *
0546 0181 2000 LOAD LAC 0 * MOVE OMB(N+1) TO DMA 112

0547 0182 6E00	LDPK	0	* WHERE IT WILL BE READY FOR
0548 0183 5070	SACL	112	* NEXT PASS THRU PULSE SHAPING.
0549 0184 6E01	LDPK	1	
0550 0185 2001	LAC	1	* MOVE EMB(N+1) TO DMA 120
0551 0186 6E00	LDPK	0	* WHERE IT WILL BE READY FOR
0552 0187 5078	SACL	120	* NEXT PASS THRU PULSE SHAPING.
0553 0188 6E01	LDPK	1	
0554 *			
0555 0189 F600	WAIT6	BIOZ	LOOP6 * WAIT FOR CLOCK
018A 018D			
0556 0188 F900	B		WAIT6
018C 0189			
0557 *			
0558 018D 4A0D	LOOP6	OUT	13,2 * OUTPUT DELAYED ODD SAMPLE TO PORT 2
0559 018E 480A		OUT	10,3 * OUTPUT EVEN SAMPLE TO PORT 3
0560 *			
0561 018F 4103	IN	3,1	* INPUT FROM PORT 1.
0562 0190 7E01	LACK	1	
0563 0191 7903	AND	3	* AND WITH 1 TO PRODUCE A 1 OR A 0.
0564 0192 5003	SACL	3	* STORE RESULTING DATA BIT IN DMA 131
0565 *			
0566 0193 F900	B	MAIN1	* BRANCH TO BEGINNING OF PULSE SHAPI
0194 007A			
0567 *			
0568 *			THIS SECTION CONTAINS CODE FOR HI PASS FILTER.
0569 *			PREVIOUS 45 FUNCTION VALUES, RCC(M) - RCC(M-45) IN
0570 *			MEMORY LOCATIONS 16-60 FOR THE ODD STREAM AND IN 61-
0571 *			FOR THE EVEN STREAM. THE OLDEST VALUE IS POINTED TO
0572 *			THIS POINT BY AUX1. THE COEFFICIENTS ARE
0573 *			SD CONSTANTS, SCALED BY 4096.
0574 *			
0575 *			NOW START FIR FILTER .
0576 *			
0577 0195 7F89	FILTER	ZAC	
0578 0196 6A98	LT	*-	
0579 0197 9F80	MPYK	-115	* RCC(M-44)*-115
0580 *			
0581 0198 6B98	LTD	*-	
0582 0199 9F0E	MPYK	-34	* + RCC(M-43)*-34
0583 *			
0584 019A 6B98	LTD	*-	
0585 019B 9FD9	MPYK	-39	* + RCC(M-42)*-39
0586 *			
0587 019C 6B98	LTD	*-	
0588 019D 9FD5	MPYK	-43	* + RCC(M-41)*-43
0589 *			
0590 019E 6B98	LTD	*-	
0591 019F 9F00	MPYK	-48	* + RCC(M-40)*-48
0592 *			
0593 01A0 6B98	LTD	*-	
0594 01A1 9FC8	MPYK	-53	* + RCC(M-39)*-53
0595 *			
0596 01A2 6B98	LTD	*-	
0597 01A3 9FC6	MPYK	-58	* + RCC(M-38)*-58
0598 *			
0599 01A4 6B98	LTD	*-	
0600 01A5 9FC1	MPYK	-63	* + RCC(M-37)*-63

0601	*			
0602	01A6 6B98	LTD	*-	
0603	01A7 9FBC	MPYK	-68	* + RCC(M-36)*-68
0604	*			
0605	01A8 6B98	LTD	*-	
0606	01A9 9FB7	MPYK	-73	* + RCC(M-35)*-73
0607	*			
0608	01AA 6B98	LTD	*-	
0609	01AB 9FB2	MPYK	-78	* + RCC(M-34)*-78
0610	*			
0611	01AC 6B98	LTD	*-	
0612	01AD 9FAD	MPYK	-83	* + RCC(M-33)*-83
0613	*			
0614	01AE 6B98	LTD	*-	
0615	01AF 9FA9	MPYK	-87	* + RCC(M-32)*-87
0616	*			
0617	01B0 6B98	LTD	*-	
0618	01B1 9FA4	MPYK	-92	* + RCC(M-31)*-92
0619	*			
0620	01B2 6B98	LTD	*-	
0621	01B3 9FA1	MPYK	-95	* + RCC(M-30)*-95
0622	*			
0623	01B4 6B98	LTD	*-	
0624	01B5 9F9D	MPYK	-99	* + RCC(M-29)*-99
0625	*			
0626	01B6 6B98	LTD	*-	
0627	01B7 9F9A	MPYK	-102	* + RCC(M-28)*-102
0628	*			
0629	01B8 6B98	LTD	*-	
0630	01B9 9F98	MPYK	-104	* + RCC(M-27)*-104
0631	*			
0632	01BA 6B98	LTD	*-	
0633	01BB 9F95	MPYK	-107	* + RCC(M-26)*-107
0634	*			
0635	01BC 6B98	LTD	*-	
0636	01BD 9F93	MPYK	-109	* + RCC(M-25)*-109
0637	*			
0638	01BE 6B98	LTD	*-	
0639	01BF 9F92	MPYK	-110	* + RCC(M-24)*-110
0640	*			
0641	01C0 6B98	LTD	*-	
0642	01C1 9F91	MPYK	-111	* + RCC(M-23)*-111
0643	*			
0644	01C2 6B98	LTD	*-	
0645	01C3 8F91	MPYK	3985	* + RCC(M-22)*3985
0646	*			
0647	01C4 6B98	LTD	*-	
0648	01C5 9F91	MPYK	-111	* + RCC(M-21)*-111
0649	*			
0650	01C6 6B98	LTD	*-	
0651	01C7 9F92	MPYK	-110	* + RCC(M-20)*-110
0652	*			
0653	01C8 6B98	LTD	*-	
0654	01C9 9F93	MPYK	-109	* + RCC(M-19)*-109
0655	*			
0656	01CA 6B98	LTD	*-	
0657	01CB 9F95	MPYK	-107	* + RCC(M-18)*-107

0658	*			
0659	01CC 6898	LTD	*-	
0660	01CD 9F98	MPYK	-104	* + RCC(M-17)*-104
0661	*			
0662	01CE 6898	LTD	*-	
0663	01CF 9F9A	MPYK	-102	* + RCC(M-16)*-102
0664	*			
0665	01D0 6898	LTD	*-	
0666	01D1 9F90	MPYK	-99	* + RCC(M-15)*-99
0667	*			
0668	01D2 6898	LTD	*-	
0669	01D3 9FA1	MPYK	-95	* + RCC(M-14)*-95
0670	*			
0671	01D4 6898	LTD	*-	
0672	01D5 9FA4	MPYK	-92	* + RCC(M-13)*-92
0673	*			
0674	01D6 6898	LTD	*-	
0675	01D7 9FA9	MPYK	-87	* + RCC(M-12)*-87
0676	*			
0677	01D8 6898	LTD	*-	
0678	01D9 9FAD	MPYK	-83	* + RCC(M-11)*-83
0679	*			
0680	01DA 6898	LTD	*-	
0681	01D8 9FB2	MPYK	-78	* + RCC(M-10)*-78
0682	*			
0683	01DC 6898	LTD	*-	
0684	01DD 9FB7	MPYK	-73	* + RCC(M-9)*-73
0685	*			
0686	01DE 6898	LTD	*-	
0687	01DF 9FBC	MPYK	-68	* + RCC(M-8)*-68
0688	*			
0689	01E0 6898	LTD	*-	
0690	01E1 9FC1	MPYK	-63	* + RCC(M-7)*-63
0691	*			
0692	01E2 6898	LTD	*-	
0693	01E3 9FC6	MPYK	-58	* + RCC(M-6)*-58
0694	*			
0695	01E4 6898	LTD	*-	
0696	01E5 9FC8	MPYK	-53	* + RCC(M-5)*-53
0697	*			
0698	01E6 6898	LTD	*-	
0699	01E7 9FD0	MPYK	-48	* + RCC(M-4)*-48
0700	*			
0701	01E8 6898	LTD	*-	
0702	01E9 9FD5	MPYK	-43	* + RCC(M-3)*-43
0703	*			
0704	01EA 6898	LTD	*-	
0705	01EB 9FD9	MPYK	-39	* + RCC(M-2)*-39
0706	*			
0707	01EC 6898	LTD	*-	
0708	01ED 9FDE	MPYK	-34	* + RCC(M-1)*-34
0709	*			
0710	01EE 6898	LTD	*-	
0711	01EF 9F8D	MPYK	-115	* + RCC(M)*-115
0712	01F0 7F8F	APAC		
0713	*			
0714	01F1 6E01	LDPK	1	

0715 01F2 5C0A SACH 10,4 *STORE FILTER OUTPUT IN 138
0716 * SHIFTED 4 SPOTS TO TAKE INTO ACCOUNT
0717 * MULT. OF 13 BIT NO. BY 16 BIT NO.
0718 01F3 200A LAC 10
0719 01F4 0006 ADD 6 * ADD BIAS TERM TO READY FOR OUTPUT
0720 * AND 15
0721 01F5 500A SACL 10 * STORE FILTER OUT + BIAS IN 138
0722 *
0723 * CHECK OCOUNT TO SEE WHICH OUTPUT WE SHOULD BRANCH BACK
0724 *
0725 01F6 300E SAR 0,14
0726 01F7 200E LAC 14
0727 *
0728 * IF ACC. IS ZERO, WE ARE DONE AND READY FOR NEXT ITERATION
0729 *
0730 01F8 FF00 BZ PREP
01F9 0160
0731 *
0732 01FA 0005 ADD 5
0733 *
0734 * IF ZERO NOW, READY FOR FOURTH EVEN OUTPUT
0735 *
0736 01FB FF00 BZ ONE
01FC 0144
0737 *
0738 01FD 0005 ADD 5
0739 *
0740 * IF ZERO, READY FOR FOURTH ODD OUTPUT
0741 *
0742 01FE FF00 BZ TWO
01FF 0125
0743 *
0744 0200 0005 ADD 5
0745 *
0746 * IF ZERO, READY FOR THIRD EVEN OUTPUT
0747 *
0748 0201 FF00 BZ THIRD
0202 0109
0749 *
0750 0203 0005 ADD 5
0751 *
0752 * IF ZERO, READY FOR THIRD ODD OUTPUT
0753 *
0754 0204 FF00 BZ FOUR
0205 00EA
0755 *
0756 0206 0005 ADD 5
0757 *
0758 * IF ZERO, READY FOR SECOND EVEN OUTPUT
0759 *
0760 0207 FF00 BZ FIVE
0208 00CE
0761 *
0762 0209 0005 ADD 5
0763 *
0764 * IF ZERO, READY FOR SECOND ODD OUTPUT
0765 *

0766 020A FF00 BZ SIX
020B 00AF
0767 *
0768 * IF ONE, READY FOR FIRST EVEN OUTPUT
0769 *
0770 020C FC00 BGZ SEVEN
020D 0093
0771 *
0772 *
0773 * BOOT ROUTINE FOR LOADING PROGRAM
0774 * MEMORY FROM EPROM TO RAM
0775 *
0776 020E 7E01 BOOT LACK >1
0777 020F 5000 SACL >0
0778 0210 6A00 LT >0
0779 0211 8700 MPYK >700
0780 0212 7F8E PAC
0781 *
0782 0213 670A NOTDUN TBLR >A
0783 0214 700A TBLW >A
0784 0215 1000 SUB >0
0785 0216 F000 BGEZ NOTDUN
0217 0213
0786 *
0787 0218 8024 MPYK RESET
0788 0219 7F8E PAC
0789 021A 500A SACL >A
0790 021B 7E01 LACK >1
0791 021C 7D0A TBLW >A
0792 021D F900 S RESET
021E 0024
0793 *
0794 END

0 ERRORS, NO WARNINGS

APPENDIX III

TMS320 MCCT DEMODULATOR PROCESSING SOFTWARE

0001 ICT "DEMPROC"
 0002 *****
 0003 *
 0004 * SOFTWARE FOR BOARD 2 OF THE REAL TIME
 0005 * IMPLEMENTATION OF THE MANCHESTER TCT
 0006 * DEMODULATOR
 0007 *
 0008 * Written by - Norman E. Lay
 0009 * Last Updated : 8/30/85
 0010 *
 0011 * General Electric Company
 0012 * Corporate Research & Development
 0013 * Schenectady, N.Y.
 0014 *
 0015 *-----*
 0016 *
 0017 * The following TMS-320 assembler code
 0018 * implements the pilot processing and
 0019 * correction to the data channels of phase
 0020 * irregularities caused by the fading chan-
 0021 * nel. The principal processing intensive
 0022 * functions implemented by this code consist
 0023 * of 4 lowpass filters -- 2 for pilot reco-
 0024 * very in each channel and 2 for filtering
 0025 * excess noise from the data band. The pilot
 0026 * processor consists of determining sine &
 0027 * cosine of the phase angle between the I & Q
 0028 * channels of the recovered pilot. One octant
 0029 * of sine and cosine values are stored as a
 0030 * lookup table in program memory. Linear in-
 0031 * terpolation is used at different processing
 0032 * rate boundaries (i.e. where the pilot is
 0033 * removed from the data and where sin & cos
 0034 * are used to correct for phase errors in the
 0035 * data). The data filters operate at a 12kHz
 0036 * rate and the pilot processing is done at a
 0037 * 2.4kHz rate.
 0038 *
 0039 *-----*
 0040 *
 0041 * 1st Data Page Ram
 0042 *
 0043 0000 ILPF EQU >0 }
 0044 0001 IZ1 EQU >1 } Beginning of Ram for
 0045 0002 IZ2 EQU >2 } Delay Storage of Filter
 0046 0003 IZ3 EQU >3 } States of the I Channel
 0047 0004 IZ4 EQU >4 } Data LPF
 0048 0005 IZ5 EQU >5 }
 0049 0006 IZ6 EQU >6 }
 0050 0007 IZ7 EQU >7 }
 0051 0008 IZ8 EQU >8 }
 0052 0009 IZ9 EQU >9 }
 0053 000A IZ10 EQU >A }
 0054 000B IZ11 EQU >B }
 0055 000C IZ12 EQU >C }
 0056 000D IZ13 EQU >D }
 0057 000E IZ14 EQU >E }

0058	000F	I215	EQU	>F	>	.
0059	0010	I216	EQU	>10	>	.
0060	0011	I217	EQU	>11	>	.
0061	0012	I218	EQU	>12	>	.
0062	0013	I219	EQU	>13	>	.
0063	0014	I220	EQU	>14	>	.
0064	0015	I221	EQU	>15	>	.
0065	0016	I222	EQU	>16	>	.
0066	0017	I223	EQU	>17	>	.
0067	0018	I224	EQU	>18	>	.
0068	0019	I225	EQU	>19	>	.
0069	001A	I226	EQU	>1A	>	.
0070	001B	I227	EQU	>1B	>	.
0071	001C	I228	EQU	>1C	>	.
0072	001D	I229	EQU	>1D	>	.
0073	001E	I230	EQU	>1E	>	.
0074	001F	I231	EQU	>1F	>	.
0075	0020	I232	EQU	>20	>	.
0076	0021	I233	EQU	>21	>	.
0077	0022	I234	EQU	>22	>	.
0078	0023	I235	EQU	>23	>	.
0079	0024	I236	EQU	>24	>	.
0080	0025	I237	EQU	>25	>	.
0081	0026	I238	EQU	>26	>	.
0082	0027	I239	EQU	>27	>	End of I Data LPF
0083	0028	I240	EQU	>28	>	Delay Storage
0084	*					
0085	0029	CLPF	EQU	>29	>	
0086	002A	QZ1	EQU	>2A	>	Beginning of Ram for
0087	002B	QZ2	EQU	>2B	>	Delay Storage of Filter
0088	002C	QZ3	EQU	>2C	>	States of the Q Channel
0089	002D	QZ4	EQU	>2D	>	Data LPF
0090	002E	QZ5	EQU	>2E	>	.
0091	002F	QZ6	EQU	>2F	>	.
0092	0030	QZ7	EQU	>30	>	.
0093	0031	QZ8	EQU	>31	>	.
0094	0032	QZ9	EQU	>32	>	.
0095	0033	QZ10	EQU	>33	>	.
0096	0034	QZ11	EQU	>34	>	.
0097	0035	QZ12	EQU	>35	>	.
0098	0036	QZ13	EQU	>36	>	.
0099	0037	QZ14	EQU	>37	>	.
0100	0038	QZ15	EQU	>38	>	.
0101	0039	QZ16	EQU	>39	>	.
0102	003A	QZ17	EQU	>3A	>	.
0103	003B	QZ18	EQU	>3B	>	.
0104	003C	QZ19	EQU	>3C	>	.
0105	003D	QZ20	EQU	>3D	>	.
0106	003E	QZ21	EQU	>3E	>	.
0107	003F	QZ22	EQU	>3F	>	.
0108	0040	QZ23	EQU	>40	>	.
0109	0041	QZ24	EQU	>41	>	.
0110	0042	QZ25	EQU	>42	>	.
0111	0043	QZ26	EQU	>43	>	.
0112	0044	QZ27	EQU	>44	>	.
0113	0045	QZ28	EQU	>45	>	.
0114	0046	QZ29	EQU	>46	>	.

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0115	0047	CZ30	EQU	>47	>	.
0116	0048	CZ31	EQU	>48	>	.
0117	0049	CZ32	EQU	>49	>	.
0118	004A	CZ33	EQU	>4A	>	.
0119	004B	CZ34	EQU	>4B	>	.
0120	004C	CZ35	EQU	>4C	>	.
0121	004D	CZ36	EQU	>4D	>	.
0122	004E	CZ37	EQU	>4E	>	.
0123	004F	CZ38	EQU	>4F	>	.
0124	0050	CZ39	EQU	>50	>	End of C Data LPF
0125	0051	CZ40	EQU	>51	>	Delay Storage
0126	*					
0127	0052	IDATA	EQU	>52	>	Ram for storing I & Q
0128	0053	QDATA	EQU	>53	>	input data
0129	*					
0130	0054	IBUFF	EQU	>54	>	Input data buffer to
0131	0059	CBUFF	EQU	>59	>	permit pilot processing
0132	*					
0133	005E	SIN	EQU	>5E	>	Sine calculation
0134	005F	PRESIN	EQU	>5F	>	Save for sine lin. interp.
0135	0060	GLDSIN	EQU	>60	>	Use as sine in interrupt
0136	0061	COS	EQU	>61	>	Cosine calculation
0137	0062	PRECCS	EQU	>62	>	Save for cosine lin. interp.
0138	0063	GLOCOS	EQU	>63	>	Use as cosine in interrupt
0139	0064	SINSTP	EQU	>64	>	Sine step size calc.
0140	0065	OSSTF	EQU	>65	>	Use in intrpt. as step size
0141	0066	COSSTP	EQU	>66	>	Cosine step size calc.
0142	0067	CCSTF	EQU	>67	>	Use in intrpt. as step size
0143	*					
0144	0068	IPILOT	EQU	>68	>	Input I pilot
0145	0069	OLDIF	EQU	>69	>	Save for I lin. interp.
0146	006A	OIPIL	EQU	>6A	>	Use as I pilot in interrupt
0147	006B	CPILOT	EQU	>6B	>	Input Q pilot
0148	006C	OLDQF	EQU	>6C	>	Save for Q pilot lin. interp.
0149	006D	OQPIL	EQU	>6D	>	Use as Q pilot in intrpt.
0150	006E	IPSTF	EQU	>6E	>	I pilot step size calc.
0151	006F	OIPSTP	EQU	>6F	>	Use in intrpt. as step size
0152	0070	QPSTF	EQU	>70	>	Q pilot step size calc.
0153	0071	OQPSTP	EQU	>71	>	Use in intrpt. as step size
0154	*					
0155	0072	CNE	EQU	>72	>	Constant = 5
0156	0073	SNCFLG	EQU	>73	>	Flag for pilot/data alignment
0157	0074	TEMP1	EQU	>74	>	Temp ram used in background
0158	0075	TEMP2	EQU	>75	>	"
0159	0076	SINMI	EQU	>76	>	Temp ram used in interrupt
0160	0077	SINMC	EQU	>77	>	"
0161	0078	IDOUT	EQU	>78	>	I data output
0162	0079	QDOUT	EQU	>79	>	Q data output
0163	007A	SNOFST	EQU	>7A	>	Table offset for stored sine
0164	007A	CSCFST	EQU	>7A	>	and cosine values
0165	007B	ISIGN	EQU	>7B	>	Temp ram used in background
0166	007C	QSIGN	EQU	>7C	>	"
0167	*					
0168	*					Ram for Saving Registers
0169	*					During an Interrupt
0170	*					
0171	007D	IACH	EQU	>7D	>	Save high accumulator

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0172	007E	IACL	EQU	>7E	>	Save low accumulator
0173	007F	ITREG	EQU	>7F	>	Save T register
0174	*					
0175	*					Address Constant for Sine
0176	*					and Cosine Lookup Table
0177	*					
0178	0500	OFFSET	EQU	>500		ORIGINAL PAGE IS OF POOR QUALITY.
0179	*					
0180	*					Data LPF Constants
0181	*					
0182	*					Only half the coefficients are coded because
0183	*					the filter is symmetrical.
0184	*					
0185	FFD8	CLPF1	EQU	-37		
0186	FFE7	CLPF2	EQU	-25		
0187	006C	CLPF3	EQU	108		
0188	FFFF	CLPF4	EQU	-1		
0189	FFD4	CLPF5	EQU	-44		
0190	FFA6	CLPF6	EQU	-90		
0191	FFF8	CLPF7	EQU	-8		
0192	0068	CLPF8	EQU	104		
0193	0078	CLPF9	EQU	120		
0194	FFE0	CLPF10	EQU	-26		
0195	FF44	CLPF11	EQU	-188		
0196	FF67	CLPF12	EQU	-153		
0197	0068	CLPF13	EQU	107		
0198	0144	CLPF14	EQU	324		
0199	0085	CLPF15	EQU	181		
0200	FEDA	CLPF16	EQU	-294		
0201	FD9E	CLPF17	EQU	-610		
0202	FF38	CLPF18	EQU	-200		
0203	03E9	CLPF19	EQU	1001		
0204	092C	CLPF20	EQU	2348		
0205	0879	CLPF21	EQU	2937		
0206	*					
0207	*					Pilot LPF Constants
0208	*					
0209	*					Only half the coefficients are coded because
0210	*					the filter is symmetrical.
0211	*					
0212	FF34	PLPF1	EQU	-204		
0213	FFE6	PLPF2	EQU	-26		
0214	FFF6	PLPF3	EQU	-10		
0215	0011	PLPF4	EQU	17		
0216	0036	PLPF5	EQU	54		
0217	0060	PLPF6	EQU	96		
0218	0088	PLPF7	EQU	139		
0219	0080	PLPF8	EQU	176		
0220	00C8	PLPF9	EQU	200		
0221	00C8	PLPF10	EQU	203		
0222	00B4	PLPF11	EQU	180		
0223	0081	PLPF12	EQU	129		
0224	0031	PLPF13	EQU	49		
0225	FFC7	PLPF14	EQU	-57		
0226	FF40	PLPF15	EQU	-179		
0227	FEC0	PLPF16	EQU	-307		
0228	FE57	PLPF17	EQU	-425		

0229	FDFB	PLPF18	EQU	-517	
0230	FDCA	PLPF19	EQU	-566	
0231	FDD4	PLPF20	EQU	-556	
0232	FE27	PLPF21	EQU	-473	
0233	FECA	PLPF22	EQU	-310	ORIGINAL PAGE IS
0234	FFC1	PLPF23	EQU	-63	OF POOR QUALITY.
0235	0106	PLPF24	EQU	262	
0236	028E	PLPF25	EQU	654	
0237	0446	PLPF26	EQU	1094	
0238	0617	PLPF27	EQU	1559	
0239	07E5	PLPF28	EQU	2021	
0240	0994	PLPF29	EQU	2452	
0241	0806	PLPF30	EQU	2822	
0242	0C23	PLPF31	EQU	3107	
0243	0CD6	PLPF32	EQU	3286	
0244	0D13	PLPF33	EQU	3347	
0245	*				
0246	*				Begin TMS-320 Code
0247	*				
0248	0000		ACRG	>0	
0249	*				
0250	0000 F900		B	800T	
	0001 0700				
0251	*				
0252	*				Begin Interrupt Routine
0253	*				
0254	0002 587D	INTRFT	SACH	IACH	}
0255	0003 507E		SACL	IACL	} Save accumulator
0256	0004 8001		MPYK	>1	} and T register dur-
0257	0005 7F8E		PAC		} ing an interrupt.
0258	0006 507F		SACL	ITREG	}
0259	*				
0260	0007 4873		OUT	IDOUT,0	} Output recovered I
0261	0008 4979		OUT	QCOUT,1	} and Q data.
0262	0009 F600		BIOZ	NCSYNC	} Check for time alignment.
	000A 0020				
0263	*				
0264	000B 6961		DMOV	COS	} Update sin, cos, I pilot
0265	000C 6962		DMOV	PRECOS	} and Q pilot and all cor-
0266	000D 6966		DMOV	CCSSTP	} responding step sizes.
0267	000E 695E		DMOV	SIN	}
0268	000F 695F		DMOV	PRESIN	.
0269	0010 6964		DMOV	SINSTP	.
0270	0011 6968		DMOV	IPILOT	.
0271	0012 6969		DMOV	OLDIP	.
0272	0013 696E		DMOV	IPSTP	.
0273	0014 6963		DMOV	QPILOT	.
0274	0015 696C		DMOV	OLDDQP	.
0275	0016 6970		DMOV	QPSTP	} End of Update.
0276	*				
0277	0017 6972		DMOV	ONE	} Set SNCFLG.
0278	*				
0279	0018 4052		IN	ICATA,0	}
0280	0019 4153		IN	QCATA,1	} Input I & Q pilot and
0281	001A 4268		IN	IPILOT,2	} data streams.
0282	001B 4368		IN	QPILOT,3	}
0283	*				

0284 001C 7054 LARK 0,IBUFF } Reset processing delay
 0285 001C 7159 LARK 1,QBUFF } buffer pointers.
 0286 *
 0287 001E F900 B CONTNU
 001F 002E
 0288 *
 0289 0020 4052 NOSYNC IN IDATA,0 } Input I & Q data
 0290 0021 4153 IN QCATA,1 } streams. ORIGINAL PAGE IS
 0291 *
 0292 0022 656A ZALH CIPIL
 0293 0023 606F ADDH OIPSTP }
 0294 0024 586A SACH OIPIL } Update filtered pilot
 0295 0025 656D ZALH OCPIL } for linear interpolation.
 0296 0026 6071 ADDH OQPSTP }
 0297 0027 586D SACH OCPIL
 0298 0028 6563 ZALH OLDCOS
 0299 0029 6067 ADDH OCSTP }
 0300 002A 5863 SACH OLDCOS } Update sin & cos for
 0301 002B 6560 ZALH OLDSIN } linear interpolation.
 0302 002C 6065 ADDH OSSTP }
 0303 002D 5860 SACH OLDSIN
 0304 *
 0305 * The following section of code
 0306 * implements the equations :
 0307 *
 0308 * Zi = Id*cos(phi) + Qd*sin(phi)
 0309 * Zq = Cd*cos(phi) - Id*sin(phi)
 0310 *
 0311 002E 2088 CONTNU LAC * }
 0312 002F 106A SUB OIPIL } Remove pilot from I data.
 0313 0030 5088 SACL * }
 0314 0031 6A60 LT OLDSIN
 0315 0032 6D81 MPY *,1
 0316 0033 7F8E PAC
 0317 0034 5976 SACH SINMI,1
 0318 0035 2088 LAC * }
 0319 0036 106D SUB OCPIL } Remove pilot from Q data.
 0320 0037 5088 SACL * }
 0321 0038 6D80 MPY *,0
 0322 0039 7F8E PAC
 0323 003A 5977 SACH SINMQ,1
 0324 003B 6A63 LT OLDCOS
 0325 003C 6D81 MPY *,1
 0326 003D 7F8E PAC
 0327 003E 0F77 ADD SINMQ,15
 0328 003F 5800 SACH ILPF,0
 0329 0040 6D80 MPY *,0
 0330 0041 7F8E PAC
 0331 0042 1F76 SUB SINMI,15
 0332 0043 5829 SACH QLPF,0
 0333 *
 0334 0044 2052 LAC IDATA
 0335 0045 50A1 SACL **+,0,1 } Store Current Input
 0336 0046 2053 LAC QDATA } I & Q Data.
 0337 0047 50A0 SACL **+,0,0
 0338 *
 0339 * The following two LPFs are for

0340 * the removal of out of band noise
0341 * in both the I & Q data channels.
0342 *
0343 *
0344 * Data LPF Code I Channel
0345 *
0346 0048 7F89 ZAC
0347 0049 6A28 LT IZ40
0348 004A 9FD8 MPYK DLPF1
0349 004B 6B27 LTD IZ39
0350 004C 9FE7 MPYK DLPF2
0351 004D 6B26 LTD IZ38
0352 004E 806C MPYK DLPF3
0353 004F 6B25 LTD IZ37
0354 0050 9FFF MPYK DLPF4
0355 0051 6B24 LTD IZ36
0356 0052 9FD4 MPYK DLPF5
0357 0053 6B23 LTD IZ35
0358 0054 9FA6 MPYK DLPF6
0359 0055 6B22 LTD IZ34
0360 0056 9FF8 MPYK DLPF7
0361 0057 6B21 LTD IZ33
0362 0058 8068 MPYK DLPF8
0363 0059 6B20 LTD IZ32
0364 005A 8078 MPYK DLPF9
0365 005B 6B1F LTD IZ31
0366 005C 9FE6 MPYK DLPF10
0367 005D 6B1E LTD IZ30
0368 005E 9F44 MPYK DLPF11
0369 005F 6B1D LTD IZ29
0370 0060 9F67 MPYK DLPF12
0371 0061 6B1C LTD IZ28
0372 0062 806B MPYK DLPF13
0373 0063 6B13 LTD IZ27
0374 0064 8144 MPYK DLPF14
0375 0065 6B1A LTD IZ26
0376 0066 8085 MPYK DLPF15
0377 0067 6B19 LTD IZ25
0378 0068 9EDA MPYK DLPF16
0379 0069 6B18 LTD IZ24
0380 006A 9D9E MPYK DLPF17
0381 006B 6B17 LTD IZ23
0382 006C 9F38 MPYK DLPF18
0383 006D 6B16 LTD IZ22
0384 006E 83E9 MPYK DLPF19
0385 006F 6B15 LTD IZ21
0386 0070 892C MPYK DLPF20
0387 0071 6B14 LTD IZ20
0388 0072 8379 MPYK DLPF21
0389 0073 6B13 LTD IZ19
0390 0074 892C MPYK DLPF20
0391 0075 6B12 LTD IZ18
0392 0076 83E9 MPYK DLPF19
0393 0077 6B11 LTD IZ17
0394 0078 9F38 MPYK DLPF18
0395 0079 6B10 LTD IZ16
0396 007A 9D9E MPYK DLPF17

0397	007B	630F	LTD	IZ15
0398	007C	9EDA	MPYK	DLPF16
0399	007C	680E	LTD	IZ14
0400	007E	8065	MPYK	DLPF15
0401	007F	650D	LTD	IZ13
0402	0080	8144	MPYK	DLPF14
0403	0081	630C	LTD	IZ12
0404	0082	806B	MPYK	DLPF13
0405	0083	680B	LTD	IZ11
0406	0084	9F67	MPYK	DLPF12
0407	0085	680A	LTD	IZ10
0408	0086	9F44	MPYK	DLPF11
0409	0087	6809	LTD	IZ9
0410	0088	9FE6	MPYK	DLPF10
0411	0089	6808	LTD	IZ8
0412	008A	8078	MPYK	DLPF9
0413	008B	6807	LTD	IZ7
0414	008C	8063	MPYK	DLPF8
0415	008D	6806	LTD	IZ6
0416	008E	9FF8	MPYK	DLPF7
0417	008F	6805	LTD	IZ5
0418	0090	9FA6	MPYK	DLPF6
0419	0091	6804	LTD	IZ4
0420	0092	9FD4	MPYK	DLPF5
0421	0093	6803	LTD	IZ3
0422	0094	9FFF	MPYK	DLPF4
0423	0095	6802	LTD	IZ2
0424	0096	806C	MPYK	DLPF3
0425	0097	6801	LTD	IZ1
0426	0098	9FE7	MPYK	DLPF2
0427	0099	6800	LTD	ILPF
0428	009A	9FD3	MPYK	DLPF1
0429	009B	7F8F	APAC	
0430	009C	5C78	SACH	ICOUT,4

0431 *

0432 *

0433 *

Data LPF Code Q Channel

0434	009D	7F89	ZAC	
0435	009E	6A51	LT	QZ40
0436	009F	9FD3	MPYK	DLPF1
0437	00A0	6850	LTD	QZ39
0438	00A1	9FE7	MPYK	DLPF2
0439	00A2	684F	LTD	QZ38
0440	00A3	806C	MPYK	DLPF3
0441	00A4	684E	LTD	QZ37
0442	00A5	9FFF	MPYK	DLPF4
0443	00A6	684D	LTD	QZ36
0444	00A7	9FD4	MPYK	DLPF5
0445	00A8	684C	LTD	QZ35
0446	00A9	9FA6	MPYK	DLPF6
0447	00AA	684B	LTD	QZ34
0448	00AB	9FF8	MPYK	DLPF7
0449	00AC	684A	LTD	QZ33
0450	00AD	8068	MPYK	DLPF8
0451	00AE	6849	LTD	QZ32
0452	00AF	8078	MPYK	DLPF9
0453	00B0	6848	LTD	QZ31

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0454 0081 9FE6	MPYK	DLPF10
0455 0082 6B47	LTD	QZ30
0456 0083 9F44	MPYK	DLPF11
0457 0084 6B46	LTD	QZ29
0458 0085 9F67	MPYK	DLPF12
0459 0086 6B45	LTD	QZ28
0460 0087 8068	MPYK	DLPF13
0461 0088 6344	LTD	QZ27
0462 0089 8144	MPYK	DLPF14
0463 008A 6343	LTD	QZ26
0464 008B 80B5	MPYK	DLPF15
0465 008C 6B42	LTD	QZ25
0466 008D 9EDA	MPYK	DLPF16
0467 008E 6B41	LTD	QZ24
0468 00BF 9D9E	MPYK	DLPF17
0469 00C0 6B40	LTD	QZ23
0470 00C1 9F38	MPYK	DLPF18
0471 00C2 6B3F	LTD	QZ22
0472 00C3 83E9	MPYK	DLPF19
0473 00C4 6B3E	LTD	QZ21
0474 00C5 892C	MPYK	DLPF20
0475 00C6 6B3D	LTD	QZ20
0476 00C7 8879	MPYK	DLPF21
0477 00C8 6B3C	LTD	QZ19
0478 00C9 892C	MPYK	DLPF20
0479 00CA 6B3B	LTD	QZ18
0480 00CB 83E9	MPYK	DLPF19
0481 00CC 6B3A	LTD	QZ17
0482 00CD 9F38	MPYK	DLPF18
0483 00CE 6B39	LTD	QZ16
0484 00CF 9D9E	MPYK	DLPF17
0485 00D0 6B38	LTD	QZ15
0486 00D1 9EDA	MPYK	DLPF16
0487 00D2 6B37	LTD	QZ14
0488 00D3 80B5	MPYK	DLPF15
0489 00D4 6B36	LTD	QZ13
0490 00D5 8144	MPYK	DLPF14
0491 00D6 6B35	LTD	QZ12
0492 00D7 8068	MPYK	DLPF13
0493 00D8 6B34	LTD	QZ11
0494 00D9 9F67	MPYK	DLPF12
0495 00DA 6333	LTD	QZ10
0496 00DB 9F44	MPYK	DLPF11
0497 00DC 6B32	LTD	QZ9
0498 00DD 9FE6	MPYK	DLPF10
0499 00DE 6B31	LTD	QZ8
0500 00DF 8078	MPYK	DLPF9
0501 00E0 6330	LTD	QZ7
0502 00E1 8068	MPYK	DLPF8
0503 00E2 632F	LTD	QZ6
0504 00E3 9FF8	MPYK	DLPF7
0505 00E4 6B2E	LTD	QZ5
0506 00E5 9FA6	MPYK	DLPF6
0507 00E6 6B2D	LTD	QZ4
0508 00E7 9FD4	MPYK	DLPF5
0509 00E8 6B2C	LTD	QZ3
0510 00E9 9FFF	MPYK	DLPF4

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0511	00EA	6928	LTD	QZ2	
0512	00EB	806C	MPYK	DLPF3	
0513	00EC	682A	LTD	QZ1	
0514	00ED	9FE7	MPYK	DLPF2	
0515	00EE	6B29	LTD	QLPF	
0516	00EF	9FD5	MPYK	DLPF1	
0517	00F0	7F8F	APAC		
0518	00F1	5C79	SACH	QDCUT,4	
0519	*				
0520	*			Restore Registers	
0521	*				
0522	00F2	657D	ZALH	IACH	
0523	00F3	617E	ACDS	IACL	
0524	00F4	6A7F	LT	ITREG	
0525	*				
0526	00F5	7F82	EINT		
0527	00F6	7F8D	RET		
0528	*				
0529	*			Begin Background Code for	
0530	*			Calculation of I & Q Pilot	
0531	*			and Sin & Cos Step Sizes.	
0532	*			Perform Pilot LPF and Sin &	
0533	*			Cos Table Lookup.	
0534	*				
0535	00F7	2073	BKGRND LAC	SNCFLG) Wait for pilot/data
0536	00F8	FF00		BZ) synchronization.
	00F9	00F7			
0537	*				
0538	*			The following two LPFs are for pilot	
0539	*			recovery of the I & Q channel.	
0540	*				
0541	*			Note : the limited internal memory of the	
0542	*			TMS-320 required that the pilot LPF	
0543	*			filter states be stored externally;	
0544	*			however, TBLW/TBLR instructions carry	
0545	*			a 6 cycle overhead for memory access;	
0546	*			to lower this overhead penalty, extra	
0547	*			ram was added to be accessed through	
0548	*			the I/O ports reducing the overhead	
0549	*			to 4 cycles; memory addressing is ac-	
0550	*			complished by an external counter that	
0551	*			is advanced by an CUT ,7 instruction;	
0552	*				
0553	*			I Pilot LPF Code	
0554	*				
0555	00FA	7F89	ZAC		
0556	00FB	6A68	LT	IPILOT	
0557	00FC	9F34	MPYK	PLPF1	
0558	00FD	4774	IN	TEMP1,7	
0559	00FE	4F68	OUT	IPILOT,7	
0560	00FF	6C74	LTA	TEMP1	
0561	0100	9FE6	MPYK	PLPF2	
0562	0101	4768	IN	IPILOT,7	
0563	0102	4F74	OUT	TEMP1,7	
0564	0103	6C68	LTA	IPILOT	
0565	0104	9FF6	MPYK	PLPF3	
0566	0105	4774	IN	TEMP1,7	

0567 0106	4F68	OUT	IPILOT,7
0568 0107	6C74	LTA	TEMP1
0569 0108	8011	MPYK	PLPF4
0570 0109	4768	IN	IPILOT,7
0571 010A	4F74	OUT	TEMP1,7
0572 010B	6C68	LTA	IPILOT
0573 010C	8036	MPYK	PLPF5
0574 010D	4774	IN	TEMP1,7
0575 010E	4F68	OUT	IPILOT,7
0576 010F	6C74	LTA	TEMP1
0577 0110	8060	MPYK	PLPF6
0578 0111	4768	IN	IPILOT,7
0579 0112	4F74	OUT	TEMP1,7
0580 0113	6C68	LTA	IPILOT
0581 0114	8085	MPYK	PLPF7
0582 0115	4774	IN	TEMP1,7
0583 0116	4F68	OUT	IPILOT,7
0584 0117	6C74	LTA	TEMP1
0585 0118	80B0	MPYK	PLPF8
0586 0119	4768	IN	IPILOT,7
0587 011A	4F74	OUT	TEMP1,7
0588 011B	6C68	LTA	IPILOT
0589 011C	80C8	MPYK	PLPF9
0590 011D	4774	IN	TEMP1,7
0591 011E	4F68	OUT	IPILOT,7
0592 011F	6C74	LTA	TEMP1
0593 0120	80C8	MPYK	PLPF10
0594 0121	4768	IN	IPILOT,7
0595 0122	4F74	OUT	TEMP1,7
0596 0123	6C68	LTA	IPILOT
0597 0124	80B4	MPYK	PLPF11
0598 0125	4774	IN	TEMP1,7
0599 0126	4F68	OUT	IPILOT,7
0600 0127	6C74	LTA	TEMP1
0601 0128	8081	MPYK	PLPF12
0602 0129	4768	IN	IPILOT,7
0603 012A	4F74	OUT	TEMP1,7
0604 012B	6C68	LTA	IPILOT
0605 012C	8031	MPYK	PLPF13
0606 012D	4774	IN	TEMP1,7
0607 012E	4F68	OUT	IPILOT,7
0608 012F	6C74	LTA	TEMP1
0609 0130	9FC7	MPYK	PLPF14
0610 0131	4768	IN	IPILOT,7
0611 0132	4F74	OUT	TEMP1,7
0612 0133	6C68	LTA	IPILOT
0613 0134	9F4D	MPYK	PLPF15
0614 0135	4774	IN	TEMP1,7
0615 0136	4F68	OUT	IPILOT,7
0616 0137	6C74	LTA	TEMP1
0617 0138	9EC0	MPYK	PLPF16
0618 0139	4768	IN	IPILOT,7
0619 013A	4F74	OUT	TEMP1,7
0620 013B	6C68	LTA	IPILOT
0621 013C	9E57	MPYK	PLPF17
0622 013D	4774	IN	TEMP1,7
0623 013E	4F68	OUT	IPILOT,7

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0624 013F 6C74	LTA	TEMP1
0625 0140 90FB	MPYK	PLPF18
0626 0141 4768	IN	IPILOT,7
0627 0142 4F74	OUT	TEMP1,7
0628 0143 6C68	LTA	IPILOT
0629 0144 9DCA	MPYK	PLPF19
0630 0145 4774	IN	TEMP1,7
0631 0146 4F68	OUT	IPILOT,7
0632 0147 6C74	LTA	TEMP1
0633 0148 9DD4	MPYK	PLPF20
0634 0149 4768	IN	IPILOT,7
0635 014A 4F74	OUT	TEMP1,7
0636 014B 6C68	LTA	IPILOT
0637 014C 9E27	MPYK	PLPF21
0638 014D 4774	IN	TEMP1,7
0639 014E 4F68	OUT	IPILOT,7
0640 014F 6C74	LTA	TEMP1
0641 0150 9ECA	MPYK	PLPF22
0642 0151 4768	IN	IPILOT,7
0643 0152 4F74	OUT	TEMP1,7
0644 0153 6C68	LTA	IPILOT
0645 0154 9FC1	MPYK	PLPF23
0646 0155 4774	IN	TEMP1,7
0647 0156 4F68	OUT	IPILOT,7
0648 0157 6C74	LTA	TEMP1
0649 0158 8106	MPYK	PLPF24
0650 0159 4768	IN	IPILOT,7
0651 015A 4F74	OUT	TEMP1,7
0652 015B 6C68	LTA	IPILOT
0653 015C 828E	MPYK	PLPF25
0654 015D 4774	IN	TEMP1,7
0655 015E 4F68	OUT	IPILOT,7
0656 015F 6C74	LTA	TEMP1
0657 0160 8446	MPYK	PLPF26
0658 0161 4768	IN	IPILOT,7
0659 0162 4F74	OUT	TEMP1,7
0660 0163 6C68	LTA	IPILOT
0661 0164 8617	MPYK	PLPF27
0662 0165 4774	IN	TEMP1,7
0663 0166 4F68	OUT	IPILOT,7
0664 0167 6C74	LTA	TEMP1
0665 0168 87E5	MPYK	PLPF28
0666 0169 4768	IN	IPILOT,7
0667 016A 4F74	OUT	TEMP1,7
0668 016B 6C68	LTA	IPILOT
0669 016C 8394	MPYK	PLPF29
0670 016D 4774	IN	TEMP1,7
0671 016E 4F68	OUT	IPILOT,7
0672 016F 6C74	LTA	TEMP1
0673 0170 8806	MPYK	PLPF30
0674 0171 4768	IN	IPILOT,7
0675 0172 4F74	OUT	TEMP1,7
0676 0173 6C68	LTA	IPILOT
0677 0174 8C23	MPYK	PLPF31
0678 0175 4774	IN	TEMP1,7
0679 0176 4F68	OUT	IPILOT,7
0680 0177 6C74	LTA	TEMP1

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0681	0178	8CC6	MPYK	PLPF32
0682	0179	4768	IN	IPILOT,7
0683	017A	4F74	OUT	TEMP1,7
0684	017B	6C68	LTA	IPILOT
0685	017C	8D13	MPYK	PLPF33
0686	017D	4774	IN	TEMP1,7
0687	017E	4F68	OUT	IPILOT,7
0688	017F	6C74	LTA	TEMP1
0689	0180	8CD6	MPYK	PLPF32
0690	0181	4768	IN	IPILOT,7
0691	0182	4F74	OUT	TEMP1,7
0692	0183	6C63	LTA	IPILOT
0693	0184	8C23	MPYK	PLPF31
0694	0185	4774	IN	TEMP1,7
0695	0186	4F68	OUT	IPILOT,7
0696	0187	6C74	LTA	TEMP1
0697	0188	8B06	MPYK	PLPF30
0698	0189	4768	IN	IPILOT,7
0699	018A	4F74	OUT	TEMP1,7
0700	018B	6C68	LTA	IPILOT
0701	018C	8994	MPYK	PLPF29
0702	018D	4774	IN	TEMP1,7
0703	018E	4F68	OUT	IPILOT,7
0704	018F	6C74	LTA	TEMP1
0705	0190	87E5	MPYK	PLPF28
0706	0191	4768	IN	IPILOT,7
0707	0192	4F74	OUT	TEMP1,7
0708	0193	6C68	LTA	IPILOT
0709	0194	8617	MPYK	PLPF27
0710	0195	4774	IN	TEMP1,7
0711	0196	4F68	OUT	IPILOT,7
0712	0197	6C74	LTA	TEMP1
0713	0198	8446	MPYK	PLPF26
0714	0199	4768	IN	IPILOT,7
0715	019A	4F74	OUT	TEMP1,7
0716	019B	6C68	LTA	IPILOT
0717	019C	828E	MPYK	PLPF25
0718	019D	4774	IN	TEMP1,7
0719	019E	4F68	OUT	IPILOT,7
0720	019F	6C74	LTA	TEMP1
0721	01A0	8106	MPYK	PLPF24
0722	01A1	4768	IN	IPILOT,7
0723	01A2	4F74	OUT	TEMP1,7
0724	01A3	6C68	LTA	IPILOT
0725	01A4	9FC1	MPYK	PLPF23
0726	01A5	4774	IN	TEMP1,7
0727	01A6	4F68	OUT	IPILOT,7
0728	01A7	6C74	LTA	TEMP1
0729	01A8	9ECA	MPYK	PLPF22
0730	01A9	4768	IN	IPILOT,7
0731	01AA	4F74	OUT	TEMP1,7
0732	01AB	6C68	LTA	IPILOT
0733	01AC	9E27	MPYK	PLPF21
0734	01AD	4774	IN	TEMP1,7
0735	01AE	4F68	OUT	IPILOT,7
0736	01AF	6C74	LTA	TEMP1
0737	01B0	9004	MPYK	PLPF20

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0738 01B1 4768	IN	IPILOT,7
0739 01B2 4F74	OUT	TEMP1,7
0740 01B3 6C68	LTA	IPILOT
0741 01B4 SDCA	MPYK	PLPF19
0742 01B5 4774	IN	TEMP1,7
0743 01B6 4F68	OUT	IPILOT,7
0744 01B7 6C74	LTA	TEMP1
0745 01B8 9DFB	MPYK	PLPF18
0746 01B9 4768	IN	IPILOT,7
0747 01BA 4F74	OUT	TEMP1,7
0748 01BB 6C68	LTA	IPILOT
0749 01BC 9E57	MPYK	PLPF17
0750 01BD 4774	IN	TEMP1,7
0751 01BE 4F68	OUT	IPILOT,7
0752 01BF 6C74	LTA	TEMP1
0753 01C0 9EC0	MPYK	PLPF16
0754 01C1 4768	IN	IPILOT,7
0755 01C2 4F74	OUT	TEMP1,7
0756 01C3 6C68	LTA	IPILOT
0757 01C4 9F4D	MPYK	PLPF15
0758 01C5 4774	IN	TEMP1,7
0759 01C6 4F68	OUT	IPILOT,7
0760 01C7 6C74	LTA	TEMP1
0761 01C8 9FC7	MPYK	PLPF14
0762 01C9 4768	IN	IPILOT,7
0763 01CA 4F74	OUT	TEMP1,7
0764 01CB 6C68	LTA	IPILOT
0765 01CC 8031	MPYK	PLPF13
0766 01CD 4774	IN	TEMP1,7
0767 01CE 4F68	OUT	IPILOT,7
0768 01CF 6C74	LTA	TEMP1
0769 01D0 8081	MPYK	PLPF12
0770 01D1 4768	IN	IPILOT,7
0771 01D2 4F74	OUT	TEMP1,7
0772 01D3 6C68	LTA	IPILOT
0773 01D4 8084	MPYK	PLPF11
0774 01D5 4768	IN	IPILOT,7
0775 01D6 4F68	OUT	IPILOT,7
0776 01D7 6C74	LTA	TEMP1
0777 01D8 80C3	MPYK	PLPF10
0778 01D9 4768	IN	IPILOT,7
0779 01DA 4F68	OUT	IPILOT,7
0780 01DB 6C74	LTA	TEMP1
0781 01DC 80C8	MPYK	PLPF9
0782 01DD 4768	IN	IPILOT,7
0783 01DE 4F68	OUT	IPILOT,7
0784 01DF 6C74	LTA	TEMP1
0785 01E0 8080	MPYK	PLPF9
0786 01E1 4768	IN	IPILOT,7
0787 01E2 4F68	OUT	IPILOT,7
0788 01E3 6C74	LTA	TEMP1
0789 01E4 8083	MPYK	PLPF7
0790 01E5 4768	IN	IPILOT,7
0791 01E6 4F68	OUT	IPILOT,7
0792 01E7 6C74	LTA	TEMP1
0793 01E8 8060	MPYK	PLPF6
0794 01E9 4763	IN	IPILOT,7

0795	01EA	4F68	OUT	IPILOT,7
0796	01EB	6C74	LTA	TEMP1
0797	01EC	8036	MPYK	PLPFS
0798	01ED	4768	IN	IPILOT,7
0799	01EE	4F68	OUT	IPILOT,7
0800	01EF	6C74	LTA	TEMP1
0801	01F0	8011	MPYK	PLPF4
0802	01F1	4768	IN	IPILOT,7
0803	01F2	4F68	OUT	IPILOT,7
0804	01F3	6C74	LTA	TEMP1
0805	01F4	9FF6	MPYK	PLPF3
0806	01F5	4768	IN	IPILOT,7
0807	01F6	4F68	OUT	IPILOT,7
0808	01F7	6C74	LTA	TEMP1
0809	01F8	9FE6	MPYK	PLPF2
0810	01F9	4768	IN	IPILOT,7
0811	01FA	4F68	OUT	IPILOT,7
0812	01FB	6C74	LTA	TEMP1
0813	01FC	9F34	MPYK	PLPF1
0814	01FD	7F8F	APAC	
0815	01FE	5968	SACH	IPILOT,1
0816	*			
0817	*			Q Pilct LPF Code
0818	*			
0819	01FF	7F89	ZAC	
0820	0200	6A68	LT	QPILOT
0821	0201	9F34	MPYK	PLPF1
0822	0202	4774	IN	TEMP1,7
0823	0203	4F68	OUT	QPILOT,7
0824	0204	6C74	LTA	TEMP1
0825	0205	9FE6	MPYK	PLPF2
0825	0206	4768	IN	QPILOT,7
0827	0207	4F74	OUT	TEMP1,7
0828	0208	6C68	LTA	QPILOT
0829	0209	9FF6	MPYK	PLPF3
0830	020A	4774	IN	TEMP1,7
0831	020B	4F68	OUT	QPILOT,7
0832	020C	6C74	LTA	TEMP1
0833	020D	8011	MPYK	PLPF4
0834	020E	4768	IN	QPILOT,7
0835	020F	4F74	OUT	TEMP1,7
0836	0210	6C68	LTA	QPILOT
0837	0211	8036	MPYK	PLPF5
0838	0212	4774	IN	TEMP1,7
0839	0213	4F68	OUT	QPILOT,7
0840	0214	6C74	LTA	TEMP1
0841	0215	8060	MPYK	PLPF6
0842	0216	4768	IN	QPILOT,7
0843	0217	4F74	OUT	TEMP1,7
0844	0218	6C68	LTA	QPILOT
0845	0219	808B	MPYK	PLPF7
0846	021A	4774	IN	TEMP1,7
0847	021B	4F68	OUT	QPILOT,7
0848	021C	6C74	LTA	TEMP1
0849	021D	8080	MPYK	PLPF8
0850	021E	4768	IN	QPILOT,7
0851	021F	4F74	OUT	TEMP1,7

0852 0220 6C6B	LTA	QPILOT
0853 0221 80C8	MPYK	PLPF9
0854 0222 4774	IN	TEMP1,7
0855 0223 4F6B	OUT	QPILOT,7
0856 0224 6C74	LTA	TEMP1
0857 0225 80C8	MPYK	PLPF10
0858 0226 476B	IN	QPILOT,7
0859 0227 4F74	OUT	TEMP1,7
0860 0228 6C6B	LTA	QPILOT
0861 0229 80B4	MPYK	PLPF11
0862 022A 4774	IN	TEMP1,7
0863 022B 4F6B	OUT	QPILOT,7
0864 022C 6C74	LTA	TEMP1
0865 022D 8081	MPYK	PLPF12
0866 022E 476B	IN	QPILOT,7
0867 022F 4F74	OUT	TEMP1,7
0868 0230 6C6B	LTA	QPILOT
0869 0231 8031	MPYK	PLPF13
0870 0232 4774	IN	TEMP1,7
0871 0233 4F6B	OUT	QPILOT,7
0872 0234 6C74	LTA	TEMP1
0873 0235 9FC7	MPYK	PLPF14
0874 0236 476B	IN	QPILOT,7
0875 0237 4F74	OUT	TEMP1,7
0876 0238 6C6B	LTA	QPILOT
0877 0239 9F4D	MPYK	PLPF15
0878 023A 4774	IN	TEMP1,7
0879 023B 4F6B	OUT	QPILOT,7
0880 023C 6C74	LTA	TEMP1
0881 023D 9ECD	MPYK	PLPF16
0882 023E 476B	IN	QPILOT,7
0883 023F 4F74	OUT	TEMP1,7
0884 0240 6C6B	LTA	QPILOT
0885 0241 9E57	MPYK	PLPF17
0886 0242 4774	IN	TEMP1,7
0887 0243 4F6B	OUT	QPILOT,7
0888 0244 6C74	LTA	TEMP1
0889 0245 9DF3	MPYK	PLPF18
0890 0246 476B	IN	QPILOT,7
0891 0247 4F74	OUT	TEMP1,7
0892 0248 6C6B	LTA	QPILOT
0893 0249 9DCA	MPYK	PLPF19
0894 024A 4774	IN	TEMP1,7
0895 024B 4F6B	OUT	QPILOT,7
0896 024C 6C74	LTA	TEMP1
0897 024D 9DD4	MPYK	PLPF20
0898 024E 476B	IN	QPILOT,7
0899 024F 4F74	OUT	TEMP1,7
0900 0250 6C6B	LTA	QPILOT
0901 0251 9E27	MPYK	PLPF21
0902 0252 4774	IN	TEMP1,7
0903 0253 4F6B	OUT	QPILOT,7
0904 0254 6C74	LTA	TEMP1
0905 0255 9ECA	MPYK	PLPF22
0906 0256 476B	IN	QPILOT,7
0907 0257 4F74	OUT	TEMP1,7
0908 0258 6C6B	LTA	QPILOT

0909	0259	9FC1	MPYK	PLPF23
0910	025A	4774	IN	TEMP1,7
0911	025B	4F6B	OUT	QPILOT,7
0912	025C	6C74	LTA	TEMP1
0913	025D	8106	MPYK	PLPF24
0914	025E	476B	IN	QPILOT,7
0915	025F	4F74	OUT	TEMP1,7
0916	0260	6C6B	LTA	QPILOT
0917	0261	828E	MPYK	PLPF25
0918	0262	4774	IN	TEMP1,7
0919	0263	4F6B	OUT	QPILOT,7
0920	0264	6C74	LTA	TEMP1
0921	0265	8446	MPYK	PLPF26
0922	0266	476B	IN	QPILOT,7
0923	0267	4F74	OUT	TEMP1,7
0924	0268	6C6B	LTA	QPILOT
0925	0269	8617	MPYK	PLPF27
0926	026A	4774	IN	TEMP1,7
0927	026B	4F6B	OUT	QPILOT,7
0928	026C	6C74	LTA	TEMP1
0929	026D	87E5	MPYK	PLPF28
0930	026E	476B	IN	QPILOT,7
0931	026F	4F74	OUT	TEMP1,7
0932	0270	6C6B	LTA	QPILOT
0933	0271	8994	MPYK	PLPF29
0934	0272	4774	IN	TEMP1,7
0935	0273	4F6B	OUT	QPILOT,7
0936	0274	6C74	LTA	TEMP1
0937	0275	8306	MPYK	PLPF30
0938	0276	476B	IN	QPILOT,7
0939	0277	4F74	OUT	TEMP1,7
0940	0278	6C6B	LTA	QPILOT
0941	0279	8C23	MPYK	PLPF31
0942	027A	4774	IN	TEMP1,7
0943	027B	4F6B	OUT	QPILOT,7
0944	027C	6C74	LTA	TEMP1
0945	027D	8CD6	MPYK	PLPF32
0946	027E	4763	IN	QPILOT,7
0947	027F	4F74	OUT	TEMP1,7
0948	0280	6C6B	LTA	QPILOT
0949	0281	8D13	MPYK	PLPF33
0950	0282	4774	IN	TEMP1,7
0951	0283	4F6B	OUT	QPILOT,7
0952	0284	6C74	LTA	TEMP1
0953	0285	8CD6	MPYK	PLPF32
0954	0286	476B	IN	QPILOT,7
0955	0287	4F74	OUT	TEMP1,7
0956	0288	6C6B	LTA	QPILOT
0957	0289	8C23	MPYK	PLPF31
0958	028A	4774	IN	TEMP1,7
0959	028B	4F6B	OUT	QPILOT,7
0960	028C	6C74	LTA	TEMP1
0961	028D	8B06	MPYK	PLPF30
0962	028E	476B	IN	QPILOT,7
0963	028F	4F74	OUT	TEMP1,7
0964	0290	6C6B	LTA	QPILOT
0965	0291	8994	MPYK	PLPF29

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0966	0292	4774	IN	TEMP1,7
0967	0293	4F6B	OUT	QPILOT,7
0968	0294	6C74	LTA	TEMP1
0969	0295	87E5	MPYK	PLPF28
0970	0296	476B	IN	QPILOT,7
0971	0297	4F74	OUT	TEMP1,7
0972	0298	6C6B	LTA	QPILOT
0973	0299	8617	MPYK	PLPF27
0974	029A	4774	IN	TEMP1,7
0975	029B	4F6B	OUT	QPILOT,7
0976	029C	6C74	LTA	TEMP1
0977	029D	8446	MPYK	PLPF26
0978	029E	476B	IN	QPILOT,7
0979	029F	4F74	OUT	TEMP1,7
0980	02A0	6C63	LTA	QPILOT
0981	02A1	828E	MPYK	PLPF25
0982	02A2	4774	IN	TEMP1,7
0983	02A3	4F6B	OUT	QPILOT,7
0984	02A4	6C74	LTA	TEMP1
0985	02A5	8106	MPYK	PLPF24
0986	02A6	476B	IN	QPILOT,7
0987	02A7	4F74	OUT	TEMP1,7
0988	02A8	6C63	LTA	QPILOT
0989	02A9	9FC1	MPYK	PLPF23
0990	02AA	4774	IN	TEMP1,7
0991	02AB	4F6B	OUT	QPILOT,7
0992	02AC	6C74	LTA	TEMP1
0993	02AD	SECA	MPYK	PLPF22
0994	02AE	476B	IN	QPILOT,7
0995	02AF	4F74	OUT	TEMP1,7
0996	02B0	6C6B	LTA	QPILOT
0997	02B1	9E27	MPYK	PLPF21
0998	02B2	4774	IN	TEMP1,7
0999	02B3	4F6B	OUT	QPILOT,7
1000	02B4	6C74	LTA	TEMP1
1001	02B5	9DD4	MPYK	PLPF20
1002	02B6	476B	IN	QPILOT,7
1003	02B7	4F74	OUT	TEMP1,7
1004	02B8	6C6B	LTA	QPILOT
1005	02B9	9DCA	MPYK	PLPF19
1006	02BA	4774	IN	TEMP1,7
1007	02BB	4F6B	OUT	QPILOT,7
1008	02BC	6C74	LTA	TEMP1
1009	02BD	9DF3	MPYK	PLPF18
1010	02BE	476B	IN	QPILOT,7
1011	02BF	4F74	OUT	TEMP1,7
1012	02C0	6C6B	LTA	QPILOT
1013	02C1	9E57	MPYK	PLPF17
1014	02C2	4774	IN	TEMP1,7
1015	02C3	4F6B	OUT	QPILOT,7
1016	02C4	6C74	LTA	TEMP1
1017	02C5	SECD	MPYK	PLPF16
1018	02C6	476B	IN	QPILOT,7
1019	02C7	4F74	OUT	TEMP1,7
1020	02C8	6C6B	LTA	QPILOT
1021	02C9	9F4D	MPYK	PLPF15
1022	02CA	4774	IN	TEMP1,7

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1023	02CB	4F6B	OUT	QPILOT,7
1024	02CC	6C74	LTA	TEMP1
1025	02CD	9FC7	MPYK	PLPF14
1026	02CE	476B	IN	QPILOT,7
1027	02CF	4F74	OUT	TEMP1,7
1028	02D0	6C6B	LTA	QPILOT
1029	02D1	8031	MPYK	PLPF13
1030	02D2	4774	IN	TEMP1,7
1031	02D3	4F63	OUT	QPILOT,7
1032	02D4	6C74	LTA	TEMP1
1033	02D5	8081	MPYK	PLPF12
1034	02D6	476B	IN	QPILOT,7
1035	02D7	4F74	OUT	TEMP1,7
1036	02D8	6C63	LTA	QPILOT
1037	02D9	8084	MPYK	PLPF11
1038	02DA	476B	IN	IPILOT,7
1039	02DB	4F68	OUT	IPILOT,7
1040	02DC	6C74	LTA	TEMP1
1041	02DD	80C9	MPYK	PLPF10
1042	02DE	476B	IN	IPILOT,7
1043	02DF	4F68	OUT	IPILOT,7
1044	02E0	6C74	LTA	TEMP1
1045	02E1	80C8	MPYK	PLPF9
1046	02E2	476B	IN	IPILOT,7
1047	02E3	4F68	OUT	IPILOT,7
1048	02E4	6C74	LTA	TEMP1
1049	02E5	80B0	MPYK	PLPF8
1050	02E6	476B	IN	IPILOT,7
1051	02E7	4F68	OUT	IPILOT,7
1052	02E8	6C74	LTA	TEMP1
1053	02E9	8088	MPYK	PLPF7
1054	02EA	476B	IN	IPILOT,7
1055	02EB	4F68	OUT	IPILOT,7
1056	02EC	6C74	LTA	TEMP1
1057	02ED	8060	MPYK	PLPF6
1058	02EE	476B	IN	IPILOT,7
1059	02EF	4F68	OUT	IPILOT,7
1060	02F0	6C74	LTA	TEMP1
1061	02F1	8036	MPYK	PLPF5
1062	02F2	476B	IN	IPILOT,7
1063	02F3	4F68	OUT	IPILOT,7
1064	02F4	6C74	LTA	TEMP1
1065	02F5	8011	MPYK	PLPF4
1066	02F6	476B	IN	IPILOT,7
1067	02F7	4F68	OUT	IPILOT,7
1068	02F8	6C74	LTA	TEMP1
1069	02F9	9FF6	MPYK	PLPF3
1070	02FA	476B	IN	IPILOT,7
1071	02FB	4F68	OUT	IPILOT,7
1072	02FC	6C74	LTA	TEMP1
1073	02FD	9FE6	MPYK	PLPF2
1074	02FE	476B	IN	IPILOT,7
1075	02FF	4F68	OUT	IPILOT,7
1076	0300	6C74	LTA	TEMP1
1077	0301	9F34	MPYK	PLPF1
1078	0302	7F8F	APAC	
1079	0303	5968	SACH	QPILOT,1

1080 *
 1081 * Sine and Cosine Calculation
 1082 *
 1083 * The values for sin & cos are
 1084 * stored for the region 0 - pi/4
 1085 * in 128 locations each; the pilot
 1086 * samples are first stripped for
 1087 * sign and then compared to determine
 1088 * the octant before table lookup;
 1089 * the sign is then re-appended after
 1090 * the values have been determined;
 1091 *

1092 0304 6568	ZALH	QPILOT)	
1093 0305 587C	SACH	QSIGN) Strip Q pilot sign.	
1094 0306 7F88	ABS)	
1095 0307 5874	SACH	TEMP1		
1096 0308 6568	ZALH	IPILOT)	
1097 0309 587B	SACH	ISIGN) Strip I pilot sign.	
1098 030A 7F88	ABS)	
1099 030B 5875	SACH	TEMP2		
1100 030C 6274	SUBH	TEMP1) Compare magnitudes to	
1101 030C FA00	BLZ	IOVERC) determine octant.	
030E 0342				
1102 *				
1103 030F 6574	COVERI	ZALH	TEMP1) Check if denominator
1104 0310 FE00		BNZ	DIVQOI) equals zero.
0311 0319				
1105 0312 7F89	ZAC			
1106 0313 5061	SACL	COS		
1107 0314 7E01	LACK	>1		
1108 0315 007A	ADD	SNOFST		
1109 0316 675E	TBLR	SIN		
1110 0317 F900	E	FIXSGN		
0318 032F				
1111 *				
1112 *	N.B. :	NOP's are inserted after each SUBC instruction because the instruction following a SUBC may not use the accumulator.		
1113 *				
1114 *				
1115 *				
1116 *				
1117 0319 6475	DIVQCI	SUBC	TEMP2) 7 Bit Fractional
1118 031A 7F80		NOP		
1119 031B 6475	SUBC	TEMP2) Divide
1120 031C 7F80	NOP			.
1121 031D 6475	SUBC	TEMP2		.
1122 031E 7F80	NOP			.
1123 031F 6475	SUBC	TEMP2		.
1124 0320 7F80	NOP			.
1125 0321 6475	SUBC	TEMP2		.
1126 0322 7F80	NOP			.
1127 0323 6475	SUBC	TEMP2		.
1128 0324 7F80	NOP			.
1129 0325 6475	SUBC	TEMP2) End of Divide
1130 0326 7F80	NOP			
1131 0327 5075	SACL	TEMP2		
1132 0328 2175	LAC	TEMP2,I		
1133 0329 007A	ADD	SNOFST		

1134 032A 675E		TBLR	SIN	> Read sine value.
1135 032B 5075		SACL	TEMP2	
1136 032C 7E01		LACK	1	> Increment lookup address.
1137 032C 0075		ADD	TEMP2	
1138 032E 6761		TBLR	COS	> Read cosine value.
1139 032F 6578	FIXSGN	ZALH	ISIGN	
1140 0330 FA00		BLZ	SUBI1	>
0331 0337				
1141 0332 657C		ZALH	QSIGN	> Re-append Sign.
1142 0333 FA00		BLZ	SUBQ1	>
0334 033E				
1143 0335 F900		B	STEPS	
0336 0373				
1144 0337 1061	SUBI1	SUB	COS	
1145 0338 5061		SACL	COS	
1146 0339 657C		ZALH	QSIGN	
1147 033A FA00		BLZ	SUBQ1	
033E 033E				
1148 033C F900		B	STEPS	
033D 0373				
1149 033E 105E	SUBQ1	SUB	SIN	
1150 033F 505E		SACL	SIN	
1151 0340 F900		B	STEPS	
0341 0373				
1152 *				
1153 0342 6575	IOVERQ	ZALH	TEMP2	> Check if denominator
1154 0343 FE00		BNZ	DIVICQ	> equals zero.
0344 034C				
1155 0345 7F89		ZAC		
1156 0346 505E		SACL	SIN	
1157 0347 7E01		LACK	>1	
1158 0348 007A		ADD	SNOFST	
1159 0349 6761		TBLR	CCS	
1160 034A F900		B	SGNFX	
034B 0362				
1161 *				
1162 *		N.B. : NOP's are inserted after each SUBC		
1163 *		instruction because the instruction		
1164 *		following a SUBC may not use the		
1165 *		accumulator.		
1166 *				
1167 034C 6474	DIVICQ	SUBC	TEMP1	> 7 Bit Fractional
1168 034C 7F80		NOP		
1169 034E 6474		SUBC	TEMP1	> Divide
1170 034F 7F80		NOP		
1171 0350 6474		SUBC	TEMP1	> .
1172 0351 7F80		NOP		
1173 0352 6474		SUBC	TEMP1	> .
1174 0353 7F80		NOP		
1175 0354 6474		SUBC	TEMP1	> .
1176 0355 7F80		NOP		
1177 0356 6474		SUBC	TEMP1	> .
1178 0357 7F80		NOP		
1179 0358 6474		SUBC	TEMP1	> End of Divide
1180 0359 7F80		NOP		
1181 035A 5074		SACL	TEMP1	
1182 035B 2174		LAC	TEMP1,1	

1183	035C	007A	ADD	SNOFST		
1184	035C	6761	TBLR	COS	} Read cosine value.	
1185	035E	5075	SACL	TEMP2		
1186	035F	7E01	LACK	1	} Increment lookup address.	
1187	0360	0075	ADD	TEMP2		
1188	0361	675E	TBLR	SIN	} Read sine value.	
1189	0362	6578	SGNFX	ZALH	ISIGN	
1190	0363	FA00	BLZ	SUBI2	}	
	0364	036A				
1191	0365	657C	ZALH	QSIGN	} Re-append Sign.	
1192	0366	FA00	BLZ	SUBQ2	}	
	0367	0371				
1193	0368	F900	B	STEPS		
	0369	0373				
1194	036A	1061	SUBI2	SUB	COS	
1195	036B	5061	SACL	COS	ORIGINAL PAGE IS	
1196	036C	657C	ZALH	QSIGN	OF POOR QUALITY.	
1197	036D	FA00	BLZ	SUBQ2		
	036E	0371				
1198	036F	F900	B	STEPS		
	0370	0373				
1199	0371	105E	SUBQ2	SUB	SIN	
1200	0372	505E	SACL	SIN		
1201	*					
1202	*			Calculate Pilot, Cosine		
1203	*			and Sine Step Sizes.		
1204	*					
1205	0373	6562	STEPS	ZALH	PRECOS	
1206	0374	6261		SUBH	COS	
1207	0375	5878		SACH	ISIGN,0	
1208	0376	7F88		ABS		
1209	0377	5874		SACH	TEMP1,0	
1210	0378	6A74		LT	TEMP1	
1211	*					
1212	0379	8333		MPYK	>333	} Multiply by 1/5.
1213	037A	7F8E		PAC		
1214	037B	0B72		ADD	ONE,11	} Round off result.
1215	*					
1216	037C	5066		SACL	COSSTP	
1217	037D	6578		ZALH	ISIGN	
1218	037E	FD00		BGEZ	NEXT1	
	037F	0382				
1219	0380	1066		SUB	COSSTP	} Correct for negative
1220	0381	5066		SACL	COSSTP	} result.
1221	*					
1222	0382	655F	NEXT1	ZALH	PRESIN	
1223	0383	625E		SUBH	SIN	
1224	0384	587C		SACH	QSIGN,0	
1225	0385	7F88		ABS		
1226	0386	5874		SACH	TEMP1,0	
1227	0387	6A74		LT	TEMP1	
1228	*					
1229	0388	8333		MPYK	>333	} Multiply by 1/5.
1230	0389	7F8E		PAC		
1231	038A	0B72		ADD	ONE,11	} Round off result.
1232	*					
1233	038B	5064		SACL	SINSTP	

1234	038C	657C	ZALH	QSIGN	
1235	038D	F000	BGEZ	NEXT2	
	038E	0391			
1236	038F	1064	SUB	SINSTP	> Correct for negative
1237	0390	5064	SACL	SINSTP	> result.
1238	*				
1239	0391	6569	NEXT2	ZALH	OLDIP
1240	0392	6268	SUBH	PILOT	ORIGINAL PAGE IS
1241	0393	587B	SACH	ISIGN,0	QE POOR QUALITY.
1242	0394	7F88	ABS		
1243	0395	5874	SACH	TEMP1,0	
1244	0396	6A74	LT	TEMP1	
1245	*				
1246	0397	8333	MPYK	>333	> Multiply by 1/5.
1247	0398	7F8E	PAC		
1248	0399	0872	ADD	ONE,11	> Round off result.
1249	*				
1250	039A	506E	SACL	IPSTP	
1251	039B	6578	ZALH	ISIGN	
1252	039C	F000	BGEZ	NEXT3	
	039D	03A0			
1253	039E	106E	SUB	IPSTP	> Correct for negative
1254	039F	506E	SACL	IPSTP	> result.
1255	*				
1256	03A0	656C	NEXT3	ZALH	OLDQP
1257	03A1	626B	SUBH	QPILOT	
1258	03A2	587C	SACH	QSIGN,0	
1259	03A3	7F88	ABS		
1260	03A4	5874	SACH	TEMP1	
1261	03A5	6A74	LT	TEMP1	
1262	*				
1263	03A6	8333	MPYK	>333	> Multiply by 1/5.
1264	03A7	7F8E	PAC		
1265	03A8	0872	ADD	ONE,11	> Round off result.
1266	*				
1267	03A9	5070	SACL	QPSTP	
1268	03AA	657C	ZALH	QSIGN	
1269	*				
1270	03AB	4072	OUT	ONE,5	> Reset ram counters.
1271	*				
1272	03AC	F000	BGEZ	BKGRND	
	03AC	00F7			
1273	03AE	1070	SUB	QPSTP	> Correct for negative
1274	03AF	5070	SACL	QPSTP	> result.
1275	*				
1276	03B0	F900	B	BKGRND	
	03B1	00F7			
1277	*				
1278	*			Reset Initialization Routine	
1279	*				
1280	03B2	6E00	RESET	LDPK	0 > Point to data page 0.
1281	03B3	7F88		SOVM	> Set overflow mode.
1282	*				
1283	03B4	4000	IN	>0,0	> Clear interrupt pin.
1284	03B5	4000	OUT	>0,5	> Reset ram counters.
1285	*				
1286	03B6	7E01	LACK	1	

1287	0387	5000	SACL	>0	
1288	0388	6A00	LT	>0	
1289	*		LARP	0	ORIGINAL PAGE IS OE POOR QUALITY
1290	0389	6880	LARK	0,>7F	
1291	038A	707F	ZAC		}
1292	038B	7F89	CLRRAM	SACL *	Clear internal ram.
1293	038C	5088	BANZ	CLRRAM	}
1294	038D	F400			
	038E	03BC			
1295	*				
1296	038F	7054	LARK	0,IBUFF	Initialize auxiliary
1297	03C0	7159	LARK	1,QBUFF	} register pointers.
1298	*		LACK	1	}
1299	03C1	7E01	SACL	ONE	}
1300	03C2	5072	MPYK	OFFSET	} Store constants in ram.
1301	03C3	8500	PAC		}
1302	03C4	7F8E	SACL	CSDFST	}
1303	03C5	507A			
1304	*		B	BKGRND	Branch to waiting state.
1305	03C6	F900			
	03C7	00F7			
1306	*				
1307	*				
1308	*		Sine and Cosine Table Lookup Values		
1309	*				
1310	*				
1311	0500		AORG	>500	
1312	*				
1313	0500	0000	DATA	0,32767,258,32767,516,32764	
	0501	7FFF			
	0502	0102			
	0503	7FFF			
	0504	0204			
	0505	7FFC			
1314	0506	0306	DATA	774,32759,1032,32752,1289,32743	
	0507	7FF7			
	0508	0408			
	0509	7FF0			
	050A	0509			
	050B	7FE7			
1315	050C	060A	DATA	1546,32731,1803,32718,2060,32703	
	050D	7FD8			
	050E	0703			
	050F	7FCF			
	0510	080C			
	0511	7FBF			
1316	0512	090C	DATA	2316,32686,2572,32667,2828,32646	
	0513	7FAE			
	0514	0A0C			
	0515	7F98			
	0516	0B0C			
	0517	7F86			
1317	0518	0C0A	DATA	3082,32623,3337,32598,3590,32571	
	0519	7F6F			
	051A	0D09			
	051B	7F56			
	051C	0E06			

051C	7F3B			
1318	051E	0F04	DATA	3844,32542,4096,32511,4347,32478
	051F	7F1E		
	0520	1000		
	0521	7EFF		
	0522	10F3		
	0523	7EDE		
1319	0524	11F6	DATA	4598,32444,4848,32407,5097,32369
	0525	7EBC		
	0526	12F0		
	0527	7E97		
	0528	13E9		
	0529	7E71		
1320	052A	14E2	DATA	5346,32329,5593,32287,5839,32244
	052B	7E49		
	052C	15D9		
	052D	7E1F		
	052E	16CF		
	052F	7DF4		
1321	0530	17C5	DATA	6085,32198,6329,32151,6572,32102
	0531	7DC6		
	0532	1889		
	0533	7D97		
	0534	19AC		
	0535	7D66		
1322	0536	1A9E	DATA	6814,32052,7055,32000,7295,31946
	0537	7D34		
	0538	188F		
	0539	7D00		
	053A	1C7F		
	053B	7CCA		
1323	053C	1D6D	DATA	7533,31890,7770,31833,8006,31775
	053D	7C92		
	053E	1E5A		
	053F	7C59		
	0540	1F46		
	0541	7C1F		
1324	0542	2031	DATA	8241,31715,8474,31653,8706,31590
	0543	78E3		
	0544	211A		
	0545	7BA5		
	0546	2202		
	0547	7B66		
1325	0548	22E8	DATA	8936,31526,9166,31460,9393,31393
	0549	7B26		
	054A	23CE		
	054B	7AE4		
	054C	24B1		
	054D	7AA1		
1326	054E	2593	DATA	9619,31324,9844,31254,10067,31183
	054F	7A5C		
	0550	267+		
	0551	7A16		
	0552	2753		
	0553	79CF		
1327	0554	2831	DATA	10289,31111,10509,31037,10727,30962
	0555	7987		

0556 2900
0557 7930
0558 29E7
0559 7BF2
1328 055A 2AC0 DATA 10944,30886,11159,30809,11373,30731
055B 78A6
055C 2B97
055D 7859
055E 2C60
055F 780B
1329 0560 2D41 DATA 11585,30652,11795,30571,12004,30490
0561 77EC
0562 2E13
0563 776B
0564 2EE4
0565 771A
1330 0566 2FE3 DATA 12211,30408,12416,30325,12620,30240
0567 76C8
0568 3080
0569 7675
056A 314C
056B 7620
1331 056C 3216 DATA 12822,30155,13022,30069,13221,29983
056D 75C8
056E 320E
056F 7575
0570 33A5
0571 751F
1332 0572 3469 DATA 13417,29895,13613,29807,13806,29718
0573 74C7
0574 352D
0575 746F
0576 35EE
0577 7416
1333 0578 36AD DATA 13997,29628,14187,29537,14375,29446
0579 738C
057A 376B
057B 7361
057C 3827
057D 7306
1334 057E 38E2 DATA 14562,29355,14746,29262,14929,29169
057F 72A8
0580 399A
0581 724E
0582 3A51
0583 71F1
1335 0584 3806 DATA 15110,29076,15290,28982,15467,28888
0585 7194
0586 3B8A
0587 7136
0588 3C6B
0589 70D8
1336 058A 3D16 DATA 15643,28793,15818,28698,15990,28602
058B 7079
058C 3DCA
058D 701A
058E 3E76

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058F 6FBA
1337 0590 3F21 DATA 16161,28506,16330,28409,16497,28312
0591 6F5A
0592 3FC4
0593 6EF9
0594 4071
0595 6E98
1338 0596 4117 DATA 16663,28215,16826,28118,16989,28020
0597 6E37
0598 41BA
0599 60D6
059A 425D
059B 6074
1339 059C 42FD DATA 17149,27922,17308,27824,17465,27726
059D 6D12
059E 439C
059F 6CB0
05A0 4439
05A1 6C4E
1340 05A2 44D4 DATA 17620,27627,17774,27528,17926,27430
05A3 68EB
05A4 456E
05A5 6888
05A6 4606
05A7 6B25
1341 05A8 469D DATA 18077,27331,18226,27232,18373,27132
05A9 6AC3
05AA 4732
05AB 6A60
05AC 47C5
05AD 69FC
1342 05AE 4857 DATA 18519,27033,18663,26934,18905,26835
05AF 6999
05B0 48E7
05B1 6936
05B2 4975
05B3 68D3
1343 05B4 4A02 DATA 18946,26735,19086,26636,19223,26537
05B5 686F
05B6 4A8E
05B7 680C
05B8 4B17
05B9 67A3
1344 05B0 48A0 DATA 19360,26438,19494,26338,19628,26239
05B8 6746
05B9 4C26
05B0 66E2
05B1 4CAC
05B2 667F
1345 05C0 4D2F DATA 19759,26140,19890,26041,20018,25942
05C1 661C
05C2 4DB2
05C3 65B9
05C4 4E32
05C5 6556
1346 05C6 4EB2 DATA 20146,25844,20272,25745,20396,25647
05C7 64F4

ORIGINAL PAGE IS
OF POOR QUALITY

05C8 4F30
05C9 6491
05CA 4FAC
05CB 642F

ORIGINAL PAGE IS
OF POOR QUALITY

1347 05CC 5027 DATA 20519,25548,20641,25450,20761,25352

05CD 63CC
05CE 50A1
05CF 636A
05D0 5119
05D1 6308

1348 05D2 5190 DATA 20880,25254,20997,25157,21113,25059

05D3 62A6
05D4 5205
05D5 6245
05D6 5279
05D7 61E3

1349 05D8 52EC DATA 21229,24962,21341,24865,21453,24769

05D9 6182
05DA 5350
05DB 6121
05DC 53CD
05DD 60C1

1350 05DE 543C DATA 21564,24672,21674,24576,21782,24480

05DF 6060
05E0 54AA
05E1 6000
05E2 5516
05E3 5FA0

1351 05E4 5581 DATA 21889,24385,21995,24290,22099,24195

05E5 5F41
05E6 55E8
05E7 5EE2
05E8 5653
05E9 5E83

1352 05EA 56BA DATA 22202,24100,22304,24005,22405,23911

05EB 5E24
05EC 5720
05ED 5DC5
05EE 5785
05EF 5D67

1353 05F0 57E9 DATA 22505,23818,22603,23724,22701,23631

05F1 5D0A
05F2 584B
05F3 5CAC
05F4 58AD
05F5 5C4F

1354 05F6 5900 DATA 22797,23538,22892,23446,22986,23354

05F7 5BF2
05F8 596C
05F9 5B96
05FA 59CA
05FB 5B3A

1355 05FC 5A27 DATA 23079,23262,23170,23170

05FD 5ADE

05FE 5A82

05FF 5A82

1356 *

1357 * Bootstrapping Routine for
1358 * Loading Program Code from
1359 * EPROM's to RAM.
1360 *
1361 0700 AORG >700
1362 *
1363 0700 7E01 BOOT LACK >1
1364 0701 5000 SACL >0
1365 0702 6A00 LT >0
1366 0703 87FF MPYK >7FF
1367 0704 7F8E PAC
1368 0705 670A NOTDUN TBLR >A
1369 0706 7D0A TBLW >A
1370 0707 1000 SUB >0
1371 0708 FD00 BGEZ NOTDOUN
0709 0705
1372 070A 8382 MPYK RESET
1373 070B 7F8E PAC
1374 070C 500A SACL >A
1375 070D 7E01 LACK >1
1376 070E 7D0A TBLW >A
1377 070F F900 B RESET
0710 0382
1378 *
1379 END

NO ERRORS, NO WARNINGS

ORIGINAL COPY MADE
OF POOR QUALITY